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THE MEMPHIS DEPOT TENNESSEE

ADMINISTRATIVE RECORD COVER SHEET

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Memphis Depot Main Installation

Remedial Design Workplan



Defense Distribution Center (Memphis)

July 2002 — Rev. 2





U.S. Army Engineering and Support Center, Huntsville

Remedial Design Workplan for the Main Installation of the Memphis Depot Memphis, Tennessee

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- B Rev. 1 Main Installation EBT Treatability Study Workplan
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Acronyms

BCT BRAC Cleanup Team

BRAC Base Realignment and Closure

CERCLA Comprehensive Environmental Response, compensation, and Liability Act

COCs chemicals of concern

DLA Defense Logistics Agency

DNAPL dense non-aqueous phase liquid

DoD Department of Defense

DOI/NPS Department of Interior/National Park Service

DQOs data quality objectives

DRC Depot Redevelopment Corporation
EBT Enhanced Bioremediation Treatment

ELCR Excess lifetime cancer risk

EPA U.S. Environmental Protection Agency
ESD Explanation of Significant Differences

FFA Federal Facilities Agreement

FR Federal Register
FS Feasibility Study

ft² square feet

FU Functional Unit

HASP Health and Safety Plan

HHRA human health risk assessment

IR Information Repository
IRAs Interim remedial actions

LTOA Long-Term Operational Area

LUCIP land use controls implementation plan

MCLs maximum contaminant levels

μg/L micrograms per liter

mg/kg milligrams per kilogram

MI Main Installation

NCP National Oil and Hazardous Pollution Contingency Plan

NPL National Priorities List

O&M Operation and maintenance

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OU Operable Unit

PAHs polynuclear aromatic hydrocarbons

PCBs polychlorinated biphenyls

PCE tetrachloroethene

PCP products with pentachlorophenol

POL petroleum/oil/lubricants

QAPP Quality Assurance Project Plan

RA remedial action

RAOs remedial action objectives

RCRA Resource Conservation and Recovery Act

RD Remedial Design

RFA Resource Facility Assessment

RI Remedial Investigation

ROD Record of Decision

SAP Sampling and Analysis Plan

SARA Superfund Amendments and Reauthorization Act

TCE trichloroethene

TDEC Tennessee Department of Environment and Conservation

USACE U.S. Army Corps of Engineers

USAESCH U.S. Army Engineering and Support Center

USC United States Code

VOCs volatile organic compounds

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Foreword

The Rev. 1 Memphis Depot Main Installation Remedial Design (RD) Workplan was approved by EPA on May 2, 2002. However, that workplan did not contain the Long-Term Operational Area (I.TOA) Technical Memorandum within Appendix A because that report had been temporarily removed pending action on comments by the Base Realignment and Closure (BRAC) Cleanup Team (BCT) That action has been completed and the revised, final LTOA Technical Memorandum, including all changes made as a result of the comments, is enclosed herein

In addition, changes have been made to the Enhanced Bioremediation Treatment (EBT) Treatability Study Workplan, contained within Appendix B, subsequent to EPA approval as a result of comments made on the document by the Remedial Process Optimization (RPO) group. These comments were received on May 14, 2002. Rather than issuing a separate page for each required change as part of an errata sheet, the EBT Workplan incorporates these changes because the entire RD Workplan is being issued as an electronic document. The changes include

- 1 Page 4-1, Seventh bullet, Second sentence The word "Seven" has replaced the word "Six".
- 2. Page 7-1, Fourth paragraph, Last Sentence: The sentence read "Therefore, the mixture injected into the aquifer should not have less than 2 mg/L electron donor substrate." The sentence now reads: "Therefore, the minimum substrate concentration in groundwater after injection into the aquifer will not be less than 2 mg/L."
- 3 Table 6-1, Column entitled "Description", 4th item down The number "19 has replaced the number "28" and the number "7" has replaced the number "20".
- 4 Fable 6-2, In the "Matrix and Analytes" column, Under the Vegetable Oil, Lactate, and Tracer portion "VOCs" has replaced "TAL/ICL"
- 5 Table 6-2, In the "Method" column, Under the <u>Vegetable Oil, Lactate, and Tracer</u> portion: "8260B" has replaced "TAL/TCL".
- 6. Figure 2-4 has been revised as a result of comments made by the BCT on the potentiometric surface map contained within the LTOA Technical Memorandum.

All changes, except for No. 6, were supposed to have been made prior to submittal of the Rev 1 version of the document and the action here does not effect the efforts made in the field portion of the treatability study as they have already been acknowledged as part of the project plan.

1.0 Introduction

This Remedial Design (RD) Workplan for the Main Installation (MI) of the former Memphis Depot (Depot) in Memphis, Shelby County, Tennessee, has been prepared for the U.S. Army Corps of Engineers (USACE) – Huntsville Center as part of Task Order 13 under contract number DACA87-94-D-0009. This document is in accordance with the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA), as amended by the Superfund Amendments and Reauthorization Act (SARA), and to the extent applicable, the National Oil and Hazardous Pollution Contingency Plan (NCP). This workplan is also consistent with the Record of Decision (ROD) for the MI issued on September 7, 2001.

This document complies with CERCLA guidance on conducting an RD and has been submitted to satisfy the requirements outlined by the Base Realignment and Closure (BRAC) Act as well as requirements set forth by the BRAC Cleanup Team (BCT) for the Depot. The BCT, which is composed of representatives of the Defense Logistics Agency (DLA), Tennessee Department of Environment and Conservation (TDEC), and the U.S Environmental Protection Agency (EPA), will monitor the progress of the RD and will review all documents prior to issuance as a final document.

Subsequent to the signing the Final MI ROD and prior to the issuance of this RD Workplan, a Long-Term Operational Area (LTOA) investigation was conducted from September through December 2001 at the MI at the request of TDEC. The following information was included in the ROD to address the pre-design LTOA data collection activity:

"TDEC requested additional confirmation that no dense non-aqueous phase liquid (DNAPL) sources occur beneath historic long-term operational areas on the MI. There is no evidence from the [Remedial Investigation] RI and groundwater [Feasibility Study] FS that a DNAPL is present in the groundwater on the MI, however, the Depot and EPA agreed to complete this testing prior to beginning the remedial design. The pre-design tests will include drilling new soil borings and monitoring wells at selected locations within the MI and obtaining soil and groundwater samples for targeted laboratory analysis. The results of these pre-design tests are not expected to change the effectiveness of the selected remedy for groundwater; however if results of the pre-design tests indicate a significant or fundamental change to the remedy is warranted, then an Explanation of Significant Differences (ESD) or a ROD amendment would be required in accordance with CERCLA §117(c) and NCP §§300.435(c)(2)(i) and (ii)."

The results of the LTOA investigation, which are presented as Appendix A to this workplan, have been used to supplement the Enhanced Bioremediation Treatment (EBT) Treatability Study workplan That workplan is presented as Appendix B to this document and presents the requirements for the work to be conducted at the MI as part of the RD.

1.1 Purposes of RD Workplan

The purposes of the RD workplan are to:

- Describe the remedy selected for the MI as stated within the ROD;
- Present the RD/Remedial Action (RA) objectives for the MI;
- Present the RD tasks along with a schedule for accomplishing each task; and
- Identify major deliverables and their submittal dates.

1.2 Organization of RD Workplan

This RD workplan is organized as follows:

Section 2	Site Description
Section 3	Remedial Design Tasks
Section 4	Remedial Design Schedule
Section 5	Project Management Plan
Section 6	References
Appendix A	LTOA Technical Memorandum
Appendix B	MI EBT Treatability Study Workplan
Appendix C	August 1995 Final Generic Quality Assurance Project Plan
• •	(amended)

2.0 Site Description

2.1 Site Name, Location, and Description

The Memphis Depot (Depot) is a former military supply facility that closed in September 1997 under the BRAC Act. The Depot is located in southeastern Memphis, Tennessee (Figure 2-1), approximately 5 miles east of the Mississippi River and just northeast of Interstate 240. The Depot includes two components: the MI, which is the focus of this workplan, and Dunn Field. Airways Boulevard borders the Depot on the east and provides primary access to the site. Dunn Avenue, Ball Road, and Perry Road form the northern, southern, and western boundaries of the MI, respectively. At the time of closure, the Depot included approximately 118 buildings, 26 miles of railroad track, and 28 miles of paved streets, the majority of which lie within the MI. The facility includes approximately 5.5 million square feet (ft²) of covered storage space and approximately 6 million ft² of open space.

For the purposes of completing the remedial investigation (RI) and feasibility study (FS), while complying with BRAC requirements, the term "Functional Unit" (FU) was established to identify groups of sites on the MI based on operational history, expected use, location, and generally uniform human health exposure. The FUs are a refinement of the "Operable Unit" (OU) designation and are based on common past and anticipated future use of the land on the MI. The MI is divided into six FUs. A seventh FU is the groundwater beneath the MI. The FUs are defined in Table 2-1 and shown graphically on Figure 2-2. The ROD for the MI addressed FUs 1 through 7. The lead agency for site activities at the Depot is the DLA. The regulatory oversight agencies are EPA and TDEC. DLA will implement the selected response actions and will incur all associated costs. The Depot has an EPA Identification Number listed as TN4210020570.

2.2 Site History and Enforcement Activities

Starting in the 1940s, the Depot received, warehoused, and distributed supplies common to all U.S. military services and some civil agencies. Activities at the MI included storing and shipping various materials (e.g., food, clothing, medical supplies) and industrial supplies (e.g., hazardous materials) Several commonly used hazardous materials were also used for facility maintenance. Hazardous materials which were used or stored at the Depot during its operational period include flammables, solvents, petroleum/oil/lubricants (POL), paints, pesticides, herbicides, wood treating products, oxidizers, corrosives, and reactives.

Types of past activities that led to the presence of hazardous materials in the environmental media at the facility included pesticide application, painting and sandblasting, vehicle maintenance, and hazardous material handling/storage. Other historical activities in open and enclosed storage areas included storing transformers with polychlorinated biphenyls (PCBs), storing and using pesticides/herbicides, and treating wood products with pentachlorophenol (PCP). These industrial activities (e.g., sandblasting of lead-based paints,

application of pesticides, use of hazardous materials) resulted in the presence of metals, pesticides, and other less frequently detected chemicals in surface soil, surface water, and sediment above background concentrations.

Important dates for the Depot as part of the cleanup process for these chemicals are as follows:

- From 1989 through 1990, Law Environmental through a contract with the U.S. Army Engineering and Support Center (USAESCH) conducted an RI at the Depot.
- In January 1990, EPA Region 4 conducted a Resource Conservation and Recovery Act (RCRA) Facility Assessment (RFA) at the facility through a contract with A.T. Kearney, Inc. (EPA, 1990).
- On September 28, 1990, the Depot was issued a RCRA Part B permit (No. TN4 210-020-570) by EPA Region 4 and TDEC. Subsequently, in accordance with Section 120(d)(2) of CERCLA, Title 42, Section 9620(d)(2) of CERCLA, and Title 42, Section 9620(d) (2) of the United States Code (USC), EPA prepared a final Hazard Ranking System (HRS) Scoring Package for the facility. On the basis of the final HRS score of 58.06, EPA added the Depot to the National Priorities List (NPL) by publication in the Federal Register (FR), 57 FR 47180 No. 199, on October 14, 1992.
- On March 6, 1995, a Federal Facilities Agreement (FFA) under CERCLA, Section 120, and RCRA, Sections 3008(h), and 3004(u) and (v), was reached by EPA, TDEC, and the Depot. The FFA identified a list of sites for investigation. Table 2-2 of the MI ROD presents these sites. The FFA also outlined the terms under which the investigation and cleanup will be conducted. The selected remedy addresses all concerns related to these sites.
- In July 1995, the Depot was identified for closure under the BRAC process, which requires environmental restoration at the Depot to comply with requirements for property transfer under Public Law 101-510 of Title XXIX, Defense Base Closure and Realignment. After the Depot was placed on the BRAC closure list, the City of Memphis and County of Shelby established the Memphis Depot Redevelopment Agency, now the Depot Redevelopment Corporation (DRC), to plan and coordinate the reuse of the Depot. The DRC conducted several public meetings during the preparation of its Memphis Depot Redevelopment Plan to obtain community feedback on future land use plans. The Memphis Depot Redevelopment Plan was approved in 1997.
- From 1995 through 2000, the Depot conducted an RI/FS under EPA, TDEC, and DLA oversight. The RI workplans were prepared in 1995 (and amended in 1998), and the RI report was finalized in January 2000. Separate FS reports were prepared for the soils and groundwater on the MI. Both FS reports were finalized in July 2000. The Proposed Plan for the MI was finalized in August 2000.

In addition, a number of interim remedial actions (IRAs) were conducted at the MI. These IRAs included removal of soils containing pesticides, PCBs and PCP surrounding the MI Housing Area, cafeteria (Building 274), and PCP dip vat area (Building 737), respectively. The removal of surface soils containing elevated metals and polynuclear aromatic hydro

carbons (PAHs) near the southwest corner of the MI (FU3) was completed in August 2000. IRAs that have been performed at the MI are detailed below.

- Approximately 602 cy³ of surface and subsurface soil was removed from the PCP dip vat area in FU4 (Building 737) because of elevated levels of PCP (completed in 1985).
- Approximately 5,000 tons or 3,700 cy³ of surface soil in the Housing Area of FU6 was removed because of the presence of dieldrin (began in June 1998; completed in October 1998) The soil was disposed at a RCRA-permitted Subtitle D landfill. The Housing Area is an exception to the overall industrial land use for MI and is acceptable for residential reuse
- Approximately 530 tons or 400 cy³ of surface soil surrounding the cafeteria (Building 274) in FU6 was removed because of elevated levels of PCBs (began in October 1998; completed in November 1998). The soil was disposed at a RCRA-permitted Subtitle D landfill.
- Approximately 980 cy³ of surface and subsurface soil from near Buildings 1084, 1085, 1087, 1088, 1089 and 1090 was removed because of elevated levels of metals and PAHs (began in May 2000, completed in August 2000). The soil was disposed at a RCRApermitted Subtitle D landfill.

In addition to these IRAs, one other remedial action (RA) was accomplished in July and August 2001. Approximately 300 cy³ of surface soil was excavated near Building 949 in FU4 because of elevated levels of lead. The removal included contaminated surface soils where lead concentrations were equal to or greater than 1,536 milligrams per kilogram (mg/kg) and were disposed of at a RCRA-approved off-site landfill. Following excavation of the contaminated soil, clean backfill was placed in all areas excavated, and the entire area was restored to pre-RA conditions. To accomplish the removal, the DLA exercised its removal authority under CERCLA Section 104, as delegated in Executive Order 12580, and removed the lead-contaminated soil after development of, but before final execution of, the ROD. Both EPA and TDEC agreed that the action was an appropriate part of a final, protective remedy, regardless of the timing of the action and the CERCLA authority under which it was performed. This remedial action is documented in the final Remediation Report, Removal Action at Building 949, dated February 15, 2002.

2.3 Planned Response Actions at the MI

The ROD detailed several RAs to achieve acceptable residual risk levels and allow for the planned industrial and recreational land use for the MI. These include:

• Restrict (1) future residential land use (except for the existing Housing Area in FU6) in FUs 1 through 6, (2) day care operations in FUs 1 through 6, and (3) casual access to FU2 from adjacent off-site residents through land use controls. It should be noted that FU6 consists of BRAC Parcels 1, 2, 4, and 5. In 1998, surface soil in the Housing Area of FU6, BRAC Parcel 2, was removed because of the presence of dieldrin. The Housing Area is the only portion of the MI that may be used for future residential purposes, according to the DRC's Memphis Depot Redevelopment Plan. As such, it has been restored to meet the risk criteria for both industrial and residential use. Analytical results from soil samples.

collected in the open area around Building 144 and the north and south paved parking lots within BRAC Parcel 1 also indicated contaminant levels that are not inconsistent with unrestricted use. The remainder of FU6 is safe for industrial use but not suitable for future residential use. Land use controls will be placed on these areas to prevent future residential use and day care operations, etc.

- Prevent future groundwater use on the MI while concentrations of chemicals of concern (COCs) are above maximum contaminant levels (MCLs).
- Reduce to MCLs the concentrations of COCs in groundwater within the entire plume both on- and offsite of the MI.
- Conduct 5-year reviews of the RA according to Section 121(c) of CERCLA and NCP §300.430(f)(5)(111)(C) if there are any hazardous substances, pollutants, or contaminants remaining at the site above levels that would allow for unlimited use and unrestricted exposure. The review will be conducted no less often than every 5 years after the initiation of such RA to assure that human health and the environment are being protected by the RA being implemented.

In addition to the RAs developed within the ROD, a Long-Term Monitoring (LTM) Plan will be developed for both groundwater and land use controls at the MI. The LTM for groundwater is further described in Section 2.5.2.1. The land use controls LTM plan will be completed through a through a land use controls implementation plan (LUCIP), as described in Section 2.5.1.1.

2.4 RD/RA Objectives

Remedial action objectives (RAOs) are medium-specific goals that the RAs are expected to accomplish to protect human health and the environment. They guide the formulation and evaluation of remedial alternatives. RAOs have been developed to reflect the anticipated future land use for the MI in accordance with EPA Policy, Land Use in the CERCLA Remedy Selection Process (OSWER Directive No. 9355.7-04).

The groundwater RAOs are expected to prevent ingestion of water contaminated with volatile organic compounds (VOCs) in excess of MCLs from potential future onsite wells; restore groundwater to levels at or less than MCLs; and prevent horizontal and vertical offsite migration of groundwater contaminants in excess of MCLs. The MCLs for trichloroethene (TCE) (5 micrograms per liter [μ g/L]) and tetrachloroethene (PCE) (5 μ g/L) are the relevant and appropriate requirements for groundwater beneath the MI.

The surface soil RAO for protection of future on-site residents is to prevent direct contact/ingestion of surface soils contaminated with dieldrin and arsenic in excess of human health risk assessment (HHRA) criteria for residents and to prevent direct contact/ingestion of surface soils contaminated with lead in excess of risk-based criteria for protection of residential children.

The RAOs will reduce the excess lifetime cancer risk (ELCR) and hazard index (HI) associated with exposure to contaminated soil to acceptable levels for future workers and will prevent future residential development of the site. This will be achieved by reducing

the exposure concentration of lead to the target cleanup level of 1,536 mg/kg (calculated using blood-lead uptake models) and by imposing land use restrictions. As discussed in Section 2.2, the reduction of lead to the target cleanup level has been accomplished with removal of soil from the Building 949 area.

Because there are no federal or state clean-up standards for soil contamination, these clean-up standards were established on the basis of the HHRA. Targets were selected that will (1) reduce the risk associated with exposure to soil contaminants to an acceptable level and (2) restrict the migration of contaminants into the groundwater.

2.5 Remedies Selected for the MI

The selected surface soil and groundwater remedies as identified in the final ROD for the MI are discussed below.

2.5.1 Surface Soil

2.5.1.1 Land Use Controls

Land use controls will leave contaminated surface soil in place, but will provide deed restrictions, in addition to the existing land use controls, thereby limiting exposure by defining the future use of the MI.

Deed (including lease) restrictions will restrict residential land use in FU1 through FU6 (exclusive of Parcels 1 and 2 in FU6 which are available for unrestricted use) where dieldrin, arsenic, and/or lead in the surface soil pose an unacceptable risk for such use. Residential use controls will include preventing day care operations in all FUs. In addition, a boundary fence surrounding FU2 will be maintained to preclude casual access by adjacent off-site residents.

Restrictions and controls will be coordinated with the Depot reuse implementation plans, and will be included in all deeds and leases. The deed restrictions and site controls, in addition to the existing land use controls, to be applied are as follows:

FU	Deed Restrictions Preventing Residential Land Use *	Site Controls
1	×	
2	×	Χp
3	×	
4	×	
5	x	
6	X °	

^{*} Includes day care restriction.

Land use controls selected in the ROD (excluding Parcels 1 and 2 of FU6) will:

Maintaining a boundary fence surrounding FU2 to preclude casual access by adjacent off-site residents

^{*}Deed restrictions do not ably to Parcels 1 and 2 of FU6

- Prevent future residential land use in FUs 1 through 6, thus eliminating the risks associated with that land use scenario.
- Prevent casual access by adjacent off-site residents through maintenance of a boundary fence surrounding FU2.
- Prevent day care operations in FU1 through 6.

Applying land use controls will result in the following in each FU (excluding Parcels 1 and 2 of FU6):

- FUs 1, 3, 4, 5, and 6 are acceptable for industrial use. Land use controls to prevent residential development are the only remedial action needed to address unacceptable risk in surface soils at FU 1, 3, 4, 5, and 6.
- FU2 is acceptable for recreational use. With land use controls in place to prevent future residential development, and to prevent casual access by adjacent off-site residents through maintenance of a boundary fence, FU2 can be used for recreational purposes. In addition, according to Section 24 of the Memphis and Shelby County zoning regulations, single-family and multi-family residential uses are prohibited. Also, under the Federal Property Management Regulations, FU2 is slated for transfer from the Department of Defense (DoD), specifically the Army, to the Department of Interior/National Park Service (DOI/NPS). It will then be transferred by public benefit conveyance to the City of Memphis for use as a park. According to 41 CFR 101-47.308-7, property for use as a public park or recreational area must be used and maintained for the purpose for which it was conveyed in perpetuity, or be returned to the United States (24 CFR 51D).

Land use controls are part of the selected remedy for the MI, and will be implemented through a land use controls implementation plan (LUCIP). The LUCIP is being developed as part of the MI RD by the DLA and the Army. The timing and nature of the monitoring and reporting for the land use controls shall be specified in the LUCIP. However, to remain protective, land use controls depend on annual monitoring, as well as maintenance of site controls. The results of the annual evaluation shall be reported to TDEC and EPA. The deed restrictions will add a layer of protection against future residential use that will augment current zoning restrictions.

2.5.1.2 Excavation and Off-site Disposal

As described in Section 2 2 of this document, this RA has been accomplished with acceptance from EPA, TDEC, and the DLA.

2.5.2 Groundwater

2.5.2.1 Enhanced Bioremediation

This RA uses injection of nutrients to enhance the natural biodegradation processes. The remedy will accelerate biodegradation in the most contaminated parts of the plume Untreated parts of the plume will degrade as a result of natural attenuation processes. In the absence of pilot test data, a conservative assumption was made that the nutrients will triple the biodegradation rate within the aquifer, and the duration of the remedial action was

assumed to be 10 years. Therefore, enhanced bioremediation must also include land use controls and groundwater monitoring.

Preliminary design components will include the following:

- Nutrient injection into the fluvial aquifer will be conducted via borings or wells
 Treatment zones will be established in the most contaminated parts of the plume within
 the MI. Treatability studies will be required to determine injection volumes, spacing,
 and depth. Nutrient re-injection will occur at intervals determined by pilot tests and
 monitoring results.
- Deed restrictions will prohibit the installation and use of production and consumptive use wells and drilling into aquifers below the fluvial aquifer until cleanup levels are achieved. The deed restrictions will also guarantee access to contingency areas, all injection, boundary, sentinel, and monitoring wells for the life of the remedy. These restrictions might be removed at the completion of the remedy. An annual evaluation will be conducted in accordance with the LUCIP to verify that land use controls and deed restrictions are in effect and to ensure that land use changes that may pose an unacceptable risk to the users have not occurred. The LUCIP is being developed as part of the RD by the DLA and the Army.
- A network of groundwater wells will be monitored at a frequency that will be
 determined during the RD; however, monitoring will be no less than annual for the first
 5 years. Well locations will be chosen during the RD with the following guidelines:
 - Wells inside the groundwater plumes to measure the effect of enhanced bioremediation and natural attenuation. Water samples will be analyzed for VOCs as well as degradation products.
 - Boundary wells to detect potential migration of a plume to the MI boundary. Water samples will be analyzed for VOCs.
 - Sentinel wells to detect potential migration of a plume into the deeper intermediate aquifer. Water samples will be analyzed for VOCs.
- Monitoring well maintenance (cleaning, wellhead repairs) will be performed as needed.
- Annual summaries of monitoring data will be produced to document the site conditions and progress of the remedy.
- Groundwater concentrations will meet MCLs in all monitoring wells for four
 consecutive monitoring periods to demonstrate completion of the remedy. The sampling
 schedule will therefore be subject to change in response to observed trends and
 variability.
- Contingency provisions will ensure that if groundwater contamination exceeds MCLs at the boundary wells or the sentinel wells, more active measures for plume control will be implemented.
- Without detailed information regarding the magnitude of MCL exceedances at boundary or sentinel wells in the future, development of a detailed contingency plan is

not possible. Rather, should it be determined that the selected RA is not achieving RAOs and an alternative remediation strategy is warranted, a detailed contingency plan would be completed at that time. The contingency plan would evaluate the existing site data and evaluate alternatives that could be implemented to achieve RAOs. The contingency plan would be reviewed by stakeholders, commented upon, and revised as necessary for the purpose of finalizing the revised remedy. The public notification and remedy modification phases of work would then be completed to document the revised remedy. Finally, the revised remedy would be designed and then implemented. The time between identifying the need for an alternative remedy and implementation of the revised remediation strategy is estimated at 8 to 12 months, provided funding is available.

Groundwater sampling conducted as part of the LTOA pre-design data collection activities have identified additional areas of groundwater contamination on the MI, and higher concentrations of VOCs from those detected during the RI/FS (see Appendix A). The EBT Treatability Study (see Appendix B) and RD will be adjusted to address this new information; however, the results of the pre-design tests don't indicate a significant or fundamental change to the remedy nor is the effectiveness of the selected remedy for groundwater expected to change.

3.0 Remedial Design Tasks

This section presents the approach for the RD and a description of the RD tasks. As described in Section 2.5, the remedies selected for surface soil have been executed prior to completion of the ROD or will be implemented through completion of the LUCIP document. The Memphis Depot will implement the tasks described herein to develop the RD for the Alternative GW3 remedy.

After the RD workplan and the EBT Treatability Study are completed, the RD will begin with the intermediate design, which will include the draft drawings and specifications, design analysis, construction needs, operation and maintenance (O&M) requirements, initial RA component cost estimate, and a Performance Standards Verification Plan. The intermediate design will represent the 60 percent completion of the design effort. The Rev. 0 EBT Treatability Study report will be submitted along with the intermediate design to the BCT. A value engineering analysis will be performed for the intermediate design. The results of the analysis will be presented in the intermediate design submittal.

The prefinal design will represent the 90 percent completion point of the design effort. The prefinal design submittal will include a complete design analysis, the final drawings and basis of design specifications, prefinal construction schedule, and revised construction cost estimate. BCT comments on the prefinal design will be addressed in the final design.

Table 3-1 provides a complete list of the tasks to be performed, information needed for each task, results expected from each task, and a description of the work products that will be submitted to the BCT.

3.1 Task I – Project Planning

This task includes gathering existing information about the site and determining if additional data are needed to support the RD process

3.1.1 Site Background

Section 2.0 discussed the current regulatory status of the MI as described in the September 2001 ROD. The presentation of this material included information from the MI RI and FS. This task has been completed.

3.1.2 Project Planning

Planning activities prior to initiating the development of the MI RD Workplan included completion of the MI ROD and the November and December 2001 BCT meetings in Memphis and Atlanta, respectively. The BCT meetings included discussions of the schedule of activities for the RD as well as discussion of additional data needs for the RD. The additional data needs are based upon review of data in the MI RI/FS documents and comparison of these data to data requirements described in the EBT Treatability Study workplan.

3.1.2.1 Documentation of Additional Data Requirements

Groundwater samples were collected from monitoring wells installed at the MI in 1996, 1997, and 1998. The 1998 event included sampling of groundwater in existing and newly installed wells and push points from both on- and offsite locations. In 2000, a Monitored Natural Attenuation Study was conducted across the Memphis Depot to define the efficacy of natural attenuation as a remedy within the fluvial aquifer that underlies the area. During this study, geochemical parameters were collected from a specific number of monitoring wells. Since the last groundwater sampling event at the MI, 5 additional monitoring wells were installed to support the CSM and 17 additional monitoring wells were installed as part of the LTOA investigation.

Review of the existing groundwater data indicates that sampling events have not occurred consistently and have only included monitoring wells that were existing at that time (i.e., not comprehensive sampling events). In addition, during comprehensive sampling events, not all wells were sampled. There has not been a recent site-wide sampling event that involves all on- and offsite monitoring wells and sample analysis for VOC and geochemical parameter content. The BCT has therefore decided to include a baseline groundwater sampling event as part of the RD process, except for those recently (December 2001) installed and sampled as part of the LTOA investigation. The data from the baseline event, which was conducted during the week of March 18 through 22, 2002, will be used to: (1) establish monitoring well locations for the EBT Treatability Study; (2) provide up-to-date VOC contaminant concentration data for the fluvial aquifer; (3) provide up-to-date geochemical parameter data for the fluvial aquifer; and (4) define the quantity of nutrient source needed to enhance reductive dechlorination within the fluvial aquifer. In addition, the data from the baseline sampling event will be reviewed along with existing groundwater sample analytical data for the MI to define those wells that will be required for long-term monitoring purposes

The methods used to sample on- and offsite monitoring wells, as well as the analytical methods to be used for VOC and geochemical parameters, are described in the Baseline Groundwater Sampling Plan for Main Installation Monitoring Wells This document was given approval for action by the BCT members during the December 2001 meeting and is included as an Appendix A to the EBT Treatability Study Workplan, which is Appendix B to this document

3.2 Task II - Remedial Design

The RD will be implemented in accordance with standard professional engineering and construction practices using currently accepted environmental protection technologies. Work products of the RD are described below.

3.2.1 Remedial Design Planning

The RD will require additional data in the form of a baseline groundwater sampling event and an EBT Treatability Study. To provide these data, additional sampling and the treatability study will be conducted based on the RD workplan as the governing document for directing this work. The baseline event field effort was conducted from March 18 through 22, 2002. In addition, the EBT Treatability Study workplan for the MI has been developed

and is submitted with this document as Appendix B. In addition, the MI Generic Health and Safety Plan (HASP) has been completely revised to include those tasks pertinent to this RD The MI Generic Quality Assurance Project Plan (QAPP) has also been internally revised to include amendments completed as required for additional data collection activities during the RI and a compendium has been added to describe these changes.

3.2.2 Preparation of the RD Workplan

This document provides information on the additional site work and the steps required to develop the RD. The workplan is based upon CERCLA guidance as well as the Federal Facility Agreement. Other resources include the *RD/RA Handbook* from the EPA Office of Emergency and Remedial Response (June 1995). Before work is conducted, the RD workplan and the EBT Treatability Study workplan will be approved by the BCT. The RD workplan will be used to prepare the intermediate, prefinal, and final RD documents.

3.2.3 Preparation of the EBT Treatability Study Workplan

EBT was selected as the groundwater remedy in the MI ROD, which outlined the requirements for a treatability study of this remedy. The treatability study workplan is included as Appendix B.

The EBT Treatability Study will assess the natural biodegradability of site-specific chemicals (specifically CVOCs) in groundwater underlying the site in response to the injection of nutrients. The nutrients will accelerate biodegradation in the most contaminated parts of the aquifer. The nutrients will typically consist of a carbon source such as vegetable oil or lactic acid. Other commercially available sources exist, including Hydrogen Releasing Compounds or HRC® from Regensis®. As described in Appendix B, the study focuses on the use of vegetable oil and lactic acid.

3.2.4 Intermediate Design

The intermediate design, submitted to the BCT when the design effort is 60 percent complete, will consist of information presented as the draft design analysis, draft drawings and specifications, draft construction schedule, operation and maintenance (O&M) requirements, initial RA component cost estimate, and a draft Performance Standards Verification Plan A value engineering analysis will be performed for the intermediate design. The results of the analysis will be presented in the intermediate design submittal.

The design analysis will include evaluations conducted to establish the design criteria for each remedy component in sufficient detail to provide the basis for the design approach and subsequent design decisions and production activities. Where necessary, supporting design calculations will be included in the intermediate design submittal.

Draft construction drawings and technical specifications for the remedy components will be prepared and submitted. Specifications may include but not be limited to specifications for construction, installation, site preparation, and field work standards. Specifications will conform to USACE ETL 1006, *Technical Requirements for Pre-design and Design Submittals*. The intermediate design will also include a draft construction schedule for the RA. The schedule will include project milestones, estimated activity duration, estimated task completion dates, and critical path tasks.

The intermediate design will also include a draft O&M plan for facilities, equipment, or and remedial methods outlined in the RD documents. The plan will include all activities that require routine maintenance, as well as a draft schedule of these activities. In addition to the O&M plan, an initial RA cost estimate will be presented. The cost estimate will include, as necessary, operating labor, maintenance material and labor, component costs, materials and energy, purchased services, and administrative costs. The cost estimate at this point will be accurate to within plus 40 percent and minus 20 percent.

A Performance Standards Verification Plan will be developed and submitted in the intermediate design. The plan will include the following:

- The Performance Standards Verification Sampling and Analysis Plan, which provides guidance for field work by defining sampling and data gathering methods to be used.
- The Performance Standards Verification Quality Assurance/Quality Control Project Plan, which describes the quality assurance and quality control protocols to be followed in demonstrating compliance with performance standards.
- A schedule for tasks to be performed to demonstrate compliance with performance standards. The schedule will also include implementation activities for the Land Use Controls as part of the overall RA.

In addition, the LUCIP, which is part of the RD, shall be submitted during the design development process in accordance with the Memphis Depot Master Schedule, so that it will be ready for approval not later than the approval date for the pre-final/final RD.

3.2.5 Prefinal/Final Design

The prefinal design, submitted to the BCT when the design effort is 90 percent complete, will consist of information presented in the complete design analysis, prefinal drawings and specifications, prefinal construction schedule, prefinal O&M plan, and a prefinal RA component cost estimate. After review by the BCT, the prefinal design will be modified to address review comments, and the modified design will be the final design. The final design submittal will include a memorandum that will describe how the prefinal design comments have been incorporated into the final design.

All completed design calculations and analyses of design criteria will be presented in support of the selected design approach. Construction drawings and technical specifications will be submitted in final form in the prefinal design along with a prefinal construction schedule, O&M plan, and cost estimate. The final construction schedule will be reviewed with Jacobs Engineering, Inc. (Jacobs), the RA contractor for the Memphis Depot. The cost estimate will also be reviewed with Jacobs, and will be within plus 15 to minus 10 percent of the construction costs associated with implementation of the RD.

4.0 Remedial Design Schedule

This section presents the RD schedule (Figure 4-1), which includes the following:

- RD tasks as described in this document;
- Start and end dates, the duration, and the predecessors(s) for each task;
- Project milestones, including submittal dates for each deliverable
- Duration of BCT review for each deliverable; and
- Critical path for the RD.

The dates for submittal of deliverables are presented in Table 4-1.

The RD consists of five major components:

- Review of site-specific data to define the procedures for the baseline groundwater sampling event required for the RD;
- Baseline groundwater sampling event,
- EBT Treatability Study to evaluate the effectiveness of the selected groundwater remedy;
- LUCIP development and completion; and
- Intermediate and prefinal and final designs.

5.0 Project Management Plan

This section presents the project organization for the RD, including key personnel and their responsibilities, a project communications matrix, a data management plan, and the reporting requirements.

5.1 Project Organization and Communication

The MI RD project team includes the BCT members (DLA, EPA and TDEC), USACE-Huntsville, CH2M HILL, USACE-Mobile, and the RAC contractor, Jacobs. CH2M HILL is developing the RD as specified in the contract with USACE-Huntsville. USACE-Huntsville, which is under contract to the DLA, will review and approve all RD material before submittal to the BCT. After approval by the BCT, USACE-Huntsville and CH2M HILL will coordinate with USACE-Mobile and their contractor, Jacobs, for implementation of the RD.

Key personnel involved in the MI RD are presented in Figure 5-1. Mr. Turpin Ballard of EPA Region IV, Mr. Jim Morrison of TDEC, and Mr. John De Back of the DLA are the BCT members. Mr. Clyde Hunt is the Remedial Program Manager for DLA for the Memphis Depot project and has responsibility as a BCT member in the absence of Mr. De Back.

Mr. Bruce Railey is the Project Manager for the Memphis Depot project at USACE-Huntsville. He is responsible for coordinating with DLA and BCT members as well as with the contractor for the Memphis Depot project, CH2M HILL

Mr. David Nelson, P.G., is the CH2M HILL Project Manager for the MI RD. He is the primary CH2M HILL contact and is responsible for overall management of the RD phase of the project.

Messrs. Steve Offner, P.G., Mike Harris, P.E., and Tom Simpkin, P.E. of CH2M HILL are involved in the Memphis Depot project as the USACE-Huntsville/Memphis Depot Program Manager, Senior Consultant, and Technical Advisor, respectively. They will participate in the RD phase in these same roles but will also lend their experience and knowledge of the Memphis Depot project to the RD development. Mr. Offner has been involved on the Memphis Depot project since 1997 in various roles and has been involved in several phases of this project beginning with the RI stage. Mr. Harris will also serve as the CH2M HILL Technical Manager for design and will be responsible for approval of project-related designs. Mr. Simpkin has extensive experience with enhanced bioremediation projects and the use of carbon sources to spur bioremediation of groundwater.

Figure 5-2 presents a project communications matrix for the MI RD. The matrix identifies communications and reporting relationships.

5.2 Data Management Plan

The CH2M HILL Data Management Plan describes procedures that will be used to document and track investigation data and results. The plan includes the following.

- Data quality objectives (DQOs), documentation and processing procedures;
- Project-related progress reporting procedures; and
- Project file requirements.

Implementation of the procedures described herein will ensure proper documentation and retrieval of data and results.

5.2.1 Data Quality Objectives, Documentation and Processing Procedures

During the pre-design baseline sampling event and the EBT Treatability Study, groundwater sampling analytical data will be collected. This subsection presents documentation and processing procedures for the data

5.2.1.1 Field Data

All sampling procedures will be noted within field logbooks according to the SAP for this effort. Geochemical parameter measurements will also be noted in the field logbooks. The information in the field logbooks will be used as a backup for data quality evaluation as well as a primary source for geochemical parameters.

5.2.1.2 Laboratory Data

Laboratory analytical data will be collected during the pre-design effort and will be handled according to procedures described in Sections 7, 8, and 9 in the Memphis Depot Generic QAPP (Appendix C). The data will be reviewed and processed through data quality procedures, as described in Section 8 of the QAPP (Appendix C).

5.2.1.3 Investigation Results

The results of the pre-design baseline sampling effort will be presented in a brief document entitled Results of RD Baseline Sampling Event, which will be presented to the BCT for review and approval. The data will be used to select final locations for the injection and monitoring points for the EBT Treatability Study.

5.2.2 Project File Requirements

This project will require the administration of a central project file. The data and records management protocols will provide adequate controls and retention of all materials related to the project. Record control will include receipt from external sources, transmittals, transfer to storage, and indication of record status. Record retention will include receipt at storage areas, indexing, filing, storage, maintenance, and retrieval

5.2.2.1 Record Control

Incoming materials related to the project will be forwarded to the CH2M HILL Project Manager or a designee. These documents will be placed in the project file. Project personnel will work from a copy of necessary documents. Records shall be legible and easily identifiable.

Examples of records that will be maintained in the project file are as follows:

- Field documents
- Authorizations:

- Correspondence
- Logs;
- Photographs;
- Drawings and sketches;
- Specifications;
- Reports; and
- Procurement agreements.

Outgoing project correspondence and reports will be reviewed and signed by the CH2M HILL Project Manager or his designee.

5.2.2.2 Record Status

The CH2M HILL Project Manager will inform the organizations involved in the RD about revisions to records. Revisions to records shall be subject to the same level of review and approval as the original document. The revised document will be distributed to all holders of the original document and discussed with project personnel. Outdated records will be marked "void." In addition, the date a document is marked "void" will be recorded.

Documents will be distributed to the BCT in various formats, including use of Adobe Acrobat software to convert documents to .pdf format. These re-formatted documents will be either posted on the Memphis Depot File Transfer Protocol website that CH2M HILL supports or issued to BCT members as compact discs.

5.2.2.3 Record Storage

Project-related information will be maintained by CH2M HILL Designated personnel will assure that incoming records are legible and are in suitable condition for storage.

Record storage will be performed in two stages. Storage will occur during and immediately following the project and permanent storage of records directly related to the project.

All records designated for permanent storage by CH2M HILL will be placed into suitable containers with appropriate project identification labeling and stored in a facility with an environment that will prevent deterioration, damage, and loss. Material from the project file may include reports, drawings, QA documents, verifications records, electronic files, and software program documentation. The DLA maintains a separate records inventory known as an Information Repository (IR)

5.3 Reporting Requirements

Major submittals for this RD will include this RD workplan, the EBT Treatability Study Workplan, the LTOA Technical Memorandum, the Intermediate Design, and the Prefinal/Final Design Table 5-1 presents the MI RD submittals to all stakeholders including number of copies per each submittal.

Tables

Table 2-1 Description of Functional Units at the MI Rev 1 MI RD Workplan

FU No.	Name	Size (acres)	Common Past Land Use	Description
1	Twenty Typical Warehouses	89	Transportation to and storage in closed warehouses	Located in the northeastern area of the Mi, consisting of about 20 large warehouses, with interspersed roadways and railroad tracks
2	Southeast Golf Course/ Recreational Area	53	Golf, other recreation	Located in the southeastern comer of the MI1, consisting of golf course (Parcel 3). This FU also includes a baseball field and a small playground in the southeastern comer. This FU includes two constructed ponds and two concrete-lined drainage ditches from the ponds leading to the off-site area.
3	Southwest Open Area	92	Transportation to and storage in open-sided warehouses, painting and sandblasting, open storage	Located in the southwestern corner of the MI, consisting of varied type of parcels and sites
4	Northern and Open Areas	193	Open storage, and transportation to and storage in closed warehouses	Located in the north-central to northwest area of the MI, covering a large area
5	Newer Warehouses	109	Transportation to and storage in closed warehouses	Located in the south-central area of the MI and includes 10 large warehouse buildings
6	Administrative and Residential Areas	33	Offices, equipment storage and maintenance, on-base housing	Located along the property boundary of the Depot along the Airways Boulevard. This FU includes the old Residential Unit Area, parking lots, and other asphalt-paved areas.

Table 3-1 List of RD Tasks

Task	Activities	Information Required/Source	Work Product			
Task I – Project Pla	nning					
Site Background	Gather previously collected data and documentation for additional data	MI RI/FS documents, LTOA data	Preliminary information to be included within the RD workplan			
Project Planning	Review items and steps for collecting additional data	MI RI/FS documents, LTOA dala	Prehminary information to be included within the RD workplan			
Task II – Remedial	Design	<u> </u>	<u> </u>			
Remedial Design Planning	Preparation of the RD workplan (includes Rev 0 LTOA Tech Memo and EBT Treatability Study Workplan with Baseline Sampling Plan)	MI RI/FS, ROD documents	RD Workplan			
	Describe test(s) to be conducted at site, test and data quality objectives, procedures, data management	MI RI/FS, ROD documents	EBT Treatability Study Workplan			
EBT Treatability Stud	Revise MI Generic Health and Safety Plan (HASP), Sampling and Analysis Plan (SAP) and Quality Assurance Project Plan (QAPP) with addenda, as necessary	MI RI/FS, ROD, MI Generic HASP, SAP, and QAPP documents	Revisions to be included as part of effort for EBT Treatability Study Workplan			
	EBT Treatability Study at the MI	EBT Treatability Study Workplan	EBT Treatability Study Technical Memorandum			
	Present data from treatability study and evaluation of design approach					
	Develop draft drawings and specifications	Listing of drawings and specifications	MI Intermediate RD document			
Intermediate Design	Operation and maintenance plan and component cost estimate	Design parameters, ROD	(will include Rev 0 EBT Treatability Study Tech			
•	Develop draft construction schedule	Schedule of construction activities from RD workplan	Memo and Rev 1 LTOA			
	Develop LUCIP	Review LUCAP and MI ROD				
	Performance Standards Venfication Plan	Design parameters, ROD				
	Prepare design approach based on BCT comments received from EPA	Intermediate RD document and comments				
	Develop final drawings and specifications	· · · · · · · · · · · · · · · · · · ·	Prefinal/Final RD document (will include Rev. 1 EBT			
Prefinal/Final Design	Develop final construction schedule	Lizaπ construction schedule	Treatability Study Tech Memo and Rev 1 LTOA Tech Memo)			
	Develop construction cost estimate	Results of EBT Treatability Study, additional site investigation, and vendor contractor cost estimates				

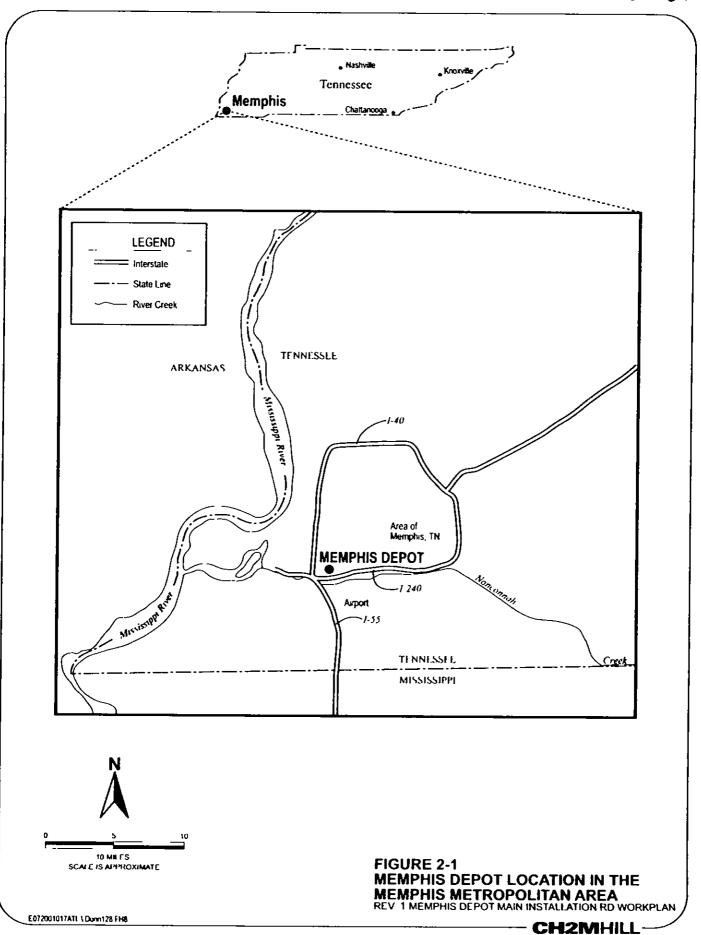
Table 4-1 MI RD Deliverable Submittal Dates Rev 1 Memphis Depot MI RD Workplan

Deliverable	Projected Submittal Date
MI RD Workplan	
Rev. 0 MI RD Workplan with Rev. 0 LTOA Technical Memorandum and Rev 0 EBT Treatability Study Workplan	January 14, 2002
Rev. 1 MI RD Workplan with and Rev. 1 EBT Treatability Study Workplan	April 14, 2002
Rev 2 MI RD Workplan with Rev. 1 LTOA Technical Memorandum and Rev. 1 EBT Treatability Study Workplan	July 12, 2002
LUCIP	
Rev. 0 Land Use Control and Implementation Plan	July 29, 2002
Rev. 1 Land Use Control and Implementation Plan	January 25, 2003
Rev. 2 Land Use Control and Implementation Plan	March 3, 2003
Intermediate (60%) Design	
Rev 0 Intermediate (60%) RD Report	March 3, 2003
Prefinal (90%) Design	
Rev. 1 Prefinal (90%) RD Report	August 30, 2003
Final (100%) Design	
Rev. 2 Final (100%) RD Report	October 14, 2003

Table 5-1 MI RD Deliverables Rev 1 Memphis Depot MI RD Workplan

Deliverable	Copy Requirement
Task I - Project Planning	
Baseline Groundwater Sampling Event	3 copies to DLA, 3 copies to USACE- Huntsville, 3 copies to EPA, 2 copies to TDEC
Task II - Remedial Design	
Rev 0 RD Work Plan, includes Rev 0 EBT Treatability Study and Rev 0 LTOA Technical Memorandum	3 copies to DLA, 3 copies to USACE- Huntsville, 3 copies to EPA, 2 copies to TDEC
Rev 1 RD Work Plan, includes Rev 1 EBT Treatability Study and Rev 1 LTOA Technical Memorandum	3 copies to DLA, 3 copies to USACE- Huntsville, 3 copies to EPA, 2 copies to TDEC
Rev 2 RD Work Plan, includes Rev. 2 EBT Treatability Study and Rev 1 LTOA Technical Memorandum	6 copies to DLA, 3 copies to USACE- Huntsville, 3 copies to EPA, 2 copies to TDEC
Intermediate (60%) Design	
Results of EBT Treatability Study	
Draft Design Analysis	3 copies to DLA, 3 copies to USACE-
Draft Drawings and Specifications	Huntsville, 3 copies to EPA, 2 copies to TDEC,
Draft Construction Schedule	2 copies to USACE-Mobile and Jacobs (4
O&M Requirements	copies will be provided for the Information
Rev 1 LUCIP	Repositories [IR])
Performance Standards Verification Plan	
Prefinal (90%)/Final (100%) Design	**
Design Analysis	6 copies to DLA, 3 copies to USACE- Huntsville, 3 copies to EPA, 3 copies to TDEC,
Prefinal/Final Drawings and Specifications	2 consected UCACE Making and James (00
Prefinal/Final Construction Schedule	format for RAB members) Final RD document distribution will include 4 copies for the IR and
Prefinal/Final O&M Plan	20 copies in CD ROM format for RAB members

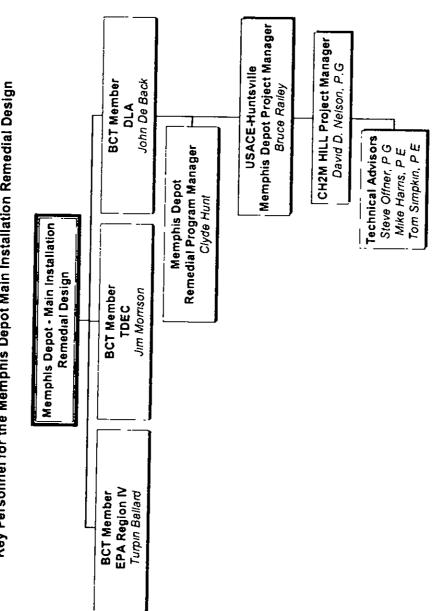
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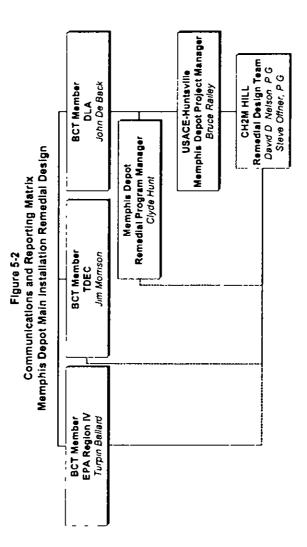


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inpins Depot Mail	Start	Mon 03/03/03	Sat 11/30/02	59(11/30(0)	Fi 12/2000	May 01/20/00	Mon-012763	Man 020303	F4101/31/01	Sun 020203	May 03.03.03	Tue colosco	Sar OSOSIOS	Fri 06/08/93	FH (05/09/03)	Worn OBSSECTS	FH (05/01/03)	Mon:07/14/03	Mon Offit Alto	Sat 00/30/01	Tue 09:02:00	Mon opizalos	Mon 09/29/03	Tue 101403		
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Figure 5-1 Key Personnel for the Memphis Depot Main Installation Remedial Design





Informal Communications Reporting

TAB

Appendix A

Appendix A – Rev. 1 LTOA Technical Memorandum

Evaluation of Soil and Groundwater Data Collected from Long-Term Operational Areas (LTOAs), Main Installation, Memphis Depot

TO:

US Army Engineering and Support Center, Huntsville

COPIES:

Defense Distribution Center (Memphis)

U.S. Environmental Protection Agency (USEPA), Region 4

Tennessee Department of Environment and Conservation (TDEC)

FROM:

CH2M HILL

DATE:

July 3, 2002

Introduction

The Data Collection Plan for Long-Term Operational Areas (LTOAs), Main Installation, Memphis Depot (June 5, 2001) and the addendum Well Construction and Sampling Techniques for Long-Term Operational Area (LTOA) Monitoring Wells Associated with SS42/SS43, NE6 (Building T702), and SS80 (September 5, 2001) were prepared to describe pre-Remedial Design (RD) sampling and testing conducted at the Main Installation (MI) within the Memphis Depot (Figure 1). The primary objective for the activities described within the Data Collection Plan (DCP) was to evaluate groundwater downgradient of known or suspected historical LTOAs on the MI where hazardous materials were used/stored, as identified by the TDEC. The LTOAs were selected by TDEC for further testing because groundwater monitoring wells were not installed down-gradient of these sites during the MI Remedial Investigation (RI).

In addition to collecting data on LTOAs, the pre-RD sampling enabled collection of information to be used in optimizing the location of injection wells for the selected remedial alternative for groundwater on the MI, enhanced bioremediation. Also, the data collected during the LTOA investigation has supplemented existing hydrogeologic and environmental data regarding the conceptual site model (CSM) for the MI.

This technical memorandum is in compliance with requirements specified in Delivery Order (DO) 13 of Contract No DACA87-94-D-0009. Under this delivery order, CH2M HILL provides architectural/engineering services for the United States Army Corps of Engineers (USACE) – Huntsville Center. Jacobs Engineering Group, Inc. (Jacobs), which is the remedial action contractor for the USACE - Mobile District (Contract No. DACA01-99-0040), was tasked by Defense Logistics Agency (DLA) with completing field activities and data collection associated with the LTOA DCP. CH2M HILL's role was to provide general oversight of Jacobs' field activities and assure compliance with the approved LTOA DCP, and complete the Technical Memorandum documenting the results of the data collection effort.

Background Information

In January 2000, the final MI RI report was submitted and in July 2000, the final MI Groundwater Feasibility Study (FS) was submitted. Differences between CSMs and implications regarding potential plume migration led the Memphis Depot Base Realignment and Closure (BRAC) Base Cleanup Team (BCT) to re-evaluate groundwater results from the RI and to request additional testing prior to beginning RD.

TDEC provided proposed well locations in August 2000 in areas identified as being LTOAs of hazardous materials at the MI, and revised these in October 2000, after discussions with all stakeholders in September 2000. The approach taken by TDEC was to review the many "sites" on the MI and determine if they were LTOAs of hazardous materials, and if there was an existing groundwater monitoring well located near or downgradient from them

After the BCT discussed the importance and purpose of each of these well locations on August 23, 2000, a memorandum of understanding was developed on September 21, 2000 by the members of the BCT regarding locations where LTOA wells were to be installed. The following excerpt from the agreement summarizes the scope of work:

"At LTOA proposal well locations for the following sites: SS66, RI58, RI59, SS37, SS36, SS35, SS83, RI27, SS80, RI34

BCT consensus is -

We will use temporary wells at these locations. Groundwater sample [sic] will be collected with the diffusion samplers at a frequency of one per 5 feet of screened intervals. The entire saturated thickness will be screened. [This portion of the plan has changed since consensus was reached, as discussed in the "Groundwater Sampling" section below].

150-[micrograms per liter] µg/L total VOCs will be the trigger for completing a well [All wells will now be installed as finished wells]. Phase 2 design (Post [Record of Decision] [ROD]) will be to delineate the plume boundary for purposes of implementing enhanced bioremediation.

If a potential source of ground water contamination is identified in the vadose zone during drilling, a well will be completed. [Each well is to be a finished well.]

If new wells change the vertical or horizontal groundwater flow picture materially, but no contamination is found exiting the base boundary or downward towards a lower aquifer, the information would focus the placement of sentinel wells, but the current proposed remedy will still be valid."

In addition to investigation areas described in the previous paragraph, another five LTOAs on the MI were proposed for potential investigation in a letter from TDEC to the Memphis Depot Caretaker on October 30, 2000. Per an e-mail issued to the BCT on November 1, 2000 from the Memphis Depot Caretaker, the investigation into five additional LTOAs was implemented as requested. As described in the October 30, 2000 letter, the five areas are as follows:

- Building T702(NE6)
- Garage and Paint Shop, Building 260

- Automotive Maintenance and Repair Shop, Building 251 (SB1)
- Automotive Maintenance and Repair Shop, Building 265 (SC1)
- Former Drum Storage Area on the south boundary of facility

The MI ROD was signed by DLA, TDEC and EPA, and finalized in September 2001. The following information was included in the ROD to address this pre-design data collection activity:

"TDEC requested additional confirmation that no dense non-aqueous phase liquid (DNAPL) sources occur beneath historic long-term operational areas on the MI. There is no evidence from the RI and groundwater FS that a DNAPL is present in the groundwater on the MI; however, the Depot and EPA agreed to complete this testing prior to beginning the remedial design. The pre-design tests will include drilling new soil borings and monitoring wells at selected locations within the MI and obtaining soil and groundwater samples for targeted laboratory analysis. The results of these pre-design tests are not expected to change the effectiveness of the selected remedy for groundwater; however if results of the pre-design tests indicate a significant or fundamental change to the remedy is warranted, then an Explanation of Significant Differences (ESD) or a ROD amendment would be required in accordance with CERCLA §117(c) and NCP §§300.435(c)(2)(i) and (ii)."

The above referenced ESD or ROD amendment would be developed only if the data obtained from the LTOA investigation indicated the groundwater remedy selected in the MI ROD required a significant and fundamental change.

Pre-RD Sampling and Testing Justification

The RI identified several groundwater plumes of chlorinated volatile organic compounds (CVOCs) beneath the MI, but did not identify specific contaminant sources in either soil or groundwater. Numerous soil borings were completed in potential CVOC source areas, and 24 monitoring wells (along with 7 piezometers and 7 hydropunch locations) were installed to test groundwater across and offsite of the MI. Many potential source areas were not specifically targeted for groundwater monitoring, because chemical analyses of surface and subsurface soil from test borings indicated little or no residual volatile organic compound (VOC) contamination. During the RI, the principal contaminants identified in monitoring wells were PCE and TCE, and associated degradation products.

Results of a re-evaluation of the RI testing by TDEC suggested that some sites may remain as a source-term (e.g., dense non-aqueous phase liquids [DNAPL] or elevated concentrations of contaminants) for groundwater contamination. The presence of an undocumented source-term would have serious implications for design and implementation of the selected MI groundwater remedy, as documented in the MI ROD. Therefore, as part of the LTOA DCP, soil and groundwater samples were collected from the LTOA locations to confirm the presence or absence of a source-term.

Long-Term Operational Areas

The following table presents the LTOA locations and site description (Figure 2):

LTOA Group Number	LTOA Site or Area	Functional Unit	LTOA Description
1	SS35	FU4	Former DRMO Bldg T-308, Hazardous Waste Storage
	SS36	FU4	Former DRMO Hazardous Waste Concrete Storage Pad
	SS37	FU4	Former DRMO Hazardous Waste Gravel Storage Pad
2	RI59	FU2	Former pesticide mixing area (Bldg. 273) located near the northeast corner of the inactive Golf Course.
	RI58	FU6	Old pesticide shop (Pad 267) located directly north of the J-Street Café. Monitoring Well MW-26 is located directly down-gradient of this LTOA
	SS66	FU6	Former vehicle maintenance shop (Bldg, 253) Located directly north of site RI58
!	B260	FU6	Former garage and paint shop (Bldg. 260). Located directly northeast of site RI58
	SB1	FU6	Former auto maintenance and repair shop SB1 (Bldg. 251) Located directly northeast of B260
	SC1	FU6	Former auto maintenance and repair shop SC1 (Bldg 265). Located directly southeast of B260
3	SS78	FU5	Former Alcohol, Acetone, Toluene, Naptha, Hydrofluonc Acid Spill (Bldg 678)
4	RI34	FU3	Former Underground Oil Storage Tanks (Bldg 770)
5	RI27	FU3	Former Recoupment Area (Bldg 873)
6	RI32	FU3	Former Painting, Sandblasting, and Waste Accumulation (Bldg. 1087 & 1088)
	SS89	FU3	Former storage of acids, paints, and cleaning solvents (Bldg 1089)
7	SS83	FU4	Dned Paint Disposal Area (Bldg. 949)
8	SS42	FU4	Former PCP Dip Vat Area
	SS43	FU4	Former Underground PCP Tank Area
	\$\$80	FU4	Former Fuel and Cleaners Dispensing (Bldg 720)
9	Bldg. 690	FU5	Former Drum Storage Area on the south boundary of the MI
10	Bldg. T702 (NE6)	FU4	Officer's Hobby Shop (former Bldg T702 – razed in 1998) [identified as a former paint shop in the U.S. Army Topographic Engineering Center Historical Environmental Aerial Photographic Analysis, dated September 1998]

Objectives of the LTOA Data Collection Plan

The objectives of the DCP were to complete the following steps and collect the resulting information and data:

- Install monitoring wells within the fluvial aquifer or underlying sand units (within the Jackson Formation/Upper Claiborne Group) within 100 to 200 feet down-gradient of the identified LTOAs to determine if an LTOA is acting as a source-term for chlorinated hydrocarbons in the groundwater.
- Collect samples of soil and groundwater at each of the monitoring well locations to define contaminant levels in both matrices
- Collect hydrogeological data during the LTOA investigation to supplement existing hydrogeologic and environmental data regarding the CSM for the MI. Specifically, the investigation provides additional data to: (1) confirm groundwater flow directions in the fluvial aquifer and the intermediate aquifer underlying the MI; (2) define the perimeter or boundary of the 'limited to no flow boundary' of the fluvial aquifer on the northnorthwest/central portion of the MI; and (3) define the areal extent of the fluvial aquifer and underlying clay unit on the north-northwest/central portion of the MI.

Scope of Work

The scope of work for the LTOA investigation has been outlined in several documents and communications, beginning primarily with the issuance of the *Draft Pre-Design Data Collection Plan for Main Installation (Functional Unit 7)* (CH2M HILL, 2000). This document was developed as a result of the BRAC BCT meeting on July 19, 2000

The scope of work for the LTOA activities is based in part on the following:

- Minutes from the August 23, 2000, BCT meeting regarding BCT review of the Draft Pre-Design Data Collection Plan for Main Installation (Functional Unit 7)
- Letter from TDEC, dated September 12, 2000, regarding conditional concurrence on Memphis Depot, MI Proposed Plan
- Letter from TDEC, dated September 13, 2000, regarding Memphis Depot, MI Groundwater FS and MI Soils FS
- Agreement between BCT Members for the MI pre-design resolution, dated September 21, 2000
- Letter from TDEC, dated October 30, 2000, regarding additional MI Pre-RD wells
- Minutes from the January 18, 2001, BCT meeting regarding LTOA wells
- Data Collection Plan for LTOAs, Main Installation, Memphis Depot, dated June 5, 2001
- Well Construction and Sampling Techniques for LTOA Monitoring Wells Associated with SS42/SS43, NE6 (Building T702), and SS80, dated September 5, 2001

The DCP and the September 5, 2001 addendum was approved by the EPA and TDEC on October 3, 2001, as part of the RD process for the MI remedial action (RA).

The final scope of work included:

- Drilling of 19 soil borings and the installation/development of 19 groundwater monitoring wells in the soil borings;
- Collection of soil samples from the 19 borings for field screening and laboratory analyses;
- Collection of groundwater samples from the 17 newly installed monitoring wells for laboratory analyses;
- Measurement of water level elevations in all monitoring wells and piezometers at the Depot
- Development of a Technical Memorandum documenting the results of the LTOA investigation, to be included in the Remedial Design Work Plan for the MI.

Investigative Methodology

The field activities described in this section were conducted at the LTOA sites on the MI. Field activities began on September 17, 2001, and continued through December 21, 2001.

Soil Boring Installation and Soil Sampling

Nineteen soil borings were drilled to define local soil conditions, stratigraphy, and collect samples of groundwater quality (Figure 2). Fourteen of these soil borings, MW-85, -86, -88, -92, -93, -94, -96, -97, -98, -99, -100, -102, -103, and -104, were completed using hollow-stem auger drilling techniques (Tri-State Testing Services, Inc., from Memphis, Tennessee); the five remaining borings, SB-105 and -106, and MW-101, -107, and -108, were completed using rotasonic drilling techniques (Prosonic Corp , from Marietta, Ohio).

Soil borings drilled using hollow-stem auger drilling techniques utilized a 5-ft continuous core sampler advanced with the augers. Core samples were collected in clear, 4-inch diameter hard plastic sleeves placed within the core barrel prior to drilling and capped on each end immediately upon return to ground surface. The five borings drilled using rotasonic drilling techniques utilized clear, flexible plastic sleeves at 10 to 20 foot intervals for sample collection. Continuous sampling was conducted at each boring location from land surface to termination depth.

Soil samples for headspace field screening were collected from each boring at a frequency of one per every five feet from land surface to the groundwater interface. The headspace in each sample was analyzed using an organic vapor analyzer (OVA) equipped with a flame ionization detector (FID). Duplicate headspace samples were also collected and analyzed with an activated carbon filter to correct for methane concentrations. One soil sample was collected every 20 feet from soil associated with the highest OVA-FID concentration greater than or equal to 20 ppm. If no OVA-FID concentrations were greater than or equal to 20 ppm, a single soil sample was collected from the boring at a depth of just above the groundwater interface and sent to the laboratory for chemical analysis. Soil samples were collected for VOC analyses via SW-846 Method 8260B at a fixed-based laboratory. A portion of each sample was placed into corresponding pre-weighed 40-ml vials preserved with

sodium bisulfate and methanol, and sent to the laboratory for extraction using EPA SW-846 Method 5035.

Eight additional soil samples were chosen at random based on field observations from monitoring wells MW-85, -86, -92, -96, -99, -101, -103, and -104. The basis for collecting these samples was the occurrence of perched water conditions associated with clay units less than 5 feet thick

Soil samples collected from 17 of the 19 borings were submitted to an analytical laboratory for subsequent VOC analysis. Soil samples collected from borings SB-105 and MW-108, which were associated with the former PCP Dip Vat (SS42/SS43), were analyzed for semi-volatile organic compounds (SVOCs) via SW-846 Method 8270C, with pentachlorophenol (PCP) being the target analyte. Since SVOCs are not detected using standard headspace field screening techniques, discrete soil samples were collected at each sand/clay interface where vertical percolation may be impeded. At SB-105, which was located within the footprint of the former PCP Dip Vat, composite soil samples were collected. Each composite sample consisted of an aliquot from each 1-foot interval over a 20-foot section of the boring, beginning at 10 feet bgs and terminating at the top of the clay interface, 99.5-feet bgs. Each of the composite samples were analyzed for leachable SVOCs (including PCP) via the synthetic precipitation leaching procedure (SPLP) (SW-846 Methods 1312/8270C).

Split soil samples from SB-105 were collected for TDEC on October 15, 2001. Three discrete soil samples were duplicated (SB-105-83, SB-105-92, and SB-105-97) and 10 composite samples were collected every 10 feet specifically for TDEC, beginning at 10 feet bgs and terminating at 107 feet bgs. The samples were collected in appropriate sample containers, labeled with the sample identifications, and placed on ice. Custody of the soil samples was transferred to TDEC on October 16, 2001.

During the drilling of 17 of 19 soil borings, soil samples were also collected for total organic carbon (TOC) analysis (SW-846 Method 9060) within the saturated portion of the borings.

Altogether, twenty-eight (28) soil samples were collected for laboratory VOC analysis using SW-846 Method 8260B. These 28 samples were analyzed by Columbia Analytical Services (CAS) in Redding, California. In addition, six samples were collected for total SVOC analysis (using SW-846 Method 8270C), five samples were collected for SPLP/SVOC leachability (using SW-846 Methods 1312/8270C), and 18 samples were collected for TOC analysis (using SW-846 Method 9060). This group of 29 samples was analyzed by Environmental Testing & Consulting, Inc., in Memphis, Tennessee. Quality Assurance/Quality Control (QA/QC) samples consisted of six sample duplicates, two equipment blanks, and eleven trip blanks (Attachment 5). Sample identifications are presented in Table 1.

Monitoring Well Installation

Seventeen LTOA soil borings with an aquifer thickness greater than 2 feet were completed as monitoring wells (Figure 2). No significant saturated thickness was found at the termination depth of borings SB-105 and -106; therefore, well casing was not installed in the borings. Soil boring logs and well completion diagrams are included in Attachments 1 and 2, respectively. Well construction details are summarized in Table 2. Each monitoring well was installed using 2-inch ID polyvinyl chloride (PVC) casing and 0 01-inch slotted PVC

screen in 5 and 10 foot sections, as necessary. No more than 20 feet of saturated thickness was screened in a well installed in the fluvial aquifer. Total length of the screened interval depended upon the saturated thickness of the aquifer. Aquifer thickness was based on field review of soil samples and, where possible, through the use of an electronic water-level tape. Screens were placed at the top of the first "clay layer" noted at the contact with the fluvial deposits; "clay layer" was defined as a unit greater than 5 feet thick and composed of clay, silty clay, or sandy clay. After the soil borings were completed into a clay layer, the bottom of the boring was plugged with bentonite pellets up to the corresponding depth of the top of the clay layer, screen and casing were then installed.

The length of the screened interval in wells MW-98, MW-101, MW-107, and MW-108, believed to be installed in the deeper intermediate aquifer of the Jackson Formation/Upper Claiborne Group, were defined in the field based on information provided by the BCT members. All monitoring wells were installed with continuous screened intervals, except for MW-101 and MW-107. These two wells were installed with multiple screened intervals based on field decisions by TDEC.

Each well was completed as a flush-mount with an 8-inch ID manhole set within a 3-foot by 3-foot by 0.5-foot concrete pad. In addition, for well-head protection pads located in high traffic areas, four bollards were placed at each corner of the concrete pad and painted with high-visibility yellow paint.

Following installation, all newly installed monitoring wells were developed in accordance with procedures presented in the Monitoring Well Installation section of the DCP. Development of multiple-screened monitoring wells required the use of an inflatable packer assembly system to isolate each screened interval.

Variations from the Defined Scope

All LTOA monitoring well locations are in accordance with the approved DCP and addendum. However, the following variances occurred in the field:

- While drilling MW-88 (SB1), the boring reached a competent clay unit at 97.5 feet bgs and was terminated at a depth of 102.5 feet bgs. The water column above the clay unit had a thickness of 17 feet; all criteria established in the DCP to install a monitoring well were accomplished. MW-88 was installed and developed in compliance with the DCP. Upon completing a base wide gauging event, the watertable at MW-88 was noticeably higher (approximately 18 feet) than other surrounding wells (i.e., MW-26, -85, -86, -92, and -96) in the immediate area. Based on the difference in water table elevation and the proximity of MW-88 to other monitoring wells (< 600 feet), the aquifer at MW-88 is considered to be perched.
- While drilling the soil boring for MW-98, which is associated with LTOA RI34, an aquifer thickness of approximately 44 feet was encountered. Within this portion of the MI, the fluvial aquifer was assumed to be 21 feet thick. As a result of this difference, BCT members and United States Geological Survey (USGS) were contacted from the field before the installation of the monitoring well. Based on the thickness of the aquifer and the depth to the top of the clay confining unit (147 feet bgs), BCT members and USGS agreed to install a monitoring well with 10 feet of screen set at the top of the clay unit All participants agreed a screen length greater than 10 feet would be affected by vertical

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hydraulic gradients if present in the aquifer. The BCT also discussed that the analytical results of the groundwater sample from well MW-98 would be reviewed to determine if an additional nested well would be needed at this location.

- Soil borings SB-105 (PCP dip vat) and SB-106 (Building T702/NE6) were terminated in a clay unit greater than 5 feet thick; no visual saturated conditions existed based on continuous soil cores. To confirm that an aquifer greater than 2 feet thick did not exist above the top of clay in either location, temporary wells were installed above the clay unit within both soil borings After approximately 15 hours had elapsed, water could not be detected in the well casing. BCT members were contacted via teleconference for each boring and a decision was made to remove the temporary wells and abandon the soil borings.
- During the teleconference for SB-105, BCT members also agreed to relocate the soil boring originally designated to be drilled immediately south of this LTOA. Based on the data from SB-105, this boring location was assumed to be to close to SB-105 and possibly may not have a sufficient aquifer thickness for monitoring purposes. Based on the available groundwater flow direction, the boring location was moved approximately 400 feet south of the PCP Dip Vat source area. TDEC was onsite for the relocation of the boring and agreed upon the location of the new soil boring. The new location is now MW-108.
- Drilling activities for MW-101 began on October 8, 2001 The hollow stem augers used to drill the boring could not be advanced past a depth of 133 feet bgs because of gravel layers and "flowing" sands within the saturated portion of the aquifer. A field decision was made by Jacobs and Tri-State Testing Services to use rotasonic drilling techniques to complete MW-101. Drilling activities using hollow-stem augers were stopped on October 10, 2001 and the boring for MW-101 was abandoned. Drilling by Prosonic Corp. on MW-101B, located approximately 50 feet north of MW-101, commenced on October 19, 2001 using rotasonic techniques. The top of the clay was reached at 133 feet bgs and the thickness of the aquifer was found to be approximately 43 feet. After reviewing the boring log and thickness measurements of the fluvial aquifer at that location, TDEC made a field decision to install three screens. The upper screen is 15 feet long, the middle 10 feet long, and lower 10 feet long, with each screen separated by five feet of riser pipe.
- During development activities, MW-100 and -102 were found to have occlusions at 40 and 50 feet, respectively Jacobs contacted Tri-State Testing Services and a downhole camera was brought on site. Upon review of the video logs, the PVC casing appeared to be melted and warped, possibly due to the heat created from the curing process of the grout. As a result, new monitoring wells, MW-100B and -102B, were installed on November 14, 2001 through November 16, 2001 to replace MW-100 and -102 The original MW-100 and -102 locations will be abandoned at a later date.

Groundwater Sampling

Collection of groundwater samples from the newly installed monitoring wells occurred after all wells were installed and developed. Each of the LTOA wells, except MW-101, MW-107, and MW-108, were sampled using 2-foot long diffusion bag samplers. Diffusion bag samplers allow for collection of discrete water samples and consist of polyethylene bags.

filled with distilled water. The concentration gradient between the VOCs in the well and the water-filled bag results in diffusion of contaminants into the sampler. Diffusion bag samplers were used continuously throughout the screened zone of each well per the requirements of TDEC. This method allowed for a more accurate representation of a potential contaminated horizon(s) compared to the use of a single diffusion bag sampler. Construction, installation, and sampling of diffusion bag samplers followed guidelines established in the *Groundwater Sampling* section of the DCP.

The semi-permeable membrane used for the diffusion bag samplers is engineered for VOC collection only. Therefore, diffusion bag samplers were not used for SVOC collection in monitoring well MW-108 at LTOA sites SS42-43 because of the historical use of PCP. Groundwater samples for SVOC analysis from MW-108 were collected using low-flow sampling procedures established in the *Groundwater Sampling* section of the DCP. Before sampling, MW-108 was purged using a bladder pump in order to minimize agitation of the groundwater. Field measurements of dissolved oxygen (DO), oxidation-reduction potential (ORP), turbidity, pH, temperature, and specific conductance were completed at predetermined intervals. These parameters were measured using an airtight flow-through cell. Purging continued until measurements indicated the parameters were stable according to the following standards: plus or minus 0.1 pH, plus or minus ten millivolts ORP, plus or minus 3 percent for specific conductance, and plus or minus 10 percent for turbidity and dissolved oxygen. After purging, MW-108 was sampled using the bladder pump system. The bladder pump was equipped with a high-density polyethylene (HDPE) tubing lined on the inside with Teflon®.

Monitoring wells MW-101 and -107 were completed with multiple screened intervals Therefore, groundwater samples from these wells were collected using a packer/submersible pump system that sealed each screened interval from other intervals; each interval was developed, purged, and sampled using low-flow sampling procedures.

All samples were preserved as required in the DCP and delivered to CAS within the appropriate holding period. Groundwater samples were analyzed using SW-846 Method 8260B or 8270C, as applicable.

In addition to groundwater samples, QA/QC samples were collected during the field effort. QA/QC samples included field duplicates, source-water blanks, equipment blanks, and trip blanks (Attachment 5).

Investigation Derived Waste

All soil cuttings were placed in roll-off boxes and staged onsite. After drilling activities were completed, representative soil samples were collected for characterization prior to disposal. The samples have been profiled and accepted for disposal as non-hazardous waste at the Tunica Landfill. Soil cuttings staged onsite were removed on January 11, 2002.

Development and purge water were containerized in poly tanks during field activities. Representative water samples were collected and analyzed for VOCs prior to off-site disposal. Analytical results for the IDW were within discharge permit requirements for the Dunn Field recovery system; therefore, approximately 3000 gallons of IDW were pumped into the Dunn Field disposal system.

Results

Potentiometric Surface Mapping

Ground-surface and top-of-casing elevations of the newly installed LTOA monitoring wells were surveyed to determine groundwater elevations within the wells. Depth-to-water measurements were collected from all monitoring wells, piezometers, and recovery wells associated with Memphis Depot on November 01, 2001 to the nearest ± 0.01 ft. Table 3 presents the depth-to-water measurements from this effort.

As discussed in the *Monitoring Well Installation* section above, the top of the water table at MW-88 was detected at a higher elevation than other wells in the immediate vicinity. Two potentiometric surface maps that include and exclude MW-88 are presented as Figures 3A and 3B, respectively. With MW-88 included, the groundwater gradient increases and the flow directions become radial downgradient of MW-88. Groundwater flow directions are not affected by MW-88 downgradient of MW-86. Due to the irregular flow pathways caused by MW-88, Figure 3A is considered to be more representative of the potentiometric surface within the fluvial aquifer underlying this portion of the MI.

Groundwater in the fluvial aquifer flows predominately toward the northeast portion of the MI from the southwest corner and also towards the southwest portion of the MI from the northeast corner; groundwater converges near the central, lower portion of the MI. The fluvial aquifer appears to be in direct contact with the lower confined aquifers in an area located within the north-northwest corner of the MI. This transition zone is surrounded by a 'no flow to limited flow' boundary and is 'open' to the fluvial aquifer toward the southeast near MW-63. Groundwater in the transition zone typically flows to the northwest. This boundary is created by the elevation of the confining clay that typically underlies the fluvial aquifer exceeding the groundwater elevation at these points. This boundary zone typically has no measurable aquifer thickness.

Site Hydrogeological Characterization

Seven geologic cross-sections (see Figures 4 through 10) and a top-of-clay map (see Figure 11) have been created from existing and LTOA soil boring log data

Soil boring logs and depth-to-water measurements from monitoring wells located in the northwest corner of the MI (i.e., MW-27, -55, -56, and -62) show a 'no flow to limited flow' boundary around an area where the confining clay underlying the fluvial deposits is discontinuous Previously, the boundary was believed to extend past MW-27/-89/-90 and MW-84/-36 locations. With the addition of soil borings SB-105 and -106, which showed no measurable water above the confining clay, the boundary was extended further southeast to include these locations

Cross-sections and top-of-clay maps presented in the MI and Dunn Field RI documents illustrated a continuous clay layer under the MI that dipped westward within the 'no flow to limited flow' boundary toward lower aquifers beginning at MW-63 and continuing to MW-34. This transition zone also appeared to be a window by which the fluvial aquifer was connected to the lower confined aquifers. In addition, based on the available depth-to-clay data, the area near MW-63 appeared to be the entrance by which groundwater entering the transition zone had to flow. With the addition of SB-105, SB-106, MW-107, and MW-108, the

connection between the fluvial aquifer and the intermediate aquifer appears to occur within a larger area.

Figure 7 shows an elongated clay layer located at SB-105 above a lower clay unit with sand separating the two units. Top-of-clay (147.18 and 133.25 feet mean sea level (MSL)) and water table (190.49 and 189.86 feet MSL) elevations at MW-107 and -108, which are positioned north and south of SB-105, suggest the two locations are connected hydrogeologically. Figure 9 adds further evidence to the interconnectivity of the fluvial aquifer with the intermediate aquifer. This cross-section transects the 'no flow to limited flow' boundary in the north-northwest corner to the southeast corner of the MI. The upper clay unit located at STB-8 and MW-27, -89, and -90 is also separated by sand from a lower clay unit located at MW-108. Evidence, such as the elevation of the bottom of the upper clay unit at MW-89 (192.5 feet MSL) being higher than the water table elevation at MW-108 (189.86 feet MSL), and the water table at MW-89 (185 37 feet MSL) being slightly lower than at MW-108, suggests the groundwater is flowing under the upper clay unit. Figure 11 also illustrates an elongated clay layer located at SB-105 above a lower clay unit dipping toward the west-southwest from MW-63 and -108; the upper clay unit connects to the lower clay unit toward the west. Therefore, the fluvial aquifer appears to be connected to the lower confined aquifers from MW-63 to -108

Top-of-clay elevations within the southwest corner were speculated to be relatively flat and gradually dip toward the center of the MI based on potentiometric surface maps and offsite soil boring logs generated for the MI RI. The addition of LTOA wells MW-97, -98, -99, -100, -101, and -102 changed the CSM for the top-of-clay in this region of the MI (Figure 11). Beginning at MW-100 and -101, the top-of-clay forms a trough with a gradual decrease in elevation to the northeast towards MW-108. The MW-108 location appears to have been placed within the deepest portion of the trough. Figures 5 through 7 present cross-sectional views of this trough. The trough does not appear to have a direct effect on groundwater flow pathways in the upper portion of the fluvial aquifer underlying the southwest corner of the MI.

Boring logs from the remaining monitoring wells installed in the northeast and southeast portions of the MI added critical lithological and hydrogeological information but did not change previous conceptual site models.

Soil

Soil samples were collected from each borehole as described in the Soil Boring and Soil Sampling Methodology section.

Volatile Organic Compounds

Twenty-eight soil samples were collected for laboratory analysis of VOCs (Table 1). Of those samples, only five soil samples had detectable concentrations of chlorinated hydrocarbons

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Monitoring Well	MW-86	MW-88	MW-92	MW-100	MW-101
Sample iD and depth of collection (ft bgs)	MW-86-78	MW-88-78	MW-92-96	MW-100-92.5	MW-101-994*
LTOA Site	Bldg. 260	SB1	SC1	SS89	RI32
CVOCs Detected (ug/l	(g)				-
Tetrachloroethene (PCE)	16	9	1.6 J	1.1 J	ND
Trichloroethene (TCE)	1.1 J	ND	ND	65J	ND
Cis-1,2-Dichloroethene (cis-1,2-DCE)	0.92 J	1.2 J	ND	ND	ND
1,2-Dichloroethane (1,2-DCA)	1.6 J	ND	ND	ND	3 J
Carbon Tetrachloride	8.5	1.3 J	ND	ND	ND
Chloroform	3.3 J	0.95 J	ND	ND	ND

MW-101-994 is a duplicate of MW-101-99; MW-101-99 did not have detectable chlorinated hydrocarbons.

Analytical results of soil samples from LTOA sites RI59/RI58/SS66/B260/SB1/SC1 and RI32/SS89 indicate soil contamination of chlorinated hydrocarbons above the watertable in the southeast and southwest corners of the MI. Previous sampling events indicate groundwater contamination of chlorinated hydrocarbons are associated with these LTOAs.

Since headspace field screening methods conducted during the LTOA investigation did not indicate contaminated soil from the ground surface to the water table, soil samples were only collected immediately above the water table. Therefore, chlorinated hydrocarbons detected in those soil samples are assumed to be caused by volatilization from the groundwater. PCE concentrations detected in soil samples from MW-86 and -88 are below the Region 9, soil screening level (Dilution Attenuation Factor [DAF] 20) of 60 ug/kg. MW-100 had a TCE concentration of 65J ug/kg, which is above the Region 9 soil screening level (DAF 20) of 60 ug/kg but below the Preliminary Remediation Goal (PRG) of 2,800 ug/kg for residential soil and 6,100 ug/kg for industrial soil. Other VOCs detected in the soil samples include acetone, bromoform, 2-butanone, methlyene chloride, and toluene, these constituents were all reported as estimated concentrations. Analytical results for all detected VOCs are located in Attachment 3.

Semi-volatile Organic Compounds

Six soil samples were collected from SB-105 and MW-108 for laboratory analysis of total SVOCs (Table 1). Bis(2-ethylhexyl)phthalate was detected in 5 of 6 samples at concentrations ranging from 225 to 377 ug/kg. According to CAS, Bis(2-ethylhexyl)phthalate is a common constituent associated with sampling gloves. Bis(2-ethylhexyl)phthalate concentrations are

ND Below analytical detection limits.

J: Estimated concentration

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well below the Region 9 PRG of 35,000 ug/kg for residential soil and 180,000 ug/kg for industrial soil. No other SVOCs were detected, including PCP.

Five composite soil samples were collected from SB-105 at the suspected source area (PCP dip vat) for SPLP SVOCs with PCP being the target analyte. According to OHM (1986), the soil at the location of SB-105 was excavated to a depth of 10 feet and replaced by clean soil. Therefore, composite soil sampling began at a depth of 10 feet and proceeded every 20 feet to a depth of 99.5 feet. Only the composite soil sample from 10 to 30 feet bgs had detectable concentrations of PCP (0 003J mg/L). All other samples did not contain PCP and other chlorophenols above laboratory detection limits. SVOC laboratory results for soil samples are located in Attachment 3.

Total Organic Carbon

Eighteen TOC soil samples were collected below the water table within the soil borings (Table 4) MW-86 had a TOC sample collected from a perched water-bearing zone (86 feet bgs) in addition to a sample taken from the fluvial aquifer (105 feet bgs).

Soil samples from MW-85 through MW-96 (9 samples total) were submitted to the laboratory as a group for TOC analysis. Results for this group of samples did not reveal TOC above laboratory detection limits (100 mg/kg). CH2M HILL contacted the laboratory to determine if any discrepancies in the data existed. According to the laboratory, the TOC samples were analyzed correctly.

Of those samples where TOC was revealed, concentrations ranged from <100 to 670 mg/kg. The average TOC in the fluvial aquifer to the southeast is less than 100 mg/kg while the average TOC in the fluvial and intermediate aquifers to the north/southwest is 519 mg/kg. This TOC data will be included into the TOC data set for the MI and will be further evaluated in the RD/RA.

Groundwater

Groundwater samples were collected from each monitoring well as described in the *Groundwater Sampling* section.

Volatile Organic Compounds

A total of 113 groundwater samples were collected from 17 monitoring wells for laboratory analysis of VOCs. Table 5 presents a summary of these results. Of those samples, 107 were collected using diffusion bag samplers and six were collected using low-flow sampling techniques from the middle of the screened interval. Eight diffusion bag samplers were accidentally suspended above or partially within the water column in wells MW-85, -92, -93, and -94. Therefore, the analytical results from those bags have been rejected and are not included in the final data set

Within Table 5, analytical results for each individual diffusion bag and screened interval are shown along with average concentrations per monitoring well for each constituent. By using diffusion bags to sample discrete intervals within the water column, a better understanding of the movement of contaminants within the aquifer is obtained. This knowledge will be used to target zones of higher contaminant concentrations within the aquifer during remedial actions

The results were averaged for possible groundwater exposure scenarios as with risk assessments. Risks for exposure to contaminated groundwater are based on a per well average. Average concentrations of the COCs for each LTOA monitoring well are shown in Figure 12. Past sampling events associated with the MI RI have indicated PCE and TCE plumes located in the southwest and southeast corners of the MI. Results from the LTOA wells re-enforce the boundaries of those existing plumes albeit at higher concentrations than previously recognized.

Groundwater samples from LTOA monitoring wells in the southwest corner of the MI (i e., MW-97, -98, -99, -100, -101, and -102) revealed concentrations of several CVOCs (Table 5). PCE was detected in well MW-100 at an average concentration of 50 ug/L (min: 14 ug/L, max: 65 ug/L) and in MW-101 at an average concentration of 480 ug/L (min: 450 ug/L, max: 530 ug/L). The highest PCE concentration of 530 ug/L was detected in the upper screened interval (89 to 104 feet bgs) of MW-101. This PCE concentration is the highest detected to date within groundwater underlying the MI. TCE was detected in MW-100 at an average concentration of 79 ug/L (min: 44 ug/L, max. 98 ug/L) and in MW-101 at an average concentration of 0.9J ug/L (min: 0.8J ug/L, max: 1 0 ug/L). Cis 1,2-DCE was detected in MW-100 at an average concentration of 1.2 ug/L (min: 1.1 ug/L, max: 1.3 ug/L) and in MW-101 at an average concentration of 0.3J ug/L (min: 0.3J ug/L, max: 0.4J ug/L). Estimated concentrations of <1J ug/L were detected for a number of the other CVOCs of concern. Only TCE and chloroform was detected at estimated concentrations of <1J ug/L in the sample collected from MW-102.

Five additional monitoring wells (MW-85, MW-86, MW-88, MW-92 and MW-96) were installed in a downgradient position from LTOA Sites SS-66, SB-1, SC-1, RI-58 and -59. The saturated thickness of the fluvial aquifer was measured at approximately 11.5- to 19.5-feet The highest concentration of PCE was detected in well MW-86 at an average concentration of 198 ug/L (min. 18 ug/L, max: 280 ug/L) and in MW-92 at an average concentration of 150 ug/L (min: 130 ug/L, max: 160 ug/L). The highest TCE concentrations were detected in MW-85 at an average concentration of 23 ug/L (min: 20 ug/L, max: 26 ug/L) and in MW-86 at an average concentration of 20 ug/L (min. 5.2 ug/L, max: 25 ug/L). The highest cis-1,2-DCE concentrations were detected in MW-86 at an average concentration of 53 ug/L (min. 18 ug/L, max. 76 ug/L) and in MW-85 at an average concentration of 28 ug/L (min 25 ug/L, max. 30 ug/L). The highest concentrations of chloroform were detected in MW-86 at an average concentration of 77 ug/L (min: 34 ug/L, max: 98 ug/L) and in MW-85 at an average concentration of 64 ug/L (min: 61 ug/L, max. 67 ug/L). The highest concentrations of carbon tetrachloride were detected in MW-85 at an average concentration of 122 ug/L (min: 110 ug/L, max: 140 ug/L) and in MW-86 at an average concentration of 77 ug/L (min: 26 ug/L, max. 94 ug/L). 1,2-DCA was detected in MW-86 at an average concentration of 3.6 ug/L (min: 2.0 ug/L, max. 75 ug/L). MW-96 is the furthest well down-gradient of this group of LTOA sites The concentrations of PCE, TCE, cis 1,2-DCE, chloroform and carbon tetrachloride are well below the concentrations detailed above.

Two additional monitoring wells (MW-103 and -104) were installed in a downgradient position of LTOA Sites SS-35, -36 &-37. The saturated thickness of the fluvial aquifer was measured at approximately 20- to 27-feet and was encountered on the confining clay layer. PCE was not detected in either well; however, TCE was detected in MW-104 at an average concentration of 11 ug/L (min. 0.9J ug/L, max. 24 ug/L) and in MW-103 at an average concentration of 4 0 ug/L (min. 0.3J ug/L, max. 5.8 ug/L). Chloroform was detected in

MW-104 at an average concentration of 12 ug/L (min: 4.0 ug/L, max: 20 ug/L) and in MW-103 at an average concentration of 13 ug/L (min: 1.9 ug/L, max: 17 ug/L). Low level concentrations of cis 1,2-DCE, 1,1-DCE, 1,1-DCA, 1,2-DCA were also detected.

MW-107 and -108 are located in the transition zone between the fluvial and the intermediate aquifer. Groundwater samples from both of these monitoring wells have detectable concentrations of PCE (0 8J and 2 6 ug/L, respectively) and TCE (2.7 and 6.4 ug/L, respectively) Chloroform is also detected in both wells but the level of chloroform is more prominent in MW-108 at 6 4 ug/L. Groundwater contamination within MW-107 and -108 suggests contaminates could be reaching the lower confined aquifers via the transition zone.

Chlorinated hydrocarbon concentrations detected within samples from LTOA monitoring wells re-enforce existing plume maps with the exception of MW-103 and MW-104. Groundwater contaminants in this portion of the MI were previously unknown. For a complete summary of laboratory analytical results, refer to Attachment 4.

Semi-volatile Organic Compounds

One groundwater sample was collected for SVOC analysis from well MW-108 using low-flow sampling techniques. Analytical results show that no detectable concentrations of chlorophenols, specifically PCP, were detected in MW-108. Bis(2-ethylhexyl)phthalate (9J ug/L) and diethylphthalate (0.81J ug/L) were the only SVOC constituents detected in MW-108. The concentration of Bis(2-ethylhexyl)phthalate violates the EPA maximum contaminate level (MCL) of 6 ug/L but could be an artifact of field or laboratory contamination. MW-108 had Bis(2-ethylhexyl)phthalate concentrations detected in both soil and groundwater samples.

Summary and Conclusions

Conceptual Site Model

Important hydrogeological information was collected during the drilling of the LTOA monitoring wells on the MI.

- With the addition of the LTOA wells to the existing MI monitoring well network, the potentiometric surface of the fluvial aquifer and groundwater flow directions did not significantly change from previous conceptual models. However, based on the new data, flow directions within the fluvial aquifer in the center portion of the MI did change it now appears to be influenced by the connection between the fluvial and intermediate aquifers located in the Northwest quadrant of the MI.
- The areal extent of the vertical window to the lower intermediate/confined aquifers appears to be larger than previously hypothesized (in the vicinity of MW-63 to MW-108).
- The 'no flow to limited flow' boundary extends further to the southeast based on boring logs from SB-105 and -106.
- As shown in Figure 11, a trough is present from the MW-101 location northeast towards MW-108. The trough is underlain by the clay confining unit present throughout the MI

subsurface. The trough elevation and, subsequently, the top of the clay confining unit, gradually decreases towards MW-108 Although the clay confining unit surface is understood from a CSM perspective, there is some doubt as to the correlation of this unit between monitoring wells MW-62, -89, -90, -98, -99, -108, and soil boring SB-105, and whether there may be two separate clay units. Based on available lithologic and soil boring data, CH2M HILL assumes that the surface of the clay located at monitoring well MW-62 is correlative to the clay surface at well MW-108. One or more wells will be specified in the Remedial Design as either Long-Term Monitoring (LTM) network or CSM wells to alleviate the current data discrepancies regarding the stratigraphy of the clay confining unit. As part of the LTM or CSM program, these wells will be scheduled for installation first and a decision tree will be included in the RD package that provides direction as to which way to proceed based on the stratigraphic data from these wells (i.e., Does the clay dip downward to MW-108 from MW-62 or are there two separate units? Also, is groundwater flowing beneath the clay at MW-62 similar to what is seen at monitoring wells MW-27, -89, and -90?)

Groundwater Quality

LTOA Group 1 (LTOA Sites SS-35, -36 &-37)

Existing piezometer PZ-06 appears to be located down- and side-gradient to the LTOA sites and existing well MW-53 appears to be located side- and up-gradient of the LTOA sites. MW-53 was sampled 5 times for VOCs from 1996 through 1998. TCE is the only CVOC constituent that has ever been detected in this well at a concentration of 1J ug/L. PZ-06 was sampled in 1998 and no VOCs were reported as being detected.

The CVOC groundwater contamination detected downgradient of this group of LTOA sites in wells MW-103 and -104 is a new finding; however, the total VOC concentration is below 150 ug/L and the detected concentrations do not indicate the presence of a DNAPL or source-term. The RD will review this portion of the fluvial aquifer on the MI as a possible candidate for natural attenuation and long-term monitoring (LTM) during the RA.

LTOA Group 2 (LTOA Sites SS-66, SB-1, SC-1, RI-58 and -59)

The closest existing wells to this group of LTOA sites includes piezometer PZ-07 (located side-gradient to the LTOA sites) and MW-26 (located downgradient of the LTOA sites). MW-53 was sampled 6 times for VOCs from 1993 through 1998. The highest concentrations of CVOCs detected include PCE at 16 ug/L, TCE at 2J ug/L, chloroform at 1J ug/L, and carbon tetrachloride at 4J ug/L. PZ-07 was sampled in 1998; however, the sample was not analyzed for CVOCs. Existing well MW-25 is located further down-gradient from MW-26 (approximately 650-feet southwest) and was also sampled 6 times from 1993 through 1998. The highest concentrations of CVOCs detected included PCE at 11 ug/L and carbon tetrachloride at 2J ug/L. Existing well MW-64 is located approximately 900 feet directly west of the LTOA sites and was sampled 1 time for VOCs in 1998. The highest concentrations of CVOCs detected include PCE at 10 ug/L, TCE at 28 ug/L, 1,2-DCA at 1J ug/L, chloroform at 1J ug/L and carbon tetrachloride at 4J ug/L.

The higher concentrations of CVOCs detected in wells MW-85, MW-86 and MW-92 constitutes a new finding. Based on the available information, this area appears to be the source for the CVOCs historically found in MW-25 and MW-26, and perhaps for MW-64

However, the detected concentrations of CVOCs do not indicate the presence of a DNAPL or source-term. The RD will consider this portion of the fluvial aquifer on the MI for enhanced bioremediation during the RA

LTOA Group 3 (LTOA Site SS-78)

One monitoring well (MW-94) was installed in an inferred downgradient position of this LTOA site, based on available groundwater flow direction data. However, with the installation and collection of potentiometric surface data from the LTOA monitoring wells, groundwater appears to be flowing east/east-northeast instead of to the southeast. Therefore, MW-94 does not meet the primary objective of being downgradient of LTOA Site SS-78. To meet this objective, the BCT agreed to the installation of a monitoring well approximately 500 to 700 feet northeast of Site SS-78, as part of the LTM program during the RA. If the thickness of the fluvial aquifer at this location is found to be significant (i.e., greater than 15 feet), nested wells will be required at this location.

No CVOCs of concern were detected in the groundwater sample from well MW-94. Based on available groundwater analytical data for the MI, MW-94 appears to be located east of the eastern, leading edge of the PCE and TCE plumes on the southwestern portion of the MI. Based on its location, the RD may consider MW-94 as part of the LTM program for the RA.

LTOA Group 4 (LTOA Site Ri-34)

One monitoring well (MW-98) was installed in an inferred downgradient position of this LTOA site, based on available groundwater flow data. However, with the installation and collection of potentiometric surface data from the LTOA monitoring wells, groundwater appears to be flowing northeast instead of southeast. Therefore, MW-98 does not meet the primary objective of being downgradient of LTOA Site RI34. To meet the objective, the BCT decided that an additional monitoring well will be installed adjacent to MW-39, as part of the LTM program during the RA. Based on available groundwater potentiometric surface data MW-39 is assumed to be downgradient of LTOA Site RI34, but is screened across the water table with approximately 10 feet of the screened interval below the water table. MW-39 does not extend to the top of the confining clay unit and the aquifer is approximately 44 feet thick. Therefore, an additional monitoring well will be installed as part of the LTM program during the RA, with a screened interval positioned directly above the clay confining unit. MW-39 has been sampled 7 times from November 1993 through March 2000 with concentrations of PCE and TCE ranging from 2.4J-12 ug/L (average: 6.9 ug/L) and 3J-8J ug/L (average: 5.5 ug/L), respectively

MW-98 is located at the eastern, leading edge of the PCE plume originating from the southwestern portion of the MI. PCE was detected at an average concentration of 4.6 ug/L (min: 1.5 ug/L, max² 7.7 ug/L) and TCE was detected at an average concentration of 0.8J ug/L (min: 0.8J ug/L, max² 0.9J ug/L) Chloroform was detected at an average concentration of 0.2J ug/L (min² 0.2J ug/L, max: 0.3J ug/L) No other CVOCs of concern were detected. Based on the location of this well, the RD may consider this well as part of the LTM program during the RA.

LTOA Group 5 (LTOA Site RI-27)

One monitoring well (MW-97) was installed in a downgradient position of this LTOA site. This location appears to be located near the southeastern edge of the PCE and TCE plumes in the southwestern portion of the MI. The saturated thickness of the fluvial aquifer was measured at approximately 14.5-feet and was encountered on the confining clay layer documented as being at least 5.5-feet thick. No PCE, TCE or other CVOCs of concern were detected. Based on the location of this well, the RD may consider this well as part of the LTM program during the RA.

LTOA Group 6 (LTOA Sites RI-32 and SS-89)

Two additional monitoring wells (MW-100 and MW-101) were installed in a downgradient position of the LTOA sites. Well MW-102 was installed along the southern boundary of the MI, north of off-site well MW-47. The saturated thickness of the fluvial aquifer in this location was measured at approximately 35 feet.

The closest existing wells to this group of LTOA sites includes MW-21 (located up-gradient to the LTOA Sites SS-89) and MW-22 (located just south of LTOA Site RI-32). MW-21 was sampled 7 times for VOCs from 1993 through 2000. The highest concentrations of CVOCs detected include PCE at 78 ug/L, TCE at 39 ug/L, cis 1,2-DCE at 1 ug/L and chloroform at 6 ug/L. MW-22 was also sampled 7 times from 1993 to 2000. The highest concentrations of CVOCs detected include PCE at 2J ug/L, TCE at 4J ug/L, and cis 1,2-DCE at 0.5J ug/L.

The higher concentration of PCE detected in well MW-101 constitutes a new finding. However, the detected concentrations of CVOCs do not indicate the presence of a DNAPL or source-term. The RD may consider this portion of the fluvial aquifer on the MI for enhanced bioremediation during the RA.

LTOA Group 7 (LTOA Site SS-83)

One monitoring well (MW-99) was installed in a downgradient position of this LTOA site. This location appears to be located near the northern leading edge of the PCE and TCE plumes on the southwestern portion of the MI. The saturated thickness of the fluvial aquifer was measured at approximately 22-feet and was encountered on the confining clay layer. PCE was not detected; however, TCE was detected in MW-99 at an average concentration of <1J ug/L (min. ND, max: 0 6J ug/L) and chloroform was detected at an average concentration of <1J ug/L (min: ND, max: 0.2J ug/L). No other CVOCs of concern were detected. This is consistent with concentrations detected up-gradient of well MW-20 in the 2000 sampling event (<1J ug/L concentrations of TCE and chloroform). Based on the location of this well, the RD may consider this well as part of the LTM program during the RA

LTOA Group 8

LTOA Site SS-80 - One monitoring well (MW-107) was installed in a downgradient position of this LTOA site in the intermediate aquifer. The saturated thickness of the aquifer was measured at approximately 44.5-feet and was encountered on a clay layer documented as being at least 8-feet thick. This well was constructed with 2 separate well screens separated by blank well casing PCE was detected at a maximum concentration of 0.95J ug/L and TCE was detected at a maximum concentration of 2.8 ug/L. Cis 1,2-DCE was detected at a maximum concentration of 0.3J ug/L. Chloroform was detected at a maximum

concentration of 0.2J ug/L, and carbon tetrachloride was detected at a maximum concentration of 0.2J ug/L. No other CVOCs of concern were detected. Based on the construction of this well, the RD may recommend that this well be abandoned during the RA.

LTOA Sites SS-42/43 - An attempt was made to install a monitoring well in the source area of the former LTOA PCP Dip Vat site. However, no significant saturated thickness was detected on top of the confining clay unit at this location. The SB-105 borehole was monitored overnight for groundwater and none was measured, and, as result, the boring was plugged and abandoned During the drilling effort for SB-105, composite and discrete soil samples were collected from this boring and analyzed for SVOCs (using PCP as the target analyte). Based on the results of the analyses, there are no soil impacts of PCP at this location.

Since there was no measurable groundwater detected at the SB-105 location and, based on the potentiometric surface at the time, monitoring well MW-108 was installed 325-feet south-southeast of SB-105. Within MW-108 the saturated thickness of the aquifer was measured at approximately 57-feet and was encountered on a clay layer documented as being at least 17-feet thick. The lower 10-foot section of the aquifer was screened. No PCP or resultant degradation products were detected in the groundwater sample at a concentration greater than the method detection limit of 3.1 ug/L. CVOCs detected included PCE at 2.6 ug/L, TCE at 6.4 ug/L, cis 1,2-DCE at 0.2] ug/L and chloroform at 6.4 ug/L.

Based on the location of monitoring well MW-108 and the concentrations of CVOCs detected, the RD may consider this well as part of the LTM program during the RA. Upon review of the hydrogeologic data derived from this investigation, MW-108 does not appear to be downgradient of Sites SS-42/43. Therefore, the primary objective of installing a monitoring well downgradient of the LTOA sites was not met. To satisfy this objective, the BCT decided that sentry wells completed in the intermediate aquifer west of LTOA Site SS-42/43 will be addressed as part of the LTM program during the RA. Additional monitoring well installation activity descriptions in the RD will be accompanied with a decision tree that provides direction as to which way to proceed based on the stratigraphic data from these wells (i.e., Does the clay confining unit dip downward to MW-108 from MW-62 or are there two separate units? Also, is groundwater flowing beneath the clay at MW-62 similar to what is seen at monitoring wells MW-27, -89, and -90?).

Additional soil sampling will also be conducted in the vicinity of the former PCP dip vat This work will be conducted under a separate scope of work and as a stand-alone workplan.

LTOA Group 9 (LTOA Site Former Drum Storage Area)

One additional monitoring well (MW-93) was installed in a downgradient position of this LTOA site. This location appears to be located down-gradient of the southwestern leading edge of the PCE and TCE plumes on the southeastern portion of the MI. The saturated thickness of the fluvial aquifer was measured at approximately 5-feet and was encountered on a confining clay layer measured to be at least 5-feet thick. Chloroform was the only CVOC of concern detected, at an average concentration of <1J ug/L (min: ND, max: 0.7J ug/L). Based on the location of this well, the RD may consider this well as part of the LTM program during the RA.

LTOA Group 10 (LTOA Site NE6 [former Bldg. T702])

During the LTOA investigation, a boring was advanced to the top of the clay confining unit and a temporary well was installed in soil boring SB-106. One soil sample was collected at a depth of 87-feet bgs, above the sand and gravel/clay interface. No CVOCs were detected in the sample. After a 24-hour period, no measurable groundwater was present. The well was removed and the boring plugged and abandoned as a result. Therefore, the primary objective of installing a monitoring well downgradient of the suspected area-of-concern was not met.

Surface soil samples were collected during the MI RI from 0-1 feet bgs at 3 locations (SS79A, -B and -C) surrounding NE6 and analyzed for VOCs. VOC concentrations for the soil samples at all three locations were below detection limits. Subsurface soil samples were also collected during the MI RI at 3 locations (SB79A, -B, and -C) within the following intervals: 0-1, 4-6, 8-10, and 18-20 feet bgs; all soil samples were analyzed for VOCs. The only VOC detected was methylene chloride at 2J ug/kg in the 4-6 and 8-10 foot samples of SS79A and at 1J ug/kg in the 18-20 foot sample of SS79C. Soil samples collected from SS79B were all below detection limits.

With the absence of the fluvial aquifer below NE6, coupled with the absence of VOCs in the surface and subsurface soil samples collected during the MI RI, it is recommended that no further investigation be conducted at this site. Existing downgradient monitoring wells MW-34, -36, -38, and -107 will be used as part of the LTM program during the RA.

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Tables

Table 1
LTOA Soil Sample Identifications and Details
Memphis Depot Main Installation LTOA Technical Memorandum

Volatile Organic Carbons (SW8260)

#	lle Organic Carbons (SW8260) Identification	Date	Time	Depth (ft bgs)	Matrix	Comment
1	MW-85-84	09/18/2001	1715	84	Soil	Comment
2	MW-85-97	09/19/2001	0900	97	Soil	1
3	MW-86-78	09/19/2001	1030	78	Soil	1
4	MW-86-86	09/19/2001	1430	86	Sort	
	Trip Blank	09/19/2001	NA	NA NA	Water	
5	MW-88-78	09/20/2001	1800	78	Soil	ŀ
	MW-88-788	09/20/2001	1800	78	Sorl	Duplicate
:	Trip Blank	09/20/2001	NA	NA NA	Water	Dop.ioato
6	MW-92-77	09/24/2001	1500	77	Soil	İ
7	MW-92-96	09/24/2001	1545	96	Soil	
	Tnp Blank	09/25/2001	NA	NA .	Water	<u> </u>
8	MW-93-100	09/26/2001	1245	100	Soil	
9	MW-94-108	09/26/2001	1315	108	Soit	
10	MW-93B-101	09/27/2001	1130	101	Soil	1
11	MW-96-62	09/27/2001	1530	62	Soil	1
	Trip Blank	09/27/2001	NA .	NA I	Water	
12	MW-96-82	09/27/2001	1615	82	Soil	
13	MW-98-106	10/01/2001	1715	106	Soil	1 1
14	MW-97-100	10/02/2001	915	100	Soil	
	Tnp Blank	10/02/2001	NA	NA	Water	
15	MW-99-20	10/04/2001	1500	20	Soil	
16	MW-99-90 5	10/05/2001	1330	90 5	Soil	
	Tnp Blank	10/05/2001	NA	NA	Water	
17	MW-100-92 5	10/08/2001	1430	92 5	Soil	•
18	MW-101-23	10/08/2001	1630	23	Soil	
19	MW-101-94	10/08/2001	1345	94	Soil	
•	MW-101-994	10/08/2001	1345	94	Soil	Duplicate
	Trip Blank	10/09/2001	NA	NA	Water	j
20	MW-102-108	10/10/2001	1035	108	Soil	
21	MW-103-15	10/15/2001	1100	15	Soil	
22	MW-103-61	10/15/2001	1438	61	Soil	
23	MW-103-72	10/15/2001	1525	72	Soil	
24	MW-104-63	10/15/2001	1550	63	Soil	
•	MW-104-663	10/15/2001	1600	63	Soil	Duplicate
	RB-1-JP	10/15/2001	1700	NA	Water	Eq. Blank
	RB-2-AK	10/15/2001	1035	NA	Water	Eq Blank
	Trip Blank	10/15/2001	NA	NA	Water	
25	MW-106-87	10/16/2001	1620	87	Soil	
26	MW-107-125	10/18/2001	1130	125	Soil	
	Tnp Blank	10/18/2001	NA	NA	Water	ļ
27	MW-101B-87	10/19/2001	1415	87	Soil	- 1
_	Trip Blank	10/19/2001	NA	NA	Water	
28	MW-108-97	10/22/2001	1700	97	Soil	ļ
	Trip Blank	10/22/2001	NA	NA	Water	

Table 1 LTOA Soil Sample Identifications and Details Memphis Depot Main Installation LTOA Technical Memorandum

Semi-Volatile Organic Carbons (SW846/8270)

#	Identification	Date	Time	Depth (ft bgs)	Matrix	Comment
1	MW-105-83	10/15/2001	1700	83	Soil	
2	MW-105-92	10/15/2001	1715	92	Soil	
3	MW-105-97	10/15/2001	1730	97	Soil	
4	MW-108-83.5	10/22/2001	1500	83.5	Soil	
5	MW-108-97	10/22/2001	1530	97	Soil	
6	MW-108-170	10/22/2001	1600	170	Soil	

SPLP/PCP Leachability

	TOT ECCONDUMNY			· · · · · · ·		T
#	Identification	Date	Time	Depth (ft bgs)	Matrix	Comment
1	MW-105-10-30	10/15/2001	1345	10-30	Soil	
2	MW-105-30-50	10/15/2001	1400	30-50	Soil	
3	MW-105-50-70	10/15/2001	1500	50-70	Soil	
•	MW-105-150-170	10/15/2001	1505	50-70	Soil	Duplicate .
4	MW-105-70-90	10/15/2001	1535	70-90	Soil	
5	MW-105-90-107	10/15/2001	1745	90-107	Soil	

Total Organic Carbons (TOC)

#	Identification	Date	Time	Depth (ft bgs)	Matrix	Comment
1	MW85-86ft-09182001	09/18/2001	1745	86	Soil	
2	MW85-105ft-09192001	09/19/2001	1030	105	Soil	
3	MW86-103ft-09192001	09/19/2001	1430	103	Soil	
4	MW88-83ft-09202001	09/20/2001	1648	83	Soil	
5	MW92-106ft-09252001	09/25/2001	0745	106	Soil	
6	MW94-110ft-09262001	09/26/2001	1335	110	Soil	
•	MW94-10ft-09262001	09/26/2001	1350	110	Soil	Duplicate
7	MW93B-106ft-09272001	09/27/2001	1245	106	Soil	
8	MW96-88ft-09272001	09/27/2001	1655	88	Soil	
9	MW98-110ft-10012001	10/01/2001	1715	110	Soil	
10	MW97-105ft-100201	10/02/2001	0920	105	Sort	
11	MW99-95ft-100501	10/05/2001	1330	95	Soil	
12	MW100-98ft-10082001	10/08/2001	1450	98	Soil	1
13	MW101-105ft-100901	10/09/2001	1400	105	Soit	
14	MW102-113ft-101001	10/10/2001	1130	113	Soil	
15	MW103-75ft-101501	10/15/2001	1500	75	Soil	
16	MW104-63ft-101501	10/15/2001	1410	63	Soil	}
17	MW107-153ft-101801	10/18/2001	1230	153	Soil	
18	MW108-167ft-102201	10/22/2001	1700	167	Soil	
•	MW108-267ft-102201	10/22/2001	1705	167	Soil	Duplicate

NA Not Applicable

fL Feel

bgs Below Ground Surface

Table 2 LTOA Wes Construction Datall Summary Went to Deck Han Kesskaton LTOA Technoli Mannesodum

Identification	Offsite or	Northing	Easting	Туре	Ground Elev (ftms ¹)	Top of Casing (f: msl)	Identification	TOC vs Ground E'ev (ft)	Length of Screen S (t)	Screen (ft)	Elev Of Top of Screen (it mst)	Elev Or Boltom of Screen (fr ms1)	Depth of Boring (bgs)	Elev of Bottom of Bonng (ft)
CONTRACTOR OF THE PROPERTY OF	_						Monitoring Wells							
25.44	δ	276704 14	806064 51	¥.W	200	38	NW 85	£ 37	0.50	:	208.4	3 603		,
MW 86	5	278696 65	806301 24	ž	304 89	304.35	KW-88	2	2 2 2	۶ :			?:	200
uw 88	ဝ်	276679 05	806512 88	M	305 47	305	MON-AS	25	``					8
WW 92	ò	276614 20	806489 66	Š	30478	30.	MW 92	7.5	7 6	2 :	22.5	200	Ç:	0.00
NW 83	δ	275542 22	804440 10	**	294.31	8 %	MW-93	0.23	2 2	, <u>(</u>	2023	1 7 6 1		
3 3	δ	276009 92	603375 23	≩	296 95	3. %	MAY 94	00	1005	9	2	3 4	? =	200
96.WA	δ	276310 14	606320 24	≩	289.67	289 02	Mrv 96	-0.65	75.5	۱ ۶	214 2	2		
16:MM	δ	276074 23	60213923	¥	297 73	297 44	76-WW	Ç 58	97.5	2	2002	2003	3 5	3 2
St Mar	5	27689 37	802572 77	Š	294 93	294 43	86 MA	8	137	Ç	157.9	67.9	64	
86-MM	5	277443 37	801114 53	ž	285 69	265 33	WW-89	96 0	218	8	2 2	74.2	2 4	
MW 100	ð	276590 40	800852 83	Š	3. 2.	291 16	Mrw-100	-0.38	\$ 40.	8	184.0	2	3 54	
BOC. AW	ģ	276600 65	800854 43	ž	29160	28108	MW 1008*	3	107.5	: 8			2 2 2	
101-1414	δ	278204 27	80111038	Š	29.58	291 73	MW 101 (first interval)	0 29	6	42	200		2 2	5
	W.: pe Sc						IVW *01 (second interval)		· ·	=	1810		;	2
	Mus ple Sc	ŧ	2				MW 101 (part laters)				2 2	? ?		
WW -C2	δ	275760 10	01.9.7008	Š	311 70	ا ا ا	NAW 222	98.0	\$ 50.	?	2	3		,
LAW 1029	δ	275760 59	620707 72	Š	312 C7	31.40	MW 1928	-0.57	3.2.	3 5		3 2	2	2 5
IAV 103	6 -	27863192	90516079	Š	G . 55	30.35	MAY-193	55.00	2	R	9.10		2	
kw 104	6 -	278677 45	80541772	ΝŽ	296 13	295 76	MW 104	2037	70.5	2 %	225.6	300		200
N.W 107	င်	278419 C7	803039 93	Š	305 18	324 92	MW-107 (first merval)	0.26	2,5	: :	177.5	207	200	3
	No. ible Scr	Mutiple Screened Monitoring	- M				NtW 107 (second rule val)	:	·	9		-	9	7 8 5
MAN TOB	δ	277658 C2	602985 53	Š	303 25	3C3 C7	MAN 108	6.	991	2 2	1433	1333	187 0	1163
Sol Bornos.									•					
SB 1C5	δ	277992 69	802931 84	88	304.29	ž	\$c av	5	-		;	;	_	
SB-106	៦	278969 20	803009 84	SB	311.81	₹ Ž	8.88	≦ ≱	£ ‡	źź	<u> </u>	2 2	0,00	1973
Replacement west for livin 30 and livin 102. Livin 100 and 132	0 and 4/W 102 A		ell be obendoned at a later date	4 a later day									5	

			Onsite or	}		Ground	TOC	Depth to	Water Level	Notes
Well 10	Туре	Location	Offsee	Northeng	Easting	Elevation	Elevation	Water 11/01/01	Elevation	
						(feet MSL)	(Seet MSL)	(feet BTOC)	(feet MSL)	1
MW-02	MW.	DF ~	On On	261693 78	802244 75	289 70	292 04	DRY		
MW-03 MW-04	MW	OF OF	On On	281598 25 281278 87	802100 69	290 40 300 00	292 35 301 61	70 69 NM	221 66	
MW-05	MW	DF	On	281254 49	802084 68	301 30	304 64	DRY	224 84	Pressure Transducer Installed
MW-06	MW	OF 1	On	280604 17	802069 13	288 10	269 11	65 11	224 00	
MW-07	ww	DF	On	201639 88	802481 70	293 10	295 10	68 39	226 71	1
MW-08	MW	DF	On .	282001 04	802727 91	292 74	292 59	63 73	228 86	į.
MW-09	MW	DF	On On	281641 18 281662 55	802518 42	304 66	304 32	77 89	226 43	1
MW 11	ww	DF	On	281353 10	802201 26 802099 00	289 20 299 59	288 79 299 47	66 51 76 81	223 18 222 66	
MW 12	MW	OF .	On	281067 19	802071 22	301 70	301 30	77 19	224 11	
MW 13	MW	OF	On	281033 56	802369 21	300 10	300 01	NM	224 81	Pressure Transducer Installed
MW 14 MW 15	MW	DF i	On :	280003 37	802288 95	302 44	302 22	75 0 0	227 22	
MAY 15	MW	DF Mi	On On	280348 88 278837 83	801985 36 807099 56	295.23 300.19	295 12	73 63	224 49	
MW 17	MW	MI	On :	2/9061 13	803801 63	316 18	299 86 315 85	58 42 NM	241 44	Obstruction in well
MW 18	MW	MI	On	279136 41	802448 08	308 34	308 04	132.84	175 20	COST OCCONT ST WILL
MW 19	MW	MI	On	278945 87	800782 26	290 86	290 57	89 65	200 92	4
MW-20	MW	M	On	277677 06	800705 19	285 71	285.21	RS 91	199 30	1
MW 21 MW 22	NAM	M	On On	276473 39	800602 39	295 21	295 00	95.05	199 95	1
MW 23	MAY	M	On	275912 38 275791 02	800702 16	298 49 299 24	298 04 298 99	98.01 100.42	200 03 198 57	ĺ
MW-24	MW	M	On	275616 05	803538 81	299 81	299 51	106 89	190 62	ĺ
MW 25	MW	M	On	275976 09	805529 10	270 32	270 17	NM .		Obstruction in well (offset casing)
MW 26	MW	M	On .	276508 16	805962 09	303 89	303 69	100 66	263 03	_
MW 27 MW 28	MW MW	Me DF	On O	278285 47	802547 09	304 28	303 98	DRY	. 	89 00 N BTOC
MW 29	MA	DF	On On	281568 58 282104 92	803154 48 802863 96	294 89 273 35	294 79 273 22	60 93 39 70	233 86 233 52	!
MW-30	MW	DF	Off (N)	282229 19	802013 96	274 10	275 14	48 55	226 59	i
MW-31	MW	DF	Off (NW)	281651 53	801783 90	287 50	290 37	72 03	218 34	i
MW-32	MW	DF	Off (W)	280834 37	80161551	285 60	285 38	63 97	221 41	
MW-33 MW-34	MW	DF DF	Off (W)	280398 10	801561.30	277 70	280 71	56 53	224 18	
MW-35	WW	DF	On I	279411 21 281072 31	801917 95 802070 44	300 80 301 70	299 97 300 45	143 31 78 12	156 66 222 34	
MW-36	MW	DF	On	279531 02	602887 01	311 15	310 24	158 71	151 53	
MW 37	MW	OF	Off (W)	280631 22	801616 58	285 50	284 91	133 79	151 12	
MW-38	MW	M	On	279141 38	602450 43	308 45	307 45	137 48	169 97	
MW-39 MW-40	MW	Mf DF	On	277280 67	802598 11	296 58	296 28	104.39	191 89	
MW-41	MW	DEMI	Off (NW)	282460 42 279621 65	800948 23 800457 21	262 50 283 15	262 23 283 81	91 18 65 95	171 05 217 86	
MW-42	MW	DF	Off (W)	281863 92	800182 40	275 10	274 83	57 13	217 70	
MW-43	MW (DF	O*(W)	280284 33	800111 73	284 99	284 99	132 24	152 75	
MW-44	MW	DF	Off (W)	281073 71	800601 09	269 40	269 07	56 10	212 97	
MW-45	MW	DF DF	Off (E)	280728 08	804125 99	293 30	293 22	NM	236 86	Pressure Transducer Instaffed
MW-47	w	340	Off (S)	281256 81 275261 64	803115 96 800780 89	286 83 292 15	267 56 306 39	55 51 102 50	232 05 203 89	
MW-48	ww	M	Off (W)	2/5616 18	799793 92	283 55	284 49	HAA	-	Well destroyed
MW-49	MW	DF	Qn i	280211 84	803051 31	309 52	310 49	79 93	230 56	
MW 50	MW	Mi	On	276455 81	807065 28	299 32	298 82	86 61	212 21	
MW 51 MW-52	MW	DF	Off (N)	282345 86	802828 62	275 50	275 23	40 61	234 62	1
MW-53	MW	Mdi Mdi	On Off (N)	275371 97 279176 66	805897.36 805136.05	279 71 305 58	279 26 306 38	82 01 73 71	197 25 232 67	
MW-54	MW	DF	O# (W)	281160 10	801183 32	295 60	295 35	81 75	213 60	
MW-55	MW	MI	0٠	279301 05	801204 62	292 48	292 08	NM	221 05	Pressure Transducer Installed
MW 56	MW	DF	On	279708 26	801971 55	293 50	293 60	67 99	225 61	
MW 57 MW-58	MW	DF DF	On On	280184 05 279845 07	802006 19 802066 44	291 10 290 70	290 77	65 80	224 97	
MW-59	MW	o∓ I	On I	281333 67	802252 00	300 40	290 51 300 13	64 22 76 21	226 29 223 92	
MW-80	MW	Dr	On	281424 39	802282 05	297 20	296 86	72 71	224 15	I
MW-61	WW	OF	On	281585 68	802347 35	294 20	294 04	69 31	224 73	
MW-82	MW	J	On	276289 69	801858 16	294 10	293 65	93 94	199 71	ł
MW-64	MW I	MJ (On On	278192 29 276951 52	803585 83 805005 97	306 ?? 304 ??	306 06	108 50 107 38	197 46	
MW-65	MW	0	Off (N)	203529 72	803887 68	264 00	304 21 263 22	107 38	196 83 252 65	
MW-86	MW	MI	Off (W)	276742 50	798517 42	289 00	288 7	NM.		Unable to remove well lid
MW-67	MW	DF	Off (W)	280474 00	800830 36	275.53	278 21	126 62	151 59	
MW-68	WW	o+ ~-	Off (W)	281500 76		291 60	291 69	69 90	221 79	
MW-69 MW 70	MW	OF DF	Off (W)	281202 55 281029 60		304 90	307 02	84 58	222 44	
MW 71	MW	DF	Off (W)	280584 68		302 80 291 90	304 99 294 40	81 93 71 97	223 06 222 43	
MW 72	MW	MI	Off (SW)	275626 27		295 41	295 11	#9 20	205 91	
MW 73	MW	DF	On i	280989 42	802144 95	301 10	300 65	76 78	223 87	
MW 74	MW	DF .	On	280991 20		304 00	303 68	80 32	223 36	
MW 75 MW 76	MW	DF DF	On	281080 10		304 30	303 61	80 52	222 99	
MW 77	MW	DF	Off (W)	281311 98 281142 96	801842 76	303 30 304 70	302 71 304 42	85 67 83 00	217 04 221 42	
MW 78	MW	O+	Off (N)		802065 28	275 40	275 00	49 89	225 11	
MW 79	MW	DF I	Off (W)	281794 22		285 40	285 03	72 40	212 63	

Table 3 Water Level Elevation Scannary - Movember 1, 2001 Memples Depot Man Installation LTOA Fechacial Memorandum

	T					Ground	TOC	Depth to	Water Level	Notes
Well ID	Туре	Location	Onate or	Northing	Easting	Elevation	Elevation	Water 11/01/01	Elevation	ļ
	"		Offsee	•		(feet MSL)	(feet MSL)	(feet BTOC)	(feel MSL)	
MW-80	IW.	DF	Off (W)	281417 56	800199 07	274 00	273 81	61 17	212 64	1
MW-81	MW	M	On	275608 42	803527 67	299 97	299 62	144.95	154 G7	
MW-82	MW	M	On	278539 89	800862 13	292 17	291 77	140 27	151 50	
MW-83	MW	М	On i	276521 38	305969 16	304 56	304 21	146 73	157 48	
MW-84	MW	DF	On	279531 09	802876 65	31127	311 15	NMA	228 46	Pressure Transducer Installed
MW-65	LAW	MI	On	276704 14	806064 51	304 50	304 13	99 97	204 15	
MW-86	MW	MI	On .	276696 85	806301 24	304 89	304 35	98 27	206 08	
MW-87	MON	DF	Ön	280696 36	802038 55	292 80	294 93	71 23	223 70	Į.
MW 88	MW	MI	On .	276879 05	80651288	305.47	305 15	80.98	224 17	1
MW-89	MW	MI	On .	278286 97	802555 25	304 38	303 98	120 41	183 57	1
MW-90	MW	Mi	On	278283 60	802539 51	304 64	304 19	120 25	183 94	!
MW-91	MW	DF .	On	280474 97	802014 43	289 30	291 99	68 23	223 76	į.
MW-92	MW	MI	On .	276614 20	806489 66	304 78	304.41	96 75	207 66	
MW-93	MW	M	On .	275647 22	804440 10	294 31	294 06	102 45	191 63	
MW 94	MW	M	On	276009 92	803375 23	296 95	296 94	107 07	189 87	
MW 95	MW	DF	Off (N)	282707 50	801850 21	259 70	259 43	30 61	228 82	
MW-96	MW	Line Line	On	2/6310 14	806320 24	289 67	289 02	83.02	206 00	
MW 97	MAN		l ión	276074 23	802139 23	297 70	297 44	101 25	196 19	
MW-98	MW	-	On	2/6891 37	802572 77	294 93	294 43	102 00	192 43	
	MW		000	277443 37	801114 53	285 69	285 33	e9 60	195 73	
MW-99			<u>بر</u>	276590 49	800852 83	291 54	291 15	92.95	198 21	
MW 100	MW	141	On On	276600 65	800854 43	291 60	291 06	NM		Installed on 11/14/2001
MW 100B	MW	M	On On	276204 27	801110 38	291 99	29170	93.32	198 38	
MW 101	MW			275760 10	80071610	311 70	31134	110.66	200 68	1
MW 102	MW	M	On	275760 10	800707 72	312 07	311 40	NM	-	Installed on 11/15/2001
MW 1028	MW	144	On On	278691 92	805160 79	301 90	30135	69 43	231 92	
MW 103	MW	M	On			296 13	295 76	63 01	232 75	1
MW 104	MW	MI	On	278677 45	805417 72.	305 18	304.92	114 43	190 49	
MW 107	. MW	M	On .	278419 07	802985 53	303 15	303 07	113 21	189 86	
MW 106	MW	M	On.	277658 02		308 00	307 76	105 02	202 74	
PZ-01	PZ	M	Off (S)	275150 00	801750 00		264 39	42 48	241 91	
PZ-02	PZ	DF .	Off (N)	262748 00	803373 00	285 00		197 04	191 47	
PZ-03	PZ	M	On	276379 33	802941 05	298 98 303 00	298 51 302 30	98 34	203 96	
PZ-04	PZ	M	Off (SW)	275905 40	799780 49			59 50	196 54	
PZ-05	PZ	MI	Off (S)	274934 58	806177 53	257 00	256 04	73 52	229 22	
PZ-06	PZ	M	On	278855 86	805100 13	302 95	302 74	98.96	205 74	1
PZ-07	₽Ž	MI	On	277053 25	806006 75	305.22	304 72		204 86	1
PZ-08	PZ	M	Off (5)	274652 33	800732 76	290 00	289 35	84 49		pumping
RW-01	RW	OF .	On	280267 14	801973 88	294 10	NEM	75 80]	· · •
RW-01A	RW	DF	On	280386 26	801990 08	293 87	NM	73 94	i -	pumping
RW-018	RW	OF	On	280504 87	802009 37	287 85	NeM	69 88	1	pumping
RW-02	RYY	OF	On	280624 56	802003 32	268 49	NAM	71 07	l -	pumping No piszometer installed
RW-03	HW	DF	On	280743 76	802012 69	297 73	NA.	NA.	l ~	
RW-04	RW	DF	On	280918 07	602027 11	303 69	305 48	82 10	223 38	pumping
RW-05	RW	OF	On	261113 38	802041 97	305 75	NM	89 30		pumping
RW-06	RW	DF	On .	281264 22	802067 17	303 15	304 94	84 12	220 82	pumping
RW-07	RW	DF	On	281442 21	802079 19	296 07	NMA	76 43	l	brimbing
RW-08	RW	D+	On	281574 72	602068 53	291 56	291 34	74 10	219 24	pumping
RW-09	RW	DF	On .	281688 06	802232 41	289 26	290 98	69 09	221 89	pumping

RW-09 RW DF On 281688 06 8
Hall + Ind measured
HAL + Not Applicable
6M* - Mandaring Well
FW - Recovery Well
FV - Recovery Well

The tablowing data regarding the flacovery Wells for 11/01/01 is frum the Jacobs Oct 2001 Operature Report RW 02 in operation on 11/01/01 (\$14.9 gmm RW 02) in operation on 11/01/01 (\$14.9 gmm RW 02) in operation on 11/01/01 (\$14.9 gmm RW 02) in operation on 11/01/01 (\$1.9 gmm RW 02

Table 4
Summary of Total Organic Carbon Analytical Results
Memphis Depot Main Installation LTOA Technical Memorandum

Monitoring	Sample Depth	TOC
Well	(ft bgs)	(mg/kg)
MW-85	86	< 100
MW-85	105	< 100
MW-86	103	< 100
MW-88	83	< 100
MW-92	106	< 100
MW-93	106	< 100
MW-94	110	< 100
MW-96	88	< 100
MW-97	105	670
MW-98	110	533
MW-99	95	760
MW-100	98	601
MW-101	105	452
MW-102	113	482
MW-103	75	501
MW-104	63	644
MW-107	153	372
MW-108	167	176

ft bgs = feet below ground surface mg/kg = milligrams per kilogram

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<u> </u>	3		2222222			2 2	222222		,	222222
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Bag 10 Interval	- INW-85	MW-86	INW 88	INW 92	MW-93	MW 94	MW-96		MW-98	66 MM = -
Bag 9 Interval Upper Lower		2 117 5 FP						,		
		5511	\$·			ļ		5211		
Oeg 6 heersal		1.3 \$	*					115.4	ļ 	
Beg / Marval Upper Lower (A BTOC)		ins ins			. voi.	 		11135 1155		103 1055
Bag Sinterval Bag Sinterval Bag Sinterval Upper Lower Upper Lower (R 810C)		20.5	16 18	. 501	en		5 26 - 5 56	1115 - 1115		2001 - 2101
Tubion Sami	90 <u>i</u>	280	١٥١	.हैं	<u>a</u>		18	S =	14	\$ 2
		2 601	ε;	§,	<u> </u>			: §	- 45 .	's;
Bag 4 interval Upper I ower	1049 - 1069	8 /01 8 2 <u>01</u>	50		<u>ā</u>		8 8 8	\$ 55.	5 1 165	*\$.
I PARA (C		50 50 10 10	£.	, <u>ā</u>	,s:		S 5 6 8 1	, 57 <u>0</u> 1	<u>;ā</u>	5 79 .
Upper Lower	107 9	201.		, 8 	7.6				· · ·	\$8.
Bag 2 Interval Upper Lower (ft BTOC)		ig.	£	ş	. %	1135	\$ 20	2 201	13.	, <u>\$</u>
		\$ 6.	.2	5	g	80	57 Ve	\$ 61	81	ŝ
Bag 1 Interval Upper Lower (ft BTOC)	£.001.	\$ 5.50	£ 6	3 3	8	2 <u>80</u>	835 R55	\$ 60. \$ 101	33	918
T	!		*	54 /0.	<i>(</i> c)	70.1	\$ 58 5 2	\$	5	\$ F
Mondoring Screen Interval Depth to Depth to West Upper Lower Waster 100 of Clark to)6 g	£	8 2	8 22	102 45	07.07	63.02	₩ ₩	201	9 6
Lower (601.	۶۶	26	8	<u></u>	ça:	8	· s · · · · · · · · · · · · · · · · · ·	*	n =
Screen in Upper (** BTOC) (**	P 2 9	\$ 76	26	s .) }	8 8	\$5	5 26	<u>.</u>	\$16
	20	9 9	88- AJN	MW-92	16W 93	76 MI	36: MUM: 36	MW-97	MW 98	66- AM

ĕ Table 5
LTOA Officeon Bag and Low-Flow Sampling Detail Summary - November/December 2
Mempry Doco Mar Viscalator LTOA Tournal Mercanous
Mempry Doco Mar Viscalator LTOA Tournal Mercanous
Mempry Docor Mar Viscalator LTOA Tournal Docor No. Bag I Enterval

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Figures

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CLAY ELEVATION EXCEEDS ORDUNDMATER

SHOUNDWATER FLOW DIRECTION

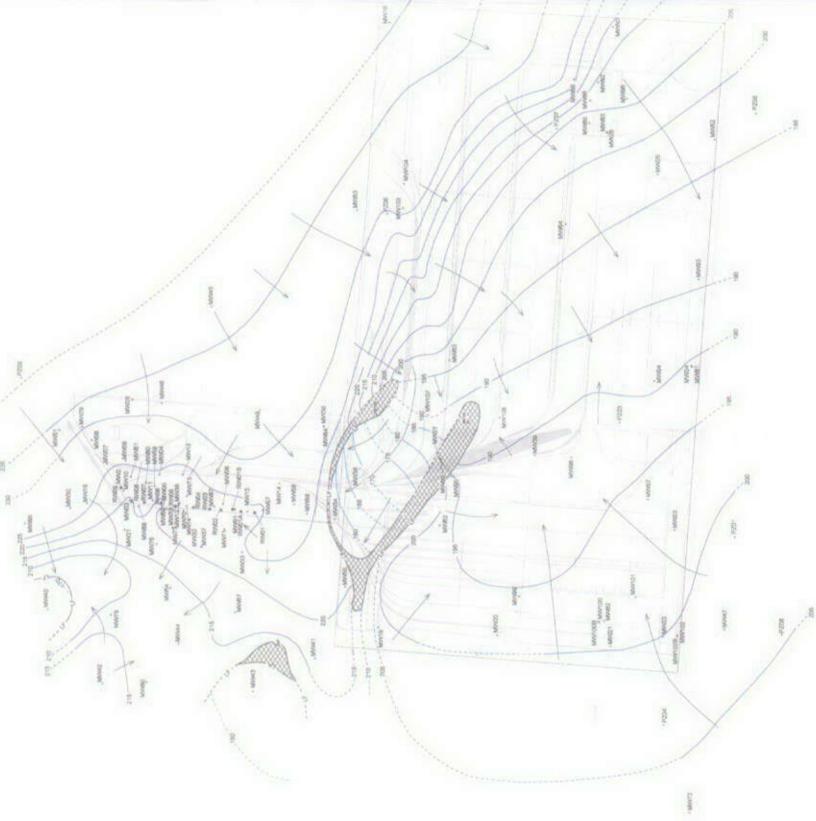
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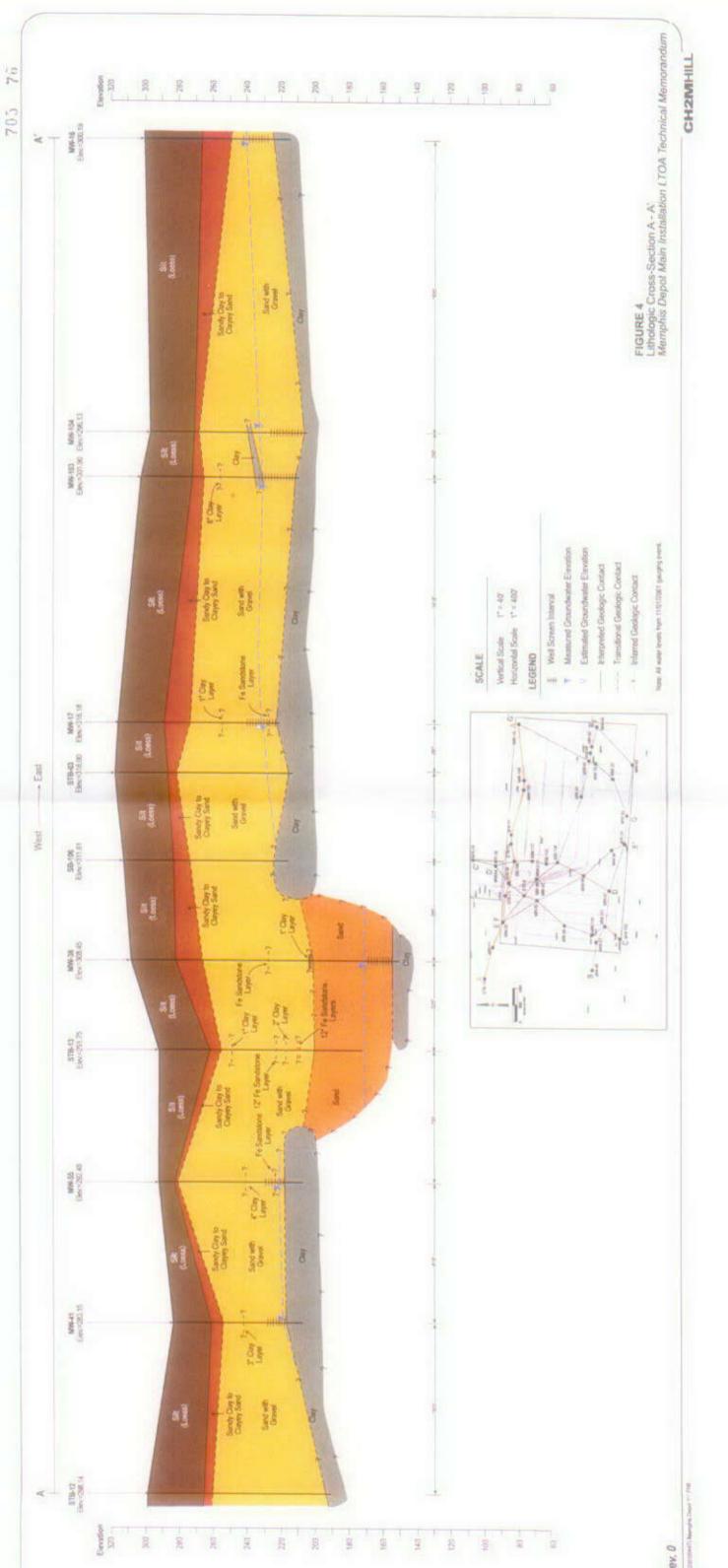
MAND? IS SCREENED IN THE MEMPHIS ADJUSTER AND THEREFORE NOT INCLUDED IN THIS POTENTIOMETRIC SURFACE MAP DEPTH TO MATER MEASUREMENTS WERE NOT COLLECTED IN MACE, 4ff AND 56. NO MEASUREABLE WATER LEVELS WERE RECORDED IN MAYO, 5, 17, AND 27.

58-105 AND 106 WERE MEASURED ON OCTOBER 18, 2001 AND OCTOBER 17, 2001, RESPECTIVELY

Including Intermediate Aquifer Map of the Fluvial Aquifer Potentiometric Surface November 01, 2001 FIGURE 3B

REV 1 MEMPHIS DEPOT, MAIN INSTALLATION LTOA TECHNICAL MEMORANDUM CH2MHILL





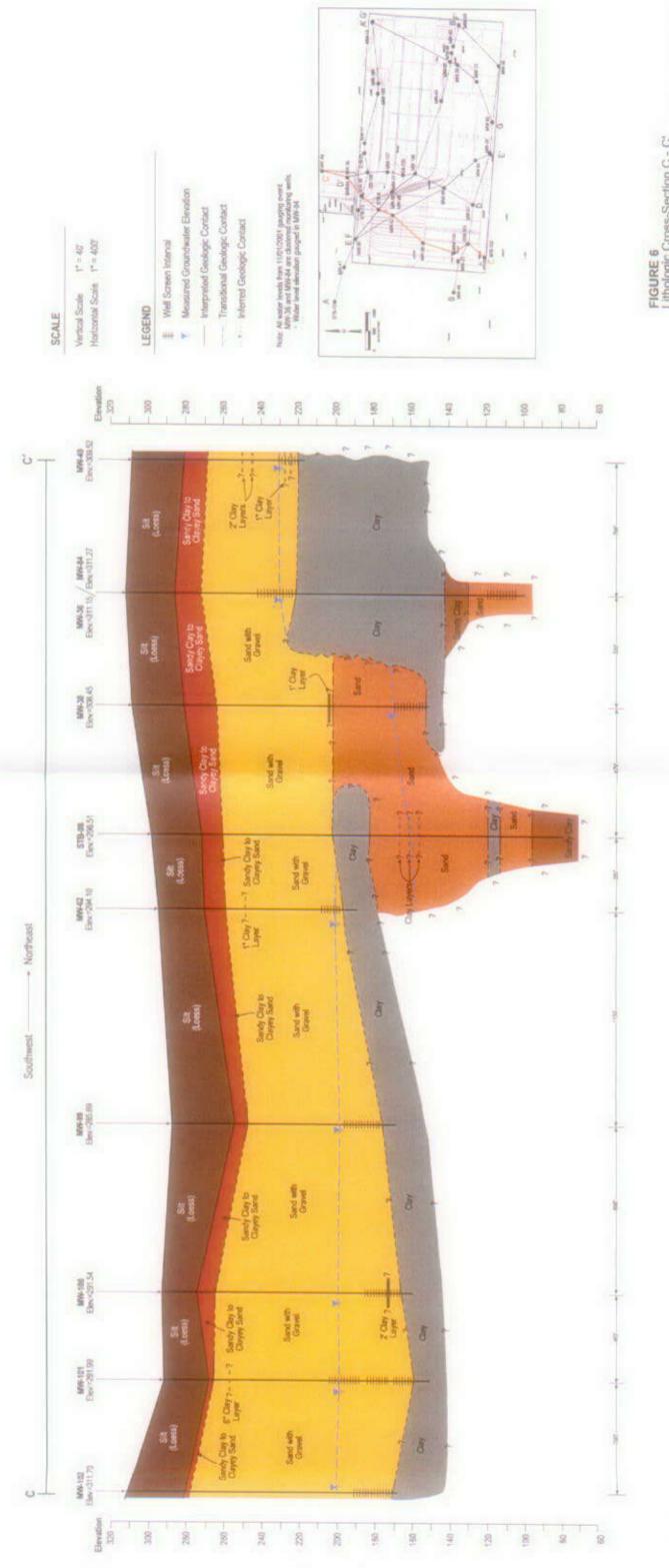


FIGURE 6 Lithologic Cross-Section C - C' Memphis Depot Main Installation EBT Treatability Study

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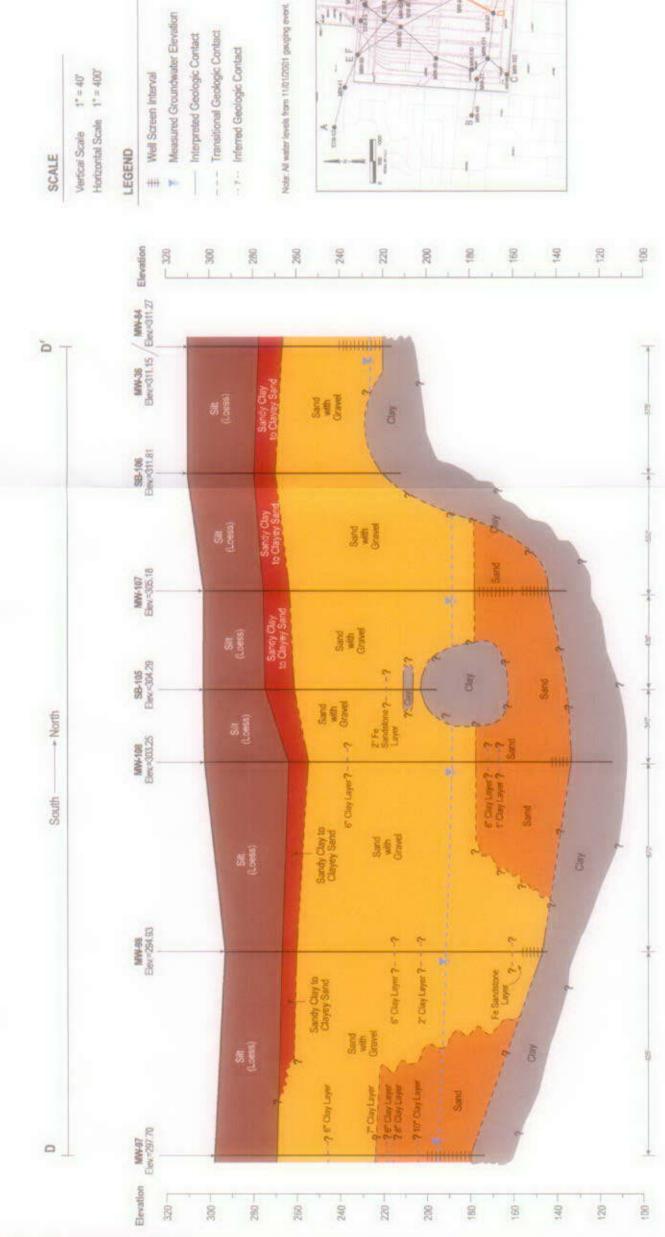
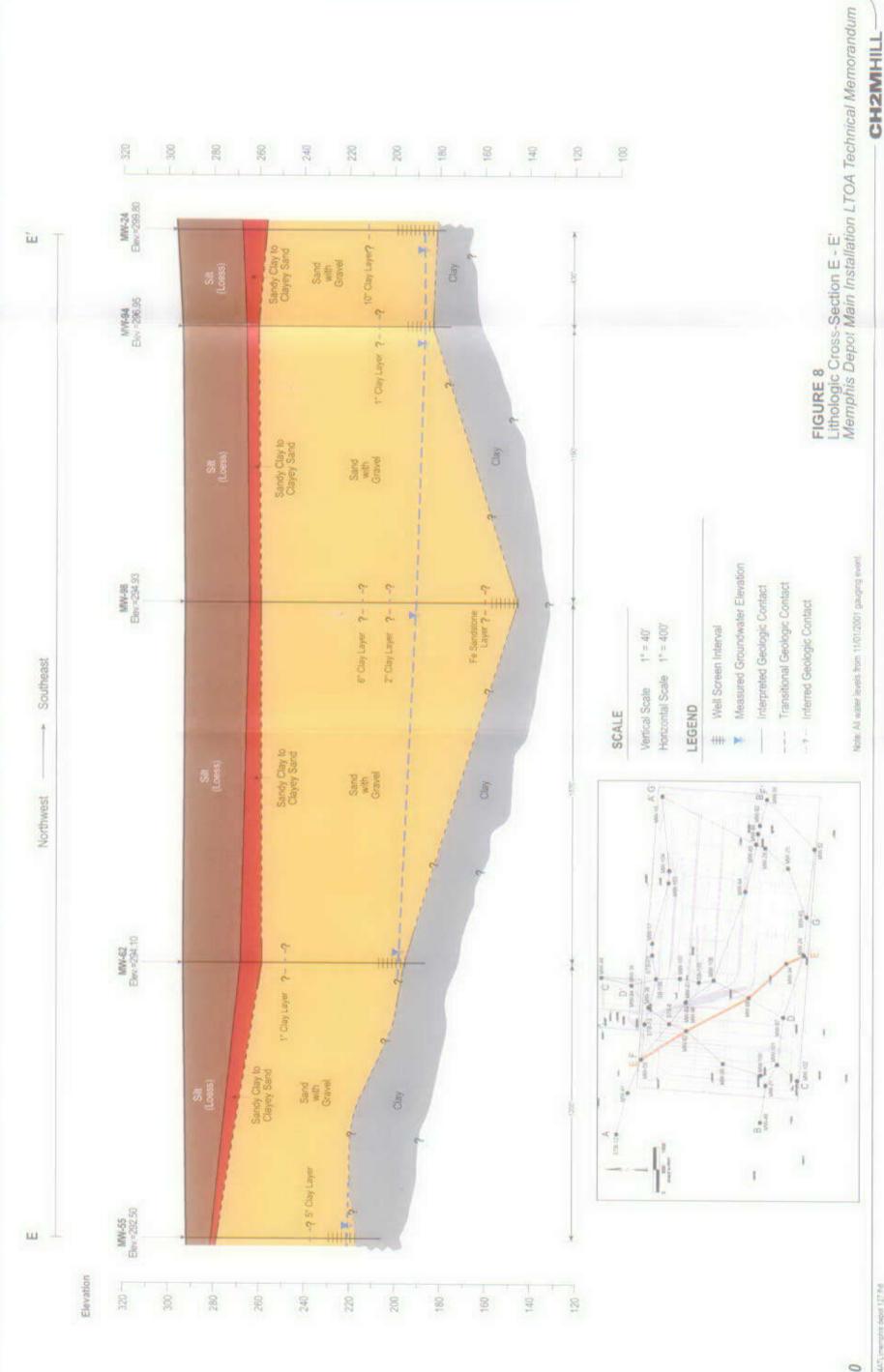


FIGURE 7
Lithologic Cross-Section D - D'
Memphis Depot Main Installation LTOA Technical Memorandum

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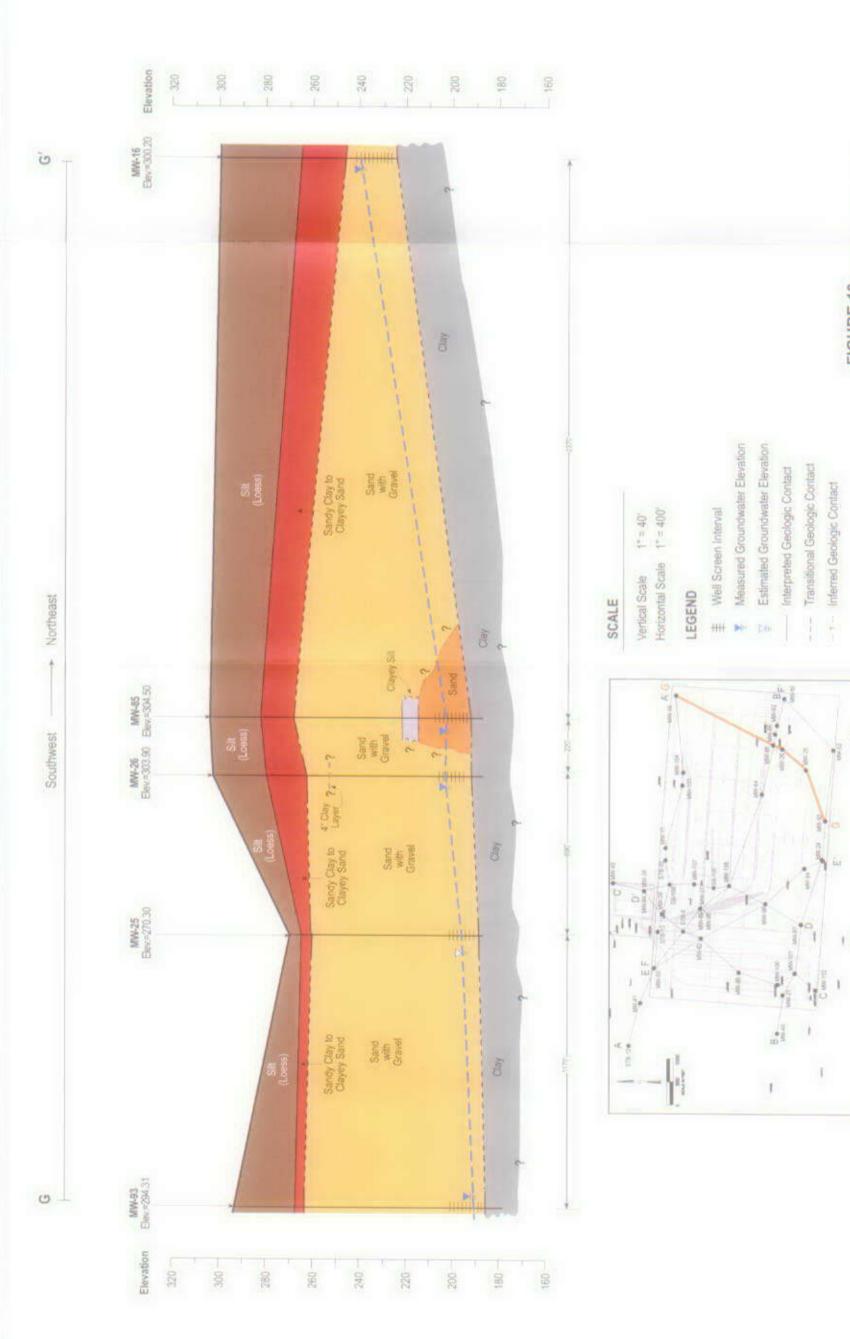


FIGURE 10
Lithologic Cross-Section G - G'
Memphis Depot Main Installation LTOA Technical Memorandum

Note: All water levels from 11/01/2001 gauging event.

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ATLANTA/CAD1/PROJECTS/9448071DDMT

Attachment 1 – LTOA Soil Boring Logs

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PROJECT NUMBER	BORING NUMBER	
160492 SA.03	MW-85	
	SOIL BORING LOG	

						···
PROJEC				al <u>Areas Me</u> mphis		
ELEVAT		304 131	cel MSL (TO	C) <u>, 304 50 fee</u> l MSI	L (ground) DRILLING CONTRACTOR Tri-State Testing Service	is, Inc
URILLIN	4G METI	HOD AND	EQUIPMEN	IT USED Hollow S	Stern Auger 4 25 inch ID with CME Sampler	
				1/2001) START	09/18/2001 END 09/19/2001 LOGGER	Jay Parker (Jacobs)
		URFACE	(FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERV			PENETRATION		1
1 1		RECOVE	RY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
1			#/TYPE	RESULTS	MOISTURE CONTENT. RELATIVE DENSITY	DRILLING FLUID LOSS
i		i		6.4.4.6.	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
		<u></u>		(N)	MINERALOGY	Corrected FID (ppm)
		ļ		Used hollow stem	Blacktop	(Soil headspace)
· -!		100		auger	6° gravel clayey silt reddish brown 5 yr 5/3 firm dam;	
_			l	drilling method		1
		ł	Į.	no penetration test		•
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PROJECT NUMBER	BORING NUMBER	
160492 SA.03	MW-85	
	SOIL BORING LOG	

PROJE	CT	Long Te	rm Operation	al Areas - <u>Memphis</u>	Depot LOCATION Memphis Tennessee	
ELFVA	TION _	304 13 (eet MSL (TO	C), 304 50 feel MSI	(ground) DRILLING CONTRACTOR Tri State Testing Service	<u>es,</u> Inc
					tem Auger 4 25 inch ID with CME Sampler	 _
				1/2001) STARY	09/18/2001 END 09/19/2001 LOGGER	Jay Purker (Jacobs)
DEPTH	BELOW S		(FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERVA			PENETRATION		
		RECOVE		TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
		i	M/TYPE	RESULTS	MOISTURE CONTENT. RELATIVE DENSITY	DRILLING FLUID LOSS
	1	l		6666.	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION Corrected FID (ppm)
		<u> </u>	-	(N)	MINERALOGY	CONTRACT D (Spin)
	!	!]	Used hollow stem	SAND fine brownishly yellow 10YR6/6 very well some grayer streaks	
_	•	i	ļ	auger	dry to damp loose	
- 3	i i	i	1	dniling method no penetration test		-
40	!!!	60]	results		10 _
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i	ĺ	١,			SAND: strong brown 7 SYR/5/8 poorly sorted, fine to coarse, small pebbles, samp, loose, rounded to subrounded pebbler	
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i	i		i		and a second burst and a second and the second and	
					SAND: strong brown 7 SYR 6/6 line: well sorted, some small pebbles to gravel loose, morst to damp.	
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į	1				SAND yellow 10YR, 7/6 very fine to fine well sorted loose, dry to dom;	-
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65	i	100				3.5
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i	;		·]		SAND reddish yellow 7 5YR 6/6 fine well sorted trace pubbles loose dams	
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70	- :	100				03
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-Ì	į					
· !	ļ		ŀ		At 71.5 turns to SAND with 40% gravel: fine to coarse gravel up to 1.5° pebbles	
-¦	:		Ī		moltied yellow coarse sand 10YR 7/4	
-i	i	1			SAND brownish yellow 7.5YR 6/4 fine to mied. With some gravel to 1.5" subrounded tionse, damp to dry. Pebbles and gravel – 10%	-
1	ı				Contaminate many mark mark i pantana markana.	

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PROJECT NUMBER	BORING NUMBER	
160492 SA 03	MW-85	
	SOIL BORING LOG	

PROJECT Long Term Operational Areas Memphis Depot **LOCATION** Memphis Tennessen DRILLING CONTRACTOR In State Testing Services, Inc. LLEVATION 304 13 feet MSL (TOC), 304 50 feet MSL (ground) DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4 25 such ID with CME Sampler WATER LEVELS 99 97 feet BTOC (11/2001) START 09/18/2001 END 09/18 09/19/2001 LOGGER Jay Parker (Jacobs) DEPTH BELOW SURFACE (FT) STANDARO SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) TEST DEPTH OF CASING DRILLING RATE, SUIL NAME USCS GROUP SYMBOL COLOR MOISTURE CONTENT: RELATIVE DENSITY DRILLING FLUID LOSS RESULTS 6-6-6-6-OR CONSISTENCY SOIL STRUCTURE TESTS, AND INSTRUMENTATION (N) MINERALOGY Corrected FID (ppm) 75 50 SAND brownish yellow 7.5YR 6/4 line to med. With some gravel to 1.5" subrounded, loose, damp to dry. Pabbles and gravel = 10% Used hollow sten 23 auger dntling method to penetration te results Same as above, fine to coarse, approx, 15% to 20% peobles and gravel 100 80 30 ecoming moist to wet at 80.0 AL81 SAND very pale brown 10YR 7/3 wet to salurated very line to fine loose SANOY SILT wickly light gray 2 5Y 7/2 very line said well to saturated." Sample collected for VOCs 85 100 (g) 86.5 yellowish brown color Sample collected for TOC me as at 86.5 grades to SAND white 10 YR 8/1 line well-sorted 90 100 oist to wel @ 89 5 Same as above, grading to SAND w/50% pebbles and gravel to 95. Light yollow brown matrix, 10YR, 6/3, med to coarse sand subrounded and ubangular pebbles and gravel damp to most 95 80 Turning wet from 95 feet to 97.5 feet, same as above to 99.5 feet, then turns it SAND-pale yellow 2.5Y-7/2 final loose well sorter. Sample collected for VOCs Same as above to 99.5 feet Water table 100 100 SAND pule yellow 2.5Y, 7/2 fine loose, well sorted, morst to writ At 101.5 GRAVELLY SAND strong brown 7.5Y 5/6 gravel to 1 inch. subrounded to subangular sand, fine to oparse. Approx. 50/50 gravel/sand wet Same GRAVEL & SAND to 103.
Then grades to a SAND salty SAND olive yellow 2.5Y 6/6 very lime to fixe flense minist/weVsaturated. 105 100 ample collected for TOC At 105.5 SAND light grey 2.5Y 7/2 very fine to line loose saturated Same as above SAND 110 100

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PROJECT NUMBER 160492 SA.03	BORING NUMBER MW-85
	SOIL BORING LOG

PROJE	cr	Long Te	m Operation	al Areas Memphis	Deput LOCATION Memphis Tennessee	
ELEVA	TION MG METI	304 13 f	eel <u>MSL (TOC</u>	C) 304 50 feet MSL	(ground) DRILLING CONTRACTOR To State Yesting Services tem Auger 4 25 inch ID with CME Sampley	, Inc
WATER	LEVEL	5 99 97	red BTOC (1	1/2001) START	09/18/2001 END 09/19/2001 LOGGER	Jay Parker (Jacobs)
DEPTH	BFLOW S	URFACE (FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
l	NIERV			PENETRATION		
l		RECOVE	RY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING, DRILLING RATE DRILLING FLUID LOSS
•	1	İ	s/TYPŁ	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	TESTS, AND INSTRUMENTATION
Ĭ		Ì	•	(N)	OR CONSISTENCY SOIL STRUCTURE MINERALOGY	Corrected FID (ppm)
<u> </u>	! 	<u> </u>		1.4	SAND	-
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PROJECT NUMBER	BORING NUMBER	
160492.SA.03	MW-86	
	SOIL BORING LOG	

PROJECT Long Term Operational Areas Memphis Depot LOCATION Memphis Tennessee
 ELFVATION
 304 35 feet MSL (TOC), 304 89 feet MSL (ground)
 DRILLING CONTR

 DRILLING METHOD AND FOUIPMENT USED WATER LEVELS
 Hollow Stem Auger 4.25 inch 1D with CME Sampler WATER LEVELS
 98 27 feet BTOC (11/2001)
 START
 09/18/2001
 FND
 09/24
 DRILLING CONTRACTOR Tri State Testing Services, Inc. END 09/24/2001 LOGGER Adam Kaiser (Jacobs) DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) TEST SOIL NAME USCS GROUP SYMBOL COLOR DEPTH OF CASING DRILLING RATE RESULTS MOISTURE CONTENT RELATIVE DENSITY DRILLING FLUID LOSS 6.-6. 9. 6. OR CONSISTENCY SOIL STRUCTURE TESTS, AND INSTRUMENTATION Corrected FID (ppm) (Soil headspace) (N) MINERALOGY ASPHALT Sity clay most brown low plasticity Used hollow sten auger drilling method no penetration tes rosults 80 23 Sity citry most, brown low plasticity 100 12 6 ty clay moist brown low plasticity 10 80 39 Sifty clay moist brown low plasticity 15 90 54 SAND very fine Sifty most, light brown SAND very fine Sulty maist, light brown 20 60 92 Clay Sundy Sitty clay modules moist brown 25 80 28 Sand medium red/Brown well sorted most 30 70 Clayey Sand red most, turning more sity sand 8.8 Okyey Sand red moist luming more silty sand ³⁵ – į 60 54

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PROJECT NUMBER 160492.SA.03	BORING NUMBER MW-86	
	SOIL BORING LOG	

ROJEC	7	Loon To	rm Oneration	nal Areas - Momphis	Depot LOCATION Memphis Tenness	ee
LEVAT	ION	304 35 1	eet MSL (TO	C) 304 89 feet MSL	ground) DRILLING CONTRACTOR In State Testing Se	
RILLIN	IG METH	OD AND	EQUIPMEN	TUSED Hollow S	em Auger 4 25 inch ID with CME Sampler	CED 44
				11/2001) START	09/18/2001 ENO 09/24/2001 LOG	GFR Adam Karser (Jacobs) COMMENTS
		JHFACE (FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERVA			PENETRATION		DEPTH OF CASING DRILLING RATE
		RECOVE		TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DRILLING FLUID LOSS
			#/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	TESTS, AND INSTRUMENTATION
			!	6. 6. 6. 6.	OR CONSISTENCY SOIL STRUCTURE.	Corrected FID (ppm
		<u> </u>	 	(N)	MINERALOGY	Contract to gas.
!		!		Used hollow stem	Yellowish ten moist medium-well sorted sand	· 1
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-i		i	1	driffing method no penetration test		
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-i	i	i	l		Medium sand - yellowish lan-moist	
_i	i	i	ŀ		·	
ļ		į		1		i
-i	. !	!		į.	Medium Sand, same as above with small angular gravet, not slup	i
5_		!				
-;	1	50				10
-i	i	i				1
i	į	j		1		
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. !	:	!				
- 1	1	[
i	ì	i	ļ	ì		
o i	i	i	1	1		
- 1	1	60	1		Tannish white/gray medium sixed i moist with small (pravel	10 0
İ		Į	1			
!		!	ļ			
-:		ł	1			
-i		i	ì			
i	ì	i	i			
<u>-i</u>	1	ļ	ļ			
5 _			i .			4.5
:		60	Į.		same more reddish	1
-i	i	i	ŀ			
_i	ì	j	i			
ļ		ļ	i			
-!	!	!	Ī		Reddish yellowish almost no gravel	
		ł	į.		•	
. i	i	i				
' —i	i	65				22
į	i	99				
į	!	!		1		1
-i		!	1	ł		
:		:				
i			1	1	Reddish sand	1
_i	i	Ì		1		1
į		l	1			70
₃ —į	!	65	1	1	Brown Clay (6"), stiff at 65"	
_ ;		} ~~	ł	1	29" of Red. white med. sand moist ino grave	`
-			ł	1		
-i	i	í	1	1		1
i	ī	1	1	1		1
1	1	}]	[Same	1
		}]	1		
ļ		, i	1			1
Ĺ	i		l	1		2.0
- <mark> </mark>	İ	an na	ı	L .		-
· -	1	80	İ	i		
 - -	1	80			SUIT gray/ten sitty clay at 71 /2	\dashv
 - - -	† 	80				\exists
 - - - -	1 1 1 1	80			Stiff gray/ten sifty clay all 71 72 medium fine sand itan moist.	\exists



BORING NUMBER
MW-86
SOIL BORING LOG

PROJECT Long Term Operational Areas Memphis Deput **LOCATION Memphis Tennessee**
 ELEVATION
 304 35 feet MSL (TOC)
 304 89 feet MSL (ground)
 DRILLING CONTE

 DRILLING MFTHOD AND EQUIPMENT USED
 Hollow Stem Auger 4 25 srxh 1D with CME Sampler

 WATER LEVELS
 96 27 feet BTOC (11/2001)
 START
 09/18/2001
 END
 09/24
 DRILLING CONTRACTOR Tri-State Testing Services, Inc. LOGGER Adam Karser (Jacobs) END 09/24/2001 DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) TEST SOIL NAME USCS GROUP SYMBOL COLOR DEPTH OF CASING DRILLING RATE MOISTURE CONTENT. RELATIVE DENSITY RESULTS DRILLING FLUID LOSS 6.6.6.6 OR CONSISTENCY SOIL STRUCTURE TESTS AND INSTRUMENTATION (N) MINERALOGY Conected FID (ppm) 75 65 Grayish white sand some small gravel 19 Same with large grave! Wet Clay Sample collected for VOCs Clay, 1° Sandy Clay Brown/Grey 80 79.5 82 Silty Sand Very Fine light gres 100 122 Clay grey with red mottles Clay still brown 85 90 7 1 sand red to grey fine no gravel mort Sample collected for VOCs Sand light grey to tan (reddesh brown) 90 65 96 and wheelgray with small rocks-pebbles Very Slow down, hard surface Difficulty removing split sporti 95 50 71 Reddish sand with large rocks (1 to 1.25 °) at 96.5 Done for 9/18/01 at 6 30 p m Water table Sand white grey increal top 24" wet 100 45 9/19/01 at 8 45 a.m. 55 Sand with rocks (1/4 to 2 1/2") bottom 4" of sampler Sand same rocks (1/2*) wet Sample collected for TOC 8"Clay grey 105 100 Sand Fine grey 21 most 65 Sity Clay with very line sand moist reddish brown to grey fem. Sity Clay with very tine sund same transitions stiff sitty clamp damp at 110' Broken auger only bored 2.5 Lost approximately 45° of auges in boring 110 _ ater recovered 100

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PROJECT NUMBER	BORING NUMBER			
160492 SA.03	MW-86			
	SOIL BORING LOG			

PROJE	ÇT	Long Te	rm Operation	al Areas Memphis	Depot LOCATION Memphis Tennessee			
ELEVA.	TION	304 35 8	eet MSL (TO	C) 304 89 feet MSL	(ground) DRILLING CONTRACTOR Tri State Testing Services	inc		
DRILLIN	DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4 25 inch ID with CME Sampler							
				1/2001) START		Adam Kaiser (Jacobs)		
		URFACE (F1)	STANDARD	SOIL DESCRIPTION	COMMENTS		
i	INTERVA			PENETRATION				
		RECOVE		TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE DRILLING FLUID LOSS		
1 :			#/TYPE	RESULTS	MAISTURE CONTENT RELATIVE DENSITY	TESTS AND INSTRUMENTATION		
1	1		1	(N) 6.2.2.2.	OR CONSISTENCY SOIL STRUCTURE MINERALOGY	Corrected FID (ppm)		
	-	-		 		33.53		
I -i	i	i				-		
1 !	ļ	ļ .			Sifty (2sy with very line sand damp red brown grey stiff			
1 7		ļ .	i			1		
l i	i	i		1				
115 _	Į	į						
1 :		50		ł				
i i	i	i	l	i		<u> </u>		
-	!	ļ	l	1	Ladandada and bad da	Well at 117 Broken head on split		
1 :		! !	ļ		1 of solid clay grey hard dry	spoon ing problems		
l i			ł		BORING TERMINATED @ 118 FEET BGS	` ` ` ` ` `		
į į						-		
120								
]			1	į		_		
	i		•					
1						-		
-1						-		
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125					•			
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PROJECT NUMBER	BORING NUMBER	
160492.SA.03	MW-88	

SOIL BORING LOG

PROJE	CT	Long Te	rm Operation	al Argas Memphis	Depot LOCATION Memphis Tennessee	
<u>ELEV</u> A	TION	305 15 1	leet MSL (TO)	C1. 305 47 feet MSI	(mound) DRILLING CONTRACTOR To State Texture Senses	s Inc
DRILLI	NG MET	HOD AND	EOUIPMEN	TUSED Hollow S	Stem Auger 4 25 inch ID with CME Sampler	
WATER	BELOW S	5 60 98	reet BTOC (1	1/2001) START	09/20/2001 END 09/21/2001 LOGGER	Jay Parker (Jacobs)
- C-111	INTERVA		<u>F1)</u>	STANDARD	SOIL DESCRIPTION	COMMENTS
1		RECOVE	· PV AV	PENETRATION TEST	50# WWW 19500 0P01 #1 #1 #1 #1	!
		LECTIVE	#/TYFE	RESULTS	SOIL NAME USCS GROUP SYMBOL, COLOR MOISTURE CONTENT RELATIVE DENSITY	DEPTH OF CASING DRILLING RATE
Į.	1			2. 6. 6e.	OR CONSISTENCY SOIL STRUCTURE	DRILLING FLUID LOSS
<u> </u>	1		P	(N)	MINERALOGY	TESTS, AND INSTRUMENTATION
	i	ī	F		One loot blackton and or and	Corrected F1D (ppm) (Soll headspace)
-	!	!		Used notiow stem auger	CLAYEY SILT (10YR4/4) dark yellowish brown most, damp	1
	i	100	i	ciriling method		12
i i	i	i		no penetration les results	1	1
	!	!		1		-
j i	!		ļ		CLAYEY SILY same as above	_
5_	i i	•	ļ			
	!	100	ľ	i		
-		100			i	2.4
_i	i	i	1		1	
1 !	!	!	ļ.,			
1 :	!	ſ	l			i
i i		:			CLAYEY SILT. Name as above shore the in SILT.	_
10	i i	i i	1	ŀ	i	_
-	!!!					_
-i		100			İ	24 _
[i	i i	i				
1 !	!!!					
1 :						-
[-i					SRT (10YR5/6) yellowsh brown damp nonplastic	
15	!!!					
1 :			i			- !
-i	i	100				18
1 !	ļ ļ					
1 ¦						-
! ⁻i	i			:	Recoming motified with grays @ 18 feet bgs	-:
-!	i	ſ			SILTY CLAY (10YR6/1) gray with some motified browns	
20	!				damp: slightly plastic to plastic.	·
	i					_
l -!		100				14 _
I -¦	!	ı				
łi	i		i			
- <u>i</u>	!	- 1	Į.			
l !	!	ı			SILTY CLAY (7 SYR4/6) same as above strong brown mortting	
25	i		ı			-
	i			i	'	-1
-!	!	100	ŀ			2 5
<u> </u>	- 1		1		·	1
[i	1		ı		
l !	!	ı	- 1			_
i :	!		1		SAND light gray 7 5/7/1 some Fe motiles fine to med, loose damp	
30	i	- 1				
⊶ <u>-i</u>	į	- 1				
-;		75	j			4.0
i	i	- 1		ł		
ļį	į	- [J	i		
	!		1	ļ		_1
-1	:	- 1		1	SAND same as above until 37 feet	1
35_	i	- 1	ļ			!
~- }	ļ	75	ļ	Į.		00 -
	i	- 1	1	J		•• [

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PROJECT NUMBER 160492 SA 03	BORING MUMBER MW-88	
	SOIL BORING LOG	

PROJECT Long Term Operation:						
ELEVA'	TION	305 15 <u>k</u>	HELMSL (TOC	305 4 <u>7 feet M</u> SL	(ground) DRILLING CONTRACTOR To State Testing Services, lem Auger 4 25 inch ID with CME Sampler	<u></u>
DRILLIP	NG METH	OD AND	FOUIPMENT	1/2001) START	09/20/2001 END 09/21/2001 LOGGER	Jay Parker (Jacobs)
	ELOW SL			STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERVA			PENETRATION		-
	1 1	RECOVE	PY (%)	TEST	SOIL NAME USCS GROUP SYMBOL, COLOR	DEPTH OF CASING DRILLING RATE
	1		#/IYPE	RESULTS	MOISTURE CONTENT. RELATIVE DENSITY	DRILLING FLUID LOSS
				6.6.6.6	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
	l i			(N)	MINERALOGY	Corrected FID (ppm)
					SAND strong brown 7 SYR S/8 very loose dry medium grained well sorted Black staining in sand tinch thick at 37 feet to 38 feet.	
	•			Used hollow stem auger	SAND brownish yellow 10YR 6/8 Fine well sorted loose damp	_
	!	!		drawing method		-
	i			no penetration test		
40 —	i i			רושפטו		
!	!!	50			TALLE I W. C	00
	:			,	SAND paid yellow fine well sorted loose 2 5Y 8/4	_
j	i i	1				
	!!					-
	!				SAND as above @ 41 feet	-
- 1	i i					
45 _	!!	!		i		
	: :	50				17 _
	i		· ·		•	_
	į į	1			SAND with gravel strong brown 7 6YR 4/6 30% pebbles and gravel	
_	!!!				subrounded dry to damp loose to firm med sand	-
	:				SAND pale yellow 2 5Y 8/2 loose free dry	-
	i i	i		1		
50	• !			t		_
	: :	100				00 _
_	i i	i			Grades to hard mid SAND	_
-	!!!					
	: :				Brown at 53 feet. Black organic P muted throughout	-
	i	i			SAND yellowsh red SYR 4/6 fine to med. loose 10% gravel and peobles. dry	-
	!!!	!			•	i
55 _	!					_
	i i	100	ļ			00 _
-	!!!	}				
-	! :					
_	i i					
	I			•	SAND yellow 10YR 7/6 fine to med fine toose dry well surfed	
_	!!!	!	1	1	,	
60	1	·		Ì		_
	i i	i 80		į		00 _
	!!	!		l		1
l	1 1	:				[
l	i i	i				-
1	!!	!			SAND white 2.5Y 8/1, very fine to line, well sorted, loose dry, trace	_
-	1	!		i	subrounded to rounded gravel	
65_	i :	i				-
ł .	i ļ	80	ŀ			00
	! !	! ~~	•			
l	:	i	}			_
	i i	į	1			
	!!	!			First 2.5 livel lost in recovery, but appeared to be same as above. SAND with	
	:	ł			pebbles and gravel light yellowish brown, 2 SY 6/4. (Ine to coarse	<u> </u>
70	i i	i	l		knose dry pebble/gravel matrix at 20%	1
l ⁻	! !		[0.0
-	:	40		1		
	i	i	1	1		-
1	!!!	!		1		
1	1	:				



PROJECT NUMBER	BORING NUMBER	
160492.SA.03	MW-88	
	SOIL BORING LOG	

PROJECT	Long Te	sm Operation	<u>al Areas - Memphis</u>	Depot LOCATION Memphis Tennessee	
ELEVATION	305 15	feet MSL (TO	C) 305 47 feet MSL	(ground) ORILLING CONTRACTOR Tri State Testing Service:	s Inc
				tem Augus 4 25 inch ID with CME Sampler	
			1/2001) START	09/20/2001 END 09/21/2001 LOGGER	Jay Parker (Jacobs)
DEPTH BELOV		(L1)	STANDARD	SOIL DESCRIPTION	COMMENTS
INTE	RVAL (FT)		PENETRATION		
	RECOVE		TEST	SOIL NAME, USGS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
	1	#/TYPE	RESULTS	MOISTURE CONTENT. RELATIVE DENSITY	DRILLING FLUID LOSS
1 1	- 1		6- 6- 6- 6-	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
			(N)	MINERALOGY	Corrected FID (ppm)
i	i	<u> </u>			
⁷⁵ —	ļ		Used hollow stem	SAND wipebblins yellowish red SYR 4/6 fine to med loose pebblins rounded perbbles <5% day	_
!	75		auger drifting method	proces con my	00
-;	1	1	no penetration les		1
I -i	i	ł	results		_
İ	i			i	
!	_!			Recoming wet with gravel at 78 feet	Sample collected for VOCs
! !	_i			Same as above to 79 feet	
80 _	- 1			SAND very fine most light grey 2.5Y 7/2 loase to firm	
! [∞] - ¦	i	ļ			•
i i	75	1	1		
ļ ļ	ļ				Water table
-!	!	ŀ			<u>-</u>
1 !	- !	į.			
i			l.		Sample collected for TOC
l i	i		f	Same as above	<u> </u>
85 _	j				1
· - !	ļ				i –
l -!	90	1	1		_
I :	-	i	1	SAND with gravel. light grey 2.5Y 7/2 saturated some lines to silt.	
l i	i				-1
_i	j		i		l
!	-i				i -
l -!	!			Same 14 above	l -
90		ı			
I ⁻ i					
l -i	75				_
i i	Ĺ				
<u> </u>	į.				l
1 !	!				
i :	-1	1		Same as above	i
l i	i	!		Opine as autilia	-
95_i	i	Ĭ			
1	!	1			
-!	100	1			
	-		ľ		1
1 7	i] ,	[Clay @ 97 feet	1 · · · · · · · · · · · · · · · · · · ·
l i	i		1		-1
ļ	-1] :	Silty clay grey bended with dark grey	
!!	!]	· · · · · · · · · · · · · · · · · · ·	-
100	1				
	100				
l i	i				-[
i	i	i			
					! <u>"1</u>
i	1			BORING TERMINATED & 102 STEET BGS	
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105 _					.
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PROJECT NUMBER 160492 SA.03	BORING NUMBER MW-92	
	SOIL BORING LOG	

PROJECT LOCATION Memphis Tennessee Long Term Operational Areas Memphis Depot 304 41 feet MSL (TOC): 304 78 feet MSL (ground) DRILLING CONTRACTOR In State Testing Services, Inc. ELEVATION DRILLING METHOD AND FQUIPMENT USED Holkow Stem Auger 4 25 inch ID with CME Sampler 09/25/2001 LOGGER Jay Parker (Jacobs) WATER LEVELS 96 75 from BTOC (11/2001) START 09/24/2001 END COMMENTS DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION PENETRATKIN INTERVAL (FT) RECOVERY (%) DEPTH OF CASING DRILLING RATE TEST SOIL NAME USCS GROUP SYMBOL COLOR DRILLING FLUID LOSS MOISTURE CONTENT RELATIVE DENSITY RESULTS TESTS, AND INSTRUMENTATION 6" 6" 6" 6" OR CONSISTENCY SOIL STRUCTURE Corrected FID (ppm) (Soil headspace) MINERALOGY (N) 5" Asphalt, 6" gravel, Clayey SILT, yellowish red 51 R 4/6 damp Used hollow sten auger dniling method no ponetration tes 00 100 results ame as above 100 00 10 00 100 Clayery SILT, reddish brown 5YR 5/4 with reddish yellow mottling 5YR 6/6 15 00 100 SANDY SILT strong brown 7.5 YR 4/6 vwry line stiff dry 20 00 100 Sandy SILT light brown 7.5 YR 6/3 with dark red mothes, very fine firm, damp 25 0.0 100 Turns to SAND dark red 2.5 YR 4/8 loose fine to med dry SAND red 2.5 YR 4/8 medium to fine well sorted damp loose 30 0 0 50 same as above red 2.5 YR 5/8 35_ 00 50



PROJECT NUMBER	BORING NUMBER	
160492.SA 03	MW-92	
	SOIL BORING LOG	

PHOJE		rang is	um Oberation	ial Areas - Memphi	s Depot LOCATION Memphis Tonnessee	<u> </u>
ELEVA	TION	304 41 1	eet MSL (TO	C), 304 78 feet MS	L (ground) DRILLING CONTRACTOR Tri-State Testing Senece	s, Inc
DRULLII	NG METH	OD AND	EQUIPMEN	TUSED Hollow	Stem Auger 4.25 inch ID with CME Sampler	
				11/2001) START		Jay Parker (Jacobs)
DEPTH		URFACE (FY)	STANDARD	SOIL DESCRIPTION	COMMENTS
1	INTERVA			PENETRATION		i
1	1	RECOVE		TEST	SOIL NAME USGS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
	1		#/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS
	1	i	ļ	6666.	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
		!		(N)	MINERALOGY	Cornicted FID (ppm)
	ļ	ļ .	į.	Used hollow ster		
-	!	!		auger	"	
	:	:		drilling method	SAND yellow 10YR 7/5 fine loose dry	1
	i	i		no ponetration te	4	1
40 —	Ĭ	İ	1	results		1
1	1	50	1	ł		••
ŀ	!	!		1		-:
		:	Ī			
1	•	1				1
1 -	i	1				!
I -	ĺ	Ì]		First half of sample lost. SAND: pale yellow 2.5Y 8/3 med to fine, well sorted	;
45	!	!	1		looke dry trace pebbles and gravel subrounded	
" " –		!	i			
1		50]
1	•	ì			1	<u>-</u>
	i i	j .			1	-
	ļ i]			
]	!!)	1	Į.]	l .
-		ļ i	Ì	1		1 1
50					Same as above no pebbles or gravel	Į.
1 ~ · :						oa –
i	i i	100				[
		ľ	1			I
-!	!!!		1			
ł -:	!			l		
1 1				l .	Same as above	!
l i	i i					
55	i i					
!					Grades to brownish yellow 10YR 6/6 damp. Becoming coarser sand, with	oo -
1 !		90	1		pebbles and gravel at 56.5 feet. fine to coarse stand. Subungular to	_
1 :					subround gravel and pebbles	
1 1				1		
I -i	i					_]
l i	ı i			1	SAND yellow brown 10YR 5/8 well sorted fine loose damp]
-!	!!!	ì			Gravel and pebbles grade away	-
60 _	. !				and the same of th	l
-	•			ŀ		oo —
-i	:	90			İ	<u>.</u> l
l i	i		,	ļ	j	
j ⁻i	į	ľ			i	
] -!	1	İ			Sandy CLAY with gravel and set, very pule brown mottled with white 2 5Y 8/1]
!	!			l		
- <u>'</u>	!			ĺ	i e	-
65_	ï	- 1		ł	1	J
	i	Ì		l		00 —
[i	ĺ	80			SAMD under 2 SV 76 for Bours date and a second	1
	į	l		l	SAND yellow 2 5Y 7/6 fine floorer didy well sorted	
1 !	!	ł		Ì		-
-¦	;	i			 	_
1 i	i	ŀ			Same as above damp	.
l i	i	ŀ				-1
70 _	į			ł		.
l į	İ					00 ^{~-}
¦ -!	ŀ	40				-
;	- !	ľ				·
l i	i				Same as above	į
–j.	i					[
1	1	- 1			i	1

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PROJECT NUMBER	BORING NUMBER MW-92	
160492 SA 03	W107-32	
	SOIL BORING LOG	

PROJE	Cı			Areas Memphis		.
ELEVA	TION	304 41 6	eel MSL (TOC) 304 78 feet MSL	(ground) DRILLING CONTRACTOR To State Testing Services	<u>, Inc </u>
				1/2001) START	tem Auger 4 25 inch ID with CME Sampler	Jay Parker (Jacobs)
	BELOW SI	_		STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERVA			PENETRATION		
	1	RECOVE	RY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
		1 .	#/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS
				ee. e. e.	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION Corrected FID (ppm)
	<u> </u>			(N)	MINERAL OGY	Canada Pib (ppii)
75	! :			Used hollow stem		
	i i	75		aug/v drilling method		
	!!	/3		no nenetration test	Grades to sity SANO wigravel yellowish brown 10 YR 5/8 small gravel and	<u> </u>
-	: :			results	pebbles angular wet sof Wei @ 77 feet	Sample collected for VOCs
	i!					
	! -					
-	i i	i				1
80	!!	!				_
	:	75			Grades slowly from the sitty sand wigravel to SANDY SILT at 80 5 feet	1
-	i i					
_	!!				CLAY yellow 10 YR 7/6 very plastic stiff	1
-	ii	i			Clayey SILT brownsh yellow 10YR 6/8 med stiff med plastic, damp	-
	!!				omja, acc. domos, jones to to to the transfer of the	
ec .	i i					:
85	į					. –
		90				-
i	i	i i				_
	!!	!			SAND white 10YR 8/1 fine loose damp well sorted	
-	¦¦]
ļ i	i i	i				
90	!!	!				l _
	ii	,,				ŀ
-	!!	75				1
	i i				As above SAND white to 92 5 feet SAND brownish yellow 10YR 6/6 loose	
	!!	.			line sume gravel dry	-
	!				Same brownish yellow SAND as above with more gravel gravel at 5 to 10%	
i	i i	i			damp to moist	
95 _	!!					-
	ii	60			<u> </u>	Sample collected for VOCs
!	!!				Sample at 96 to 98 appears to be well to safurated	
	: :					Water Table
-	ii				GRAVELLY SAND dark yellowish brown 10YR 4/6 fine to coarse sand	j 7
-!	. !				50% gravel wet	-
100						
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	!!	١ ١	i		CLAY grayish brown 10YR5/2 with blackush bands stiff medium plastic race sand]
-1	;¦				SAND light gray 2 SY 7/12 fere to very fine loose	1
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105 _		l				j - i
i	į				Wel @ 105 5 feet, durker gray sand from 103 to 105 5 feet	_
	!!				· · · · · · · · · · · · · · · · · · ·	Sample collected for TOC
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_	İ	l		ı	Sand is saturated	{
1	. !	l			Sitry CLAY (poks the clay at 108 feet SILTY CLAY graysh brown 10YR5/2 with blaclush pieces stiff medium plastic	
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CH2MHILL

PROJECT NUMBER	BORING NUMBER		
160492.SA 03	MW-92		
	SOIL BORING LOG		

			Areas Memphis			Memphis Tennessee	
ELEANIHOW _	304 41 feet	MSL (TOC), 304 78 feet MSL	(ground)	DRILLING CONTRACTOR	<u>Tn-State Testing Service:</u>	s Inc
DRILLING MET	HOD AND EC	THEMPILE	USED Hollow S	tem Auger 4 25 inch	ID with CME Sampler		
			/2001) START	09/24/2001	END 09/25/2001	LOGGER	Jay Parker (Jacobs)
DEPTH BELOW S	URFACE (FT)		STANDARD		SOIL DESCRIPTION		COMMENTS
INTERVA			PENETRATION	<u> </u>			
ł I	RECOVERY		TEST	LOW MANE MESSES	COLOR CYALBOX COLOR		DENTALOS 648440 8044 445 844
	INFO OVER T	YPE			GROUP SYMBOL COLOR		DEPTH OF CASING DRILLING RATE
1 1	j ""	''''*	RESULTS		IT RELATIVE DENSITY		DRILLING FLUID LOSS
f l		1	6-4-6-6-	OR CONSISTENCY	SOIL STRUCTURE		TESTS, AND INSTRUMENTATION
	<u>. </u>		(N)	MINERALOGY			Corrected FID (ppm)
1 1	1						1
!	!		Used hollow stem	SILTY CLAY graymin t	zown 10YRS/2 with blackish piece	es stiff medium plasac	1
l !	!		auger drifting method				
1 -1	1 1		no penetration test	BORING TERMINATE	D 60 102 5 FEET BGS	~	-
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PROJECT NUMBER 160492 SA 03	BORING NUMBER MW-93A (Replaced by MW-93B)	•
	SOIL BORING LOG	

PROJECT	Long Te	erm Operation:	al Areas Morr	his Depot LOCATION Memphis Termessee	
ELEVATION	Not App	acable .		DRILLING CONTRACTOR To State Testing Service	s, <u>inc</u>
				w Stem Auger 4 25 inch ID with CME Sampler	 ., .,
WATER LEVELS		Not Applicable			Adam Karser (Jacobs)
DEPTH BELOW S		FT)	STANDAR		COMMENTS
INTERVA			PENETRATI	9	
	RECOVE		15.51	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE DRILLING FLUID LOSS
		a/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	
			6.6.6.6	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
	<u> </u>	├	(N)	MINERALOGY Clayey sat-brown dry stat	Corrected FID (ppm) (Soll headspace)
!!	!		Used hollow:	em.	(**************************************
	i		auger	. i	0.8
- i i	100	l	drilling met no penetratio	tos	· · ·
_1	ı	ł	results		
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- i	i			Sand reddish med coarse dwise most gravelly (smell)	
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ii	1			Sand <5% smalt gravel ~1/2" in size. Iransitioning into more gravel: 40%	.
!!!				Sand <5% smar graver ~1/2" er size litarismoneng into more graver =0% 1/2 to 1" er size	_
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PROJECT NUMBER
160492.SA 03
BORING NUMBER
MW-93A (Replaced by MW-93B)

SOIL BORING LOG

PROJECT Long Term Operational Areas - Memphis Depot **LOCATION Memphis Tennessee** DRILLING CONTRACTOR Tri-State Testing Services, Inc. **ELEVATION** Not Applicable DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4 25 Inch ID with CME Sampler Not Applicable START 09/25/2001 END 09/27/2001 LOGGER Adam Karser (Jacobs) WATER LEVELS COMMENTS DEPTH BELOW SURFACE (FT) SOIL DESCRIPTION STANDARD INTERVAL (FT) PENETRATION RECOVERY (%) DEPTH OF CASING DRILLING RATE TEST SOIL NAME USCS GROUP SYMBOL COLOR MOISTURE CONTENT. RELATIVE DENSITY DRILLING FLUID LOSS RESULTS TESTS, AND INSTRUMENTATION 6. 6. 6. 6. OR CONSISTENCY SOIL STRUCTURE Corrected FiD (ppm) (N) MINERALOGY Used hollow sten auger dniling method no penetration te nd reddish coerse loos most small gravel 5% 1/4 1/2 4" sift zone 40 results 13 65 sand red coarse medidense most no gravel, more tannish lims densa 45 90 and reditaringh charse medidense most 50 90 ne w/smu≅ gravel <5% 1/4° 55 00 100 and redition med med-dense most no gravel fore coase, some large rocks 1° to 1, 1/2 °, small, gravel <1/4°. 60 06 100 Aure gravel: 5% 1/4": 1/2" large gravel:60% (1") 65 Sand Lan m to 1.1/2* 90 m dense damp with small gravel 20% 30% 1/4" 1" up 70 90 nd tan/white five loose damp



PROJECT NUMBER	BORING NUMBER
160492 SA.03	MW-93A (Replaced by MW-93B)

SOIL BORING LOG

PROJECT LOCATION Memphis Tennessee Long Term Operational Areas Memphis Depot ELEVATION Not Applicable DRILLING CONTRACTOR In State Testing Services, Inc. DRILLING METHOD AND EQUIPMENT USED. Hollow Stem Auger 4.25 inch ID with CME Sampler WATER LEVELS Not Applicable START 09/25/2001 FND 09/27/2001 LOGGER Adam Kaiser (Jacobs) DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) TEST SOIL NAME USCS GROUP SYMBOL COLOR DEPTH OF CASING DRILLING RATE RESULTS MOISTURE CONTENT RELATIVE DENSITY DRILLING FLUID LOSS 6.4.6.4. OR CONSISTENCY SOIL STRUCTURE TESTS AND INSTRUMENTATION MINERALOGY (N) Corrected FID (ppm) 75 Used hollow stem 09 auger drifting method no penetration les 100 results 80 12 100 nd redicoarse and tan fine loose damp 85 100 14 ore coarse: 10:20% gravel 1/2" to 1" in size 90 90 17 l ets gravni 95 90 0.4 More gravel: 50% (1/2" to 1 1/4") 100 0 Sample collected for VOCs Vel emmented iron stone sand reddish tan medium to course grained saturated 100 105 BORBING, TERBURNATEO (§) 105.5 feet.
Thi State could not advance the augms pusit 105.5 feet bincause of "confusionments" A division was made by Thi-State to abandon the soil boring MW 93A. The new soil boring (MW 93B) was offset approximately 25 feet west of MW 93A. 110



PROJECT NUMBER	BORING NUMBER	
160492.SA.03	MW-93B	
	SOIL BORING LOG	

PROJE				<u>ial Areas</u> Memph <u>is</u>		
<u>ELEV</u> A	TION	294 03	feet MSL (TO	C) 294 31 font MSt	(ground) DRILLING CONTRACTOR To State Testing Service	ars, Inc
DRILLI	NG METI	HOD AND) FQUIPMEN	TUSED Hollow S	tem Auger 4 25 inch ID with CME Samplur	
WATER	RLEVELS	5 102 4	5 feet BTOC (11/2001) START	09/25/2001 END 09/27/2001 LOGGER	Adam Keiser (Jacobs)
DEPTH	BELOW S	URFACE	(FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
1	INTERV	u (FI)		PENETRATION		· · · · · · · · · · · · · · · · · · ·
ł	1	RECOVE	RY (%)	1651	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
1	1		s/TYPE	RESULTS	MOISTURE CONTENT. RELATIVE DENSITY	DRILL ING FLUID LOSS
			i	6. 9. 9. 9.	OR CONSISTENCY SOIL STRUCTURE.	TESTS, AND INSTRUMENTATION
	↓	<u> </u>	<u>i</u>	(N)	MINERALOGY	Corrected FID (ppm)
	i	i				(Soil headspace)
-	!	!		auger	Refer to soil buring log. MW 93A, for soil lithologies from ground surface to 90.5 feet.	
		!		drilling method		1
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PROJECT NUMBER 160492 SA 03	BORING NUMBER MW-93B		
	SOIL BORING LOG		

PROJE	CT	Long To	m Operationa	el Areas <u>Me</u> mphis	Depot LOCATION Memphis Tonnessee	. <u>— -</u> — —
FLEVA	TION	294 03 fe	NO MISL (TOC) 294 31 feet MSL	(ground) DRILLING CONTRACTOR In State Testing Service:	
DRILLI	DRILLING METHOD AND EQUIPMENT			USED Hollow St	tern Auger 4 25 inch ID with CME Sampler	
WATER	LEVELS	102 45	feet BTOC (1	1/2001) START	09/25/2001 END 09/2//2001 LOGGER	Adam Keiser (Jacobs) COMMENTS
DEPTH		URFACE (I	-T)	STANDARD	SUIL DESCRIPTION	COMMENTS
l	NTERVA			PENETRATION		DEPTH OF CASING DRILLING RATE
{	1	RECOVE		1657	SOIL NAME USCS GROUP SYMBOL COLOR	DRILLING FLUID LOSS
1	ł .		#/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	TESTS, AND INSTRUMENTATION
1	f			6.4.4.6.	OR CONSISTENCY SOIL STRUCTURE	Corrected FID (ppm)
—	<u> </u>	<u> </u>		(N)	MINERALOGY	
Į.	!	!		Used hollow stem	Refer to soil boring log: MW 93A, for soil bithologies from ground surface to 90.5 feet	
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	PROJECT NUMBER 160492.SA.03	BORING NUMBER MW-93B
CH2MHILL		SOIL BORING LOG

PROJECT ___ Long Term Operational Areas Memphis Dispot LOCATION Memphis, Tennessee ELEVATION 294 03 feet MSL (TOC) 294 31 feet MSL (ground) DRILLING CONTRACTOR Tri-State Testing Services, Inc. DRILLING METHOD AND LOUIPMENT USED Hollow Stem Auger 4.25 inch 1D with CME Sampler LOGGER Adam Keiser (Jacobs) WATER LEVELS 102 45 feet BTOC (11/2001) START 09/25/2001 END 09/27/2001 DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) TEST SOIL NAME USGS GROUP SYMBOL COLOR DEPTH OF CASING DRILLING RATE RESULTS MOISTURE CONTENT. RELATIVE DENSITY DRILLING FLUID LOSS <u></u> ይዲዲድ OR CONSISTENCY SOIL STRUCTURE TESTS, AND INSTRUMENTATION Corrected FID (ppm) (N) MINERALOGY 75 Used hollow sten Refer to soil boring log: MW 93A, for soil kihologies from ground surface to 90.5 feet auger drilling method no prinetration tes results 80 85 and reddish tank med coarse med dense damp <5% gravel (1/4" to 3/4") 90 _ 85 09 nore gravel 10 to 15% Gravelly Sand more gravel 30% up to 1" most 95 75 0 7 50% gravet 1 1/2" and less gravel to no gravel red and tan line dense morst 100 _ 90 Sample collected for VOCs Water Tuble Sand reddish (8" gray) fine saturaled 105 100 Sample collected for TOC Clay grey dense dry Clay grey dense dry 110 _

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PROJECT NUMBER	BORING NUMBER	
160492 SA 03	MW-93B	
	SOIL BORING LOG	

PROJE	LT.			al Areas Memphis			
FLEVA	TION	294 03 f	<u>rei M</u> SL (TOC	C) 294 31 feet M <u>SL</u>	(ground) DRILLING CONTRACTOR Tri-State Testing Services	Inc	
	DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4 25 inch ID with CME Sampler WATER LEVELS 102 45 leet BTOC (11/2001) START 09/25/2001 END 09/27/2001 LOGGER Adam Keiser (Jicobs)						
WATER	CIFVELS	URFACE (reet BTOC (1		09/25/2001 END 09/27/2001 LOGGER SOIL DESCRIPTION	Adam Keiser (Jecobs) COMMENTS	
	INTERVA		F1)	STANDARD	SOIL DESCRIPTION	(XAMMENTS	
1	IN IE KV			PENETRATION	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE	
ł	1	RECOVE	RY (%) B/TYPE	IFSY RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS	
		ĺ	2/11/2	6. 6. 6. 6.	OR CONSISTENCY SOIL STRUCTURE	TESTS AND INSTRUMENTATION	
]	l	j	(N)	MINERALOGY	Corrected FID (ppm)	
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ł		ľ		results	BORING TERMINATED @ 113 5 FEET BGS	_	
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PROJECT NUMBER	BORING NUMBER	
160492.SA 03	MW-94	
	SOIL BORING LOG	

<u>PROJE</u>		_Long Te	noit <u>eraqO mw</u>	ul <u>Areas</u> Me <u>mp</u>	his Depot LOCATION Memphis Tennessee	
ELEVA	TION	296 94 (fret MSL (TO)	C), 296 95 feet N	ISI. (ground) DRILLING CONTRACTOR, To State Tentre Sender	s, Inc
DRILLI	NG MET	HOD AND) EONILMEN.	T <u>US</u> FD Ho <u>lo</u>	V Stern Auger 4 25 inch (D with CMF Samoler	
WATER	₹ LEVELS	5 107 07	/ feet BTOC (11/2001) STAF	T 09/25/2001 END 09/27/2001 LOGGER	Jay Parker (Jacobs)
DEPTH		URFACE (<u>m</u>	STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERV			PENETRATIO	· · · · · · · · · · · · · · · · · · ·	
ĺ		RECOVE		TEST	SOIL NAME USGS GROUP SYMBOL COLOR	DEPTH OF CASING ORILLING RATE
1		l	#/TYPE	RESULTS	MOISTURE CONTENT: RELATIVE DENSITY	DRILLING FLUID LOSS
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	Щ.	Ь	↓ _	(N)	MINERALOGY	Corrected FID (ppm)
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-:	1	i		Í	Same as above slightly more clay content slightly plastic med stiff	
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PROJECT NUMBER 160492.SA.03	BORING NUMBER	MW-94	
,	SOIL BOF	RING LOG	

PROJE				Areas Memphis		
ELEVA1	IG METH	<u>/9</u> 0 94 R	FOLIPMENT	JUSED Hottow St	tern Auger 4.25 inch ID with CME Sampler	
WATER	LEVELS	107.07	feet BTOC (1	1/2001) START	09/25/2001 END 09/27/2001 LOGGER	Jay Parker (Jacobs)
	LLOW SI			STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERVA			PENETRATION		
		RECOVE	RY (%)	TEST	SOIL NAME USGS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
			ø/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS
				6.4.4.4.	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
				(N)	MINERALOGY	Corrected FID (ppm)
				Used hollow slem		<u>.</u> .
			!	ande.	SAND as above reddish yellow 7.5 YR 7/6 med very loose dry	
_			i I	drilling method		
	i		!	no penetration test		
40 _	j i	İ	į	results		00 —
	!!!	60	F			
			į			
l i	i					
_[i!		[-
!	!!!			1		_
	1		l			1
45	i	i	ŀ		Gravelly SAND as above, with gravel and pubbles 50% mix. Sample wits only	_ 00 -
	j j	50			from 45.5 to 48 due to problems with ng	1
!	!!!	_~			Becomes a pebbly SAND 7 SYR 4/6 dry loose	
		! !				1
	i					1
i -i					Pebbly SAND as above to 49.5 feet	
	!				Sharp change to SAND yellow 10YR 7/6 fine very loose dry	-
50	}				Ship Change to Grand John W. 1911. 110 mar 121/ and 191/	
i	j i					0 0
- !	!!!	100				1
	}					-
-	1					_
i -i	ı——-	1			Gradus to brownish yellow: SAND: yellow 10YR 7/8; med to fine, well sorted	
!	!				very loose dry	-
55 _	1					_
33 -	i i				Grades coarser sand to 58 fort	0.0
_!]	100				-
i :						_
-	1				Pubbles at 57 to 58 feet	1
	ii	İ	ŀ		Gravelty SAND as above yellow 10YR 7/6 med to coarse peobles 40%	-
!	!!!	į			toose damp	_
-	}					
60	i					00 -
ľ	j j	90	i I			
!!	!!!]]
! :	! !	! !				
1	ii					-
l i	!!				Gradus down to pebbles ino gravel	[
	!!	l 				l
65_						,
	j				As above to 65.5 moist. Casivel replaces pebbles, rounded to submunded	
	!!!	90			pose grub	·
_!	!!!	! !				j -
]	1	! 				l .
l i	ii	l			Gravetly SAND strong brown 7 5YR 5/8 Coarse loose damp gravef approx	ĺ
!	!!	!			10% of matrix. New pebbles	-
70	}					_
٠٠- ۱	i i	i				00
l i	i i	65		1		
!	!!!	l !		[-
'				ŀ	Grades to a SAND very pale brown 10YR 8/2 fine loose dry	
-i	ii	İ	l '	1	Same fele sand as above -yellow 10YR 7/6	· ·
I :	1 1			1		i



PROJECT NUMBER	BORING NUMBER	·	_
160492.SA 03	MW	N-94	
			_

PROJE FLEVA		Long Te	erm Operation	al Areas Memphis		
DRILLI	FLEVATION 296 94 feet MSL (TOC), 296 95 feet MSL (ground) DRILLING CONTRACTOR Tin-State Testing Services, Inc. DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4 25 such ID with CMF Sampler					<u></u>
WATER	マ しEVEL	S 1070	7 feet BTOC (11/2001) START	09/25/2001 END 09/27/2001 LOGGER	Jay Parker (Jacobs)
юсетн	BELOW S	URFACE	(FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERV	AL (FT)		PENETRATION		
1	i	RECOVE	ERY (%) MIYPE	1651	SOIL NAME USCS GROUP SYMBOL, COLOR	DEPTH OF CASING DRILLING RATE
			WI TPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	ORILLING FLUID LOSS
		ļ	1	6. 66. -6.	OR CONSISTENCY SOIL STRUCTURE MINERALOGY	TESTS, AND INSTRUMENTATION
	:	+		. (17)	MINERALOGY	Corrected FtD (ppm)
75 _	i	i	1	Used hollow stem		.
ł	!	90	ŀ	auger dnilling method		00 -
_) 1	! **		no penetration les		
-	i	i	ł	results		i
	!	!	1	ļ		
	!	1	F	ľ	Sity CLAY brownish yellow 10YR 6/8 plastic fine soft damp to most 1" thick	- I
_	i	i		1	SAND yellow 10YR 7/6 fine loose dry some gravet, subrounded	1
80 _	į	į	Į.	1		i l
	!	l 1 90				00 -
1	i	1 30		j		[i
1 -	į	i				ļ
	!	!	ł			
-	!	•	l .		Grading to brownish yellow 10YR 6.8 and no graver dump to moss	-!
-i	i	i			Same as above with gravel	<u> i</u>
85	!	!				
1 :	!		ł I			00 -
1 1	ł	100				1
<u>l j</u>	i	i	l :			
1 !]	!	j		1 inch city band, no water above	<u>-</u>
l i	`	ł	1		No gravel as above	1
į i	i	i			SAND pale yellow 2.5Y 8/2 hns loose dry some subrounded gravets	
90		!	Į l		-	i
l '' '		1	ĺ			
-i		100				,
!		! .	i]
l ⁻i					Same as above damp	ľ
1	ı]	Ì		Owner as autore (gamp	
95 [!					-[
! ~~-¦	j					11
.i	i	75		1		°° -
l!				Į.		
						! - !
l i						
!!			1	Ī	Gravelly SAND yellow 10YR 7/6 line loose dry 20% gravel	1
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100 -	i	65				Į
_i	į	ا د				00
!	!					
-:	:	l	ŀ	j		<u>.</u> l
l i.	i	- 1	1			
ĺ	Ĭ	ŀ		ŀ	less gravely. SAND pole yellow 2 5Y 8/2 fine well sorted loose dry	1
-	. !	l	- 1	ľ		-l
105 _	i	1	ĺ	ļ		ı
į į	i	75		I		00 -
<u>-i</u>	. !	- 1	ŀ	į	j	4
-	!	I	1	l	No. 11	
i	i	ļ		į.	Net moved coarse sand	Water Table
Į į.	1	j	į	ŀ		Sample collected for VOCs
!	!]	1	1.	Same as above, suturated	_
110_				ľ	recine on warren. Hellin eller	}
į	į	100	I		No CLAY often value 2 SY 6/1 at 2/1 instrument 110 F	Sample collected for TOC

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PROJECT NUMBER 160492.SA.03	BORING NUMBER MW-94	
	SOIL BORING LOG	

PROJE	CT	Long Ter	m Operationa	<u>al Areas Mo</u> mphes (Depot LOCATION Memphis Tennessee	
CL CVA	TION	206 04 6	MSL (TOC	1) 296 95 Inet MSL	(oround) DRILLING CONTRACTOR Tri-State Testing Service:	i, In <u>c</u>
DRILLI	NG METH	OD AND	EQUIPMENT	LUSED Howlow St	em Auger 4.25 inch ID with CME Sampler	
WATER	LEVELS	107 07	feet BTOC (1	1/2001) START	09/25/2001 END 09/21/2001 LOGGER	Jay Parker (Jacobs)
	BELOW SI			STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERVA			PENETRATION	<u> </u>	
l		RECOVE	RY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
i	i	TO COTE	ø/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS
ĺ	l		,	6. 6. 6. 6.	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
•	ŀ		1 1	(N)	MINERAL OGY	Corrocted FID (ppm)
1	!	}	i !	Used hollow stem	Clay grey still] -
_	•	i	,	auger drilling method		
1 -	i	i		no penetration test	Clau at above	
	i	i	1	results	Cally as active	-
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PROJECT NUMBER	BORING NUMBER	•
160492.SA.03	MW-96	
	SOIL BORING LOG	

Long Term Operational Areas - Memphis Depot **PROJECT** LOCATION Memphys Tennessee
 ELEVATION
 289 02 feet MSL (TOC), 289 67 feet MSL (ground)
 DRILLING CONTI

 DRILLING METHOD AND EQUIPMENT USED
 Hollow Stern Auger 4 25 inch 1D with CME Sampler

 WATER LEVELS
 83 02 feet BTOC (11/2001)
 START
 09/27/2001
 END
 09/27/2001
 DRILLING CONTRACTOR Tri State Testing Services Inc. 09/28/2001 LOGGER Jay Parker (Jacobs) DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) TEST SOIL NAME USCS GROUP SYMBOL COLOR DEPTH OF CASING DRILLING RATE #/TYPE RESULTS MOISTURE CONTENT RELATIVE DENSITY DRILLING FLUID LOSS 6.-6. 2. 2. OR CONSISTENCY SOIL STRUCTURE TESTS, AND INSTRUMENTATION MINERALOGY Corrected FID (ppm)
(Sall headspace) Clayery SILT: reddish brown SYR 4/3: damp, staff, organics Used hollow sten auger drilling method no penetration tes results 100 00 ime as above, no organica, some gray mottles in places. 75 00 ne as above dry more gray mottles, slightly more sit content 10 100 00 Same as above to 13.5 SAMD reddish brown 2.5 YR 4/4 with light reddishbitiwn mothiis. damp loose fine 15 75 00 SILTY SAND light red 2.5 YR 6/6 ined loose moist to wet 20 100 00 SAND light red 2 5YR6/6 medium grained loose most to wet 25 55 4 inches of CLAY SAND reddish yellow 7 5YR 6/8 line louse dry SAND, as above, with interbeds of dense, hard day CLAY dense, followed by a thin layer of SAND ...AY dense SAND same at above CLAY 4" thick, dense SAND same as above 30 50 SAND reddish yellow 7.5YR 6/6 fine to med loose damp trace probles ³⁵ — 50 0 0



ROJECT NUMBER 160492.SA 03	BORING NUMBER MW-96	
	SOIL BORING LOG	

PROJECT Long Term Operational Areas Memphis Deput LOCATION Memphis Tennessee ELEVATION 289 02 Irest MSL (TOC) 289 67 feet MSL (ground) DRILLING CONTE DRILLING METHOD AND EQUIPMENT USED Hollow Stern Auger 4 25 inch ID with CME Sampler DRILLING CONTRACTOR In State Testing Services, Inc. LOGGER Jay Parker (Jacobs) WATER LEVELS 83 02 feet BTOC (11/2001) START 09/27/2001 END 09/28/2001 COMMENTS SOIL DESCRIPTION DEPTH BELOW SURFACE (FT) STANDARD INTERVAL (FT) PENETRATION DEPTH OF CASING DRILLING RATE SOIL NAME BISCS GROUP SYMBOL COLOR RECOVERY (%) TEST DRILLING FLUID LOSS MOISTURE CONTENT, RELATIVE DENSITY A/TYPE RESULTS TESTS, AND INSTRUMENTATION 6. 6. 2. 4. OR CONSISTENCY SOIL STRUCTURE Corrected FID (ppm) MINE RALOGY Used hollow sten Gravetly SAND strong brown 7 SYR 5/8 fine to med to cuarse subangular gravet gravet 100% SAND reddish yellow 2 SYR 6/8 augry drilling method no penetration tes 40 results 100 ine loose most SAND yellow 10YR 7/8 fine loose damp to dry 45 00 100 ne as above: brownish ynllow 13YR 6/6 50 00 90 CLAY pale yellow 2 5Y 7/4 plustic, soft, damp. Clay was at end of shoe. 6" LAY as above to 54.5 SANU strong brown 7 5YR 5/6 med to course Inonemoist to well, trace pubbles 55 00 90 Pebbly SAND very pale brown 10YR 7/4 med to coarse pebbles and trace gravet subangutar loose moist 60 04 75 Sample collected for VOCs Wet SAND at 62 and 62 5 feet Same as above, wel, some that interbedded Clays very coarse sand and rounded pea gravels 65 75 Sand becomes finer with pebbles rounded imned SAND pale yellow 2.5Y 8/2 fine loose dry 70 100 Same as above, brownish yellow 10YR 6/6



PROJECT NUMBER	BORING NUMBER	
160492.SA 03	MW-96	
	SOIL BORING LOG	

ELEXA		200,02	TO OTO	ar Areas Memphis				mph <u>is Tennessee</u>		
PLEY-	TION	289 UZ :	OCT MSI (ICA	C)_289 67 frei MSL	(ground)	DRILLING C	ONTRACTOR Tri	State Testing Service	s, Inc	_
UKILL	ING ME II	100 AND	PEONINEMEN	TUSED Horlow S	<u>item Auger 4_25 inch I</u> D i	with CME Sar	mpler			_
WALE	BELOWS	5 63 Uz	teet BTOC (1	1/2001) START	09/27/2001		09/28/2001	LOGGER		
μæ			FT)	STANDARD		SOILU	ESCRIPTION		COMMENTS	
)	INTERV			PENETRATION	I			_	T	
1	1	RECOVE	RY (%)	TEST	SOIL NAME USCS GRO				DEPTH OF CASING DRILLING RATE	
Ì	İ	[M/TYPE	RESULTS	MOISTURE CONTENT I				DRILLING FLUID LOSS	
		l		6.6.6.6.	OR CONSISTENCY SOL	LISTRUCTURE	Г		TESTS, AND INSTRUMENTATION	
	ļ	<u> </u>		(N)	MINERALOGY				Corrected FID (p.	pm)
75	<u> </u>	!		Used hollow stem	1			_		
] '	;	:	ļ	Ackger Storm	i					_
	-i	85	i	draffing method						
	İ	Ĭ		no penetration tes results						
	ļ.	ļ.		resurs	CLAY layer 4°				4	
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	:	ľ	l		Grades to med sand, same	ras above pele	r yellow 25Y 8/3 fine I	loose dry	1	•
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	ï	1							Sample collected for VOCs	
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		i			SAND as above subtrated	med to course			Sample collected for TOC	
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		I	1		Same yellow day then the	rest is gray rigi	y with black bands	i		-
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PROJECT NUMBER 160492.SA.03	BORING MUMBER MW-97	
	SOIL BORING LOG	

	PROJECT Long Term Operational Areas Memohis Depot LOCATION Memohis Tennessee ELEVATION 297 44 feet MSL (TOC), 297 70 feet MSL (ground) [NRILLING CONTRACTOR To State Testing Services Inc.						
ELEVA"	TION	297 4 <u>4 f</u>	COLUBATION	(), 297 70 fect MSL	(ground) DRILLING CONTRACTOR To State Testing Service tom Auger 4 25 inch ID with CMF Sampler	<u> </u>	
WATER LEVELS 101 25 feet BTOC (1/2001) START	10/01/2001 FND 10/03/2001 LOGGER	Adam Karser (Jacobs)	
DEPTH (BELOW S	JRFACE (FT)	STANDARD	SOIL DESCRIPTION	COMMENTS	
	INTERVA			PENETRATION			
		RECOVE	RY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE	
{			9/TYPE	RI-SULTS	MOISTURE CONTENT. RELATIVE DENSITY	DRILLING FLUID LOSS	
1			j	6.4.4. 6.	OR CONSISTENCY SOIL STRUCTURE	TESTS AND INSTRUMENTATION	
			<u> </u>	(N)	MINERALOGY	Corrected FID (ppm) (Solf headspace)	
	ī	i "		t lead hollow stern	Asphall Clayey SILT brown dry stifl	15057155545557	
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		100	[i	drilling method			
	j	i		no penetration test results		_	
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1 7	i	j			SAND red coase dense damp some gravel 10% 1/4" to 1/2" more gravel 50% 1/2" to 2"		
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		l L			SAND red medicoase dense damp no gravel	_	
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1	1	i			2000 At 100 and 4000 400 and 500 100 1/47		
35_	i i	70	}		SAND reddish/orange med med dense damp small gravel 5 to 10% 1/4"	25	
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PROJECT NUMBER	BORING NUMBER	
160492 SA 03	MW-97	

PKUJE				<u>al Areas</u> Memphis		<u> </u>
	TION	297 44	feet MSL_(TO	C) 297 70 feet MSL	(ground)DRILLING CONTRACTOR _Tri State Testing Se	arvices Inc.
DRILLI	NG METI	HOD AND	D EQUIPMEN	TUSED <u>Hollow</u> S	item Auger 4:25 inch ID with CME Sampler	
				11/2001) START	10/01/2001 END 10/03/2001 LOGO	GER Adam Keiser (Jacobs)
DEPTH	BELOW S		(FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
1	INTERV			PENETRATION		
		RECOVE		TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING ORILLING RATE
	į	l	#/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS
	ŀ	l	i e	6666.	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
				(N)	MINERAL OGY	Corrected FID (ppm)
	1	1				
1 -	i	!		Used hollow stem auger	ļ	
	!	!	1	drilling method	SAND redds/vlun med/fine loose damp no gravel	1
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40	i	i	1	results		
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li	i	ľ			SAND tan coarse med damp to 20% gravef 1/4 to 3/4" rounded	-
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	- !	100	ı	j	SAND tan fine loose damp no gravel	20
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PROJECT NUMBER 160492 SA.03	BORING NUMBER MW-97	
	SOIL BORING LOG	

PROJE	CT	Long Ter	m Operations	al Areas Memphis	Depot LOCATION Memphs Tennessee	<u> </u>
ELEVA	TION	297 44 ft	et MSL (TOC), 297 70 feet MSL	(ground) DRILLING CONTRACTOR Tin State Testing Services	_Inc
					tem Auger 4 25 inch ID with CME Sampler	Adam Kaiser (Jacobs)
				1/2001) START STANDARD	SOIL DESCRIPTION	COMMENTS
DEPIN	INTERVA		1)	PENETRATION	332223	
l		RECOVE	PY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
		KECOVE.	#/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS
	,		· -	6.6.6.	OR CONSISTENCY SOIL STRUCTURE	TESTS AND INSTRUMENTATION
1				(N)	MINERALOGY	Corrected FII) (ppm)
75 —	!!	!		Used hollow stem	SAND grey line those damp	13 -
j _		95		draling method		
1 :	i i	i		no penetration test results		
1	!!					
1		}		:		!
	i i	j			6°CLAY grey, fem, damp	-
.]	!!	!				
80	:	}				0.0
1 :	i i	100			SAND grey and red fine loose damlp	
	!!]			8" SILTY CLAY, Lank, firm, damp, plastic	
1		}				
-	ii	i			SAND tan med line loose diamp med coarse	j
. .	!!					-
85	:					1 _
65 -	į	i				13
-	!!	100				-
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					SAND tun med fine foose dismp med coarse]
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	i i	95				
	!!	!				
	:			•	SAND tar/red fine mediterise damp some six	_
	ii	j				i
_	!!]			10" SILTY CLAY grey soft plastic	-
95	1					18
	i i	i				16
	!!	100				
1 ;	i :			•		
l i	į					
7	!!				SAND tanked med fine med decise damp wet]
	i	i				
100 _	!	!				Sample collected for VOCs
	:	85				·
-	•				SAND (an line saturated	Water Table
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	!			•		-
]	i:	i			SAND tan fine saturated	
	!	!]		<u> </u>
105	:					Sample collected for TOC
	i i	30		}		
]	!!			1		
-	•]
	ii	j			L] -
	[]	!			SAND tan fine saturated	_
	1 1			}		
110 _	į i	ا ہے ا		!	SAND tan medium sohiralled	-
		50				



PROJECT NUMBER	BORING NUMBER	
160492.SA.03	MW-97	
	SOIL BORING LOG	

PROJE				<u>ol Ar</u> eas Memphis		
ELEVA1	ION	297 44 8	eel MSL (TOO	 297 70 feet MSL 	(ground) DRILLING CONTRACTOR In State Testing Service	s, Inc
DRILLIN	IG METH	OO AND	EQUIPMENT	TUSED Hollow S	tem Auger 4 25 inch ID with CME Sampler	 -
WATER	LEVELS	101 25	feet BTOC (1	1/2001) START	10/01/2001 END 10/03/2001 LOGGER	Adam Kaiser (Jacobs)
DEPTHE			FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
1 1	INTERVA		****	PENETRATION		
1 1		RECOVE	MTYPE	TEST RESULTS	SOIL NAME USCS GROUP SYMBOL COLOR MOISTURE CONTENT RELATIVE DENSITY	DEPTH OF CASING DIRELING RATE DRILLING FLUID LOSS
1 1				6.4.4.4.	OR CONSISTENCY SOIL STRUCTURE	B
l l			ł	(N)	MINERALOGY	TESTS, AND INSTRUMENTATION Corrected FID (ppm)
			1			солисио газ (ррп)
-i	i i	i		Used hollow stem		_
! !	!	!		auger drilling method		1
1 7		 			SAND tan medium, saturated	·
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115		ļ				
	 	75		ì		j :
l i	i	i				
-!		ļ				_
1 :]]			CLAY brown very hard dry	
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PROJECT NUMBER 160492 SA.03	BORING NUMBER MW-98	
	SOIL BORING LOG	

 PROJECT
 Long Term Operational Areas - Memphis Depot
 LO

 ELEVATION
 294 43 (set MSL (TOC), 294 93 (set MSL (ground))
 DRILLING CONTR

 DRILLING METHOD AND FOLIPMENT USED WATER LEVELS
 102 00 (set BTOC (11/2001))
 Hollow Stem Auger 4.25 (such ID) with CME Sampler

 WATER LEVELS
 102 00 (set BTOC (11/2001))
 START
 10/01/2001
 END
 10/01/2001
 LOCATION Memphis Tennessee DRILLING CONTRACTOR In State Testing Services, Inc. LOGGER Jay Parker (Jacobs) 10/05/2001 COMMENTS SOIL DESCRIPTION DEPTH BELOW SURFACE (FT) STANDARD INTERVAL (FT) PENETRATION RECOVERY (%) DEPTH OF CASING DRILLING RATE SOIL NAME USCS GROUP SYMBOL COLOR TEST MOISTURE CONTENT RELATIVE DENSITY DRILLING FLUID LOSS RESULTS TESTS, AND INSTRUMENTATION OR CONSISTENCY SOIL STRUCTURE 6°-6'-6'-6' (Sail headspace) (N) MINERALOGY 5" concrete Clayey SILT dark reddish brown 5YR 4/2 med stiff damp Used hollow stem auger drilling method no penetration tes results 00 100 Same as above, brown, 7 SYR 4/4 5_ 05 100 e as above moist, slightly higher day content 10 00 100 Wet/saturaled soil may be due to open fire hydranis last week e as above most to well, soft, slightly plastic 15 0.0 100 ame as above, wet to saturated, becomes less wet by 20.5 20 00 100 Acre salty at 20 5 firm Clayey silt. strong brown 7 5YR 5/6 firm, damp. nonptastic Water appears to be running down hole outside is wet, but actual sample is not 25 00 100 Saty SAND strong brown 7 SYR 5/8 very fine to fine loose to firm damp 30 00 100 SAND yellowish red 5YR 5/8 fine to very line loose moist gray motiles Less motind w/kght gray @ 33 leef 35 00 100



PROJECT NUMBER BORING NUMBER MW-98 160492.SA.03

SOIL BORING LOG

PROJECT ELEVATION Long Term Operational Areas - Memphis Depot - 294 43 feet MSL (TOC) - 294 93 feet MSL (mound) LOCATION Memphis Tennessee

ELEVA				C), 294 93 feet MSL		s, fnc
					Stern Auger 4.25 inch ID with CME Sampler	·
				1/2001) START		Jay Parker (Jacobs)
DEPTH	BET OM 2		FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERVA			PENETRATION]
	1	RECOVE		TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
ł	ļ	1	#/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	ORILLING FLUID LOSS
Į.	1	1	ľ	62. 22.	OR CONSISTENCY, SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
<u> </u>		1		(N)	MINERALOGY	Corrected FID (ppm)
	i	!		Used hollow stem		
1	!	!		auger	Same as above more gray moties, grading coarser with depth	i
١.		:		drifting method		
1	ì	;		no penetration tes	1	! 1
40 _	-i	ì		results		l =
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	!	!	1		4.42.64004.2000.47.4	
	!	ł	1		At 43 SAND red 25YR 4/8 fine to mild loose to firm dump	1
	:	:	l		GraveRy SANO red 2 5YR 4/8 frm to loose med gravel up to 2" subrounded	t I
	ï	i			damp pebbles	[-
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	•	•	1		SAND with pebbles reddish yellow 7 SYR 6/6 med loose most	
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	i	i	Į		Pebbly SAND reddrsh yellow 7 5YR 6/8 loose med to fine most. Pebbles are	Sand is writ at top, but believe it?
	i	i			subangular	still running down hole from above
55	t .	1				
	! !	1				11 -
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	i					
ı	i	i l			Same as above, trace small gravel, damp, med, submunded	1
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1	i				SAND strong brown 7 SYR 5/6 course some pebbles loose moist]
1 -	ı i				subangular pebbles, trace rounded gravel	_i
l 1	ļ i					[
65 _						,
!	!!!	80				0 2
[!
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1						!
-i	j;				SAND strong brown 7 5YR 5/6 very coarse to fine gravel pebbles loose moist,	-1
l i) i				40% fine grave/pebbles	1
] [į					-1
70	!!	1				
1 !	!!					06
1 3		90			SAND goes to med to coarse, yellowish brown, with pebbles, loose, damp	- 1
						
1 3	1					l l
I -i	i]
J i	i	- 1			SAND strong brown 7 SYR 5/8 few to med few piritities loose damp to moist	1
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PROJECT NUMBER	BORING NUMBER	
160492.SA.03	MW-98	-
	SOIL BORING LOG	

PROJECT Long Term Operational Areas - Memphis Depot LOCATION Memphis Tennessee ELFVATION 294 43 feet MSL (TOC), 294 93 feet MSL (ground) DRILLING CONTRACTOR Tri-State Testing Services, Inc. DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4.25 inch ID with CME Sampler WATER LEVELS 102 00 feet BTOC (11/2001) START END 10/05/2001 LOGGER Jay Parker (Jacobs) 10/01/2001 SOIL DESCRIPTION COMMENTS DEPTH BELOW SURFACE (FT) STANDARD INTERVAL (FT) PENETRATION RECOVERY (%) SOIL NAME USCS GROUP SYMBOL COLOR, DEPTH OF CASING DRILLING RATE TEST MOISTURE CONTENT RELATIVE DENSITY DRILLING FLUID LOSS RESULTS OR CONSISTENCY SOIL STRUCTURE TESTS AND INSTRUMENTATION 6. 6. 6. 6. Corrected FID (ppm) MINERALOGY (N) 75 SAND strong brown 7 5YR 5/8 fine to med few peobles loose damp to moist auger dniling method no penetration test 90 results SAND pale yellow 2.5Y 8/2 very fine to fine very loose damp ame as above, but strong brown CLAY byw 6 Gravelly SAND light brown 7 SYR 6/4 sand is med gravel is fine to 80 rounded 00 90 Gravel zone is well at 80.5 to 81.5 ebbly SAND AND white SY 9/1 very fine to line very loose dry 85 05 100 Gravety SAND at 67 to 88 feet SAND Same as above at 83 and dark to gravelly SAND at 90.5 feet. 90 2" of clay at 90 feet Pebbry SAND as above down to 93 feet 08 100 Pebbly SAND as above med to coarse damp 95 03 100 As above with some gravel up to 1" becoming most to wet at 103 feet 100 90 Water Toble Secoming maist to well at 103 feet samples lost, probably saturated 105 0 Sample collected for VOCs Samples lost probably saturated SAND med to coarse saturated 110 Sample collected for TOC



PROJECT NUMBER	BORING NUMBER	
160492 SA.03	MW-98	
	SOIL BORING LOG	

PROJE				al Areas Memphis		
FLEVA	TION	294 431	eet MSL (TO	C) 294 93 feet MSL	(ground) ORILLING CONTRACTOR Tri State Testing Services	s Inc
WATER	NG METI	HOD AND	EQUIPMEN	T <u>USED</u> Hollow S 11/2001) START	Stern Auger 4 25 mch ID with CMF Sampler	
		URFACE (STANDARD	10/01/2001 END 10/05/2001 LOGGER	Jay Parker (Jacobs)
	INTERV		• • • • • • • • • • • • • • • • • • • •	PENETRATION	SOIL DESCRIPTION	COMMENTS
		RECOVE	HV (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	1
	i i	" ' ' ' ' ' '	s/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DEPTH OF CASING DRILLING RATE DRILLING FLUID LOSS
ł		ļ		6. 6. 6. 6.	OR CONSISTENCY SOIL STRUCTURE	TESTS AND INSTRUMENTATION
	<u>L</u>	<u> </u>		(N)	MINERALOGY	Corrected FID (ppm)
	į.	<u> </u>				
	!	!	1	osed notion stem	SAND med to coarse saturated	-
i	i	i		dn0irk) method		
ł	i	i		no penetration tes results	Pebbly SAND as above nive yellow 2.5Y 6/6 med to coarse with fine gravel/pebbles very loose saturated	i
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;		ŀ			Same as above broken ironstone and gravel at 132.5 to 133 feet	i
	i				SAND no gravel saturated line to coarse	-
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PROJECT NUMBER	BORING NUMBER	
160492 SA.03	MW-98	
	SOIL BORING LOG	

PROJE	CT	Long Te	m Operationa	al Areas - Memphis	Depot LOCATION Momphis Tennessee	
FLEVA	TION	294 43 f	DOLMSL (TOC), 294 93 teet MSt	(ground) DRILLING CONTRACTOR Tri State Testing Services	inc
DRILLI	VG METI	HOD AND	EQUIPMENT	1/2001) START	tem Auger 4 25 inch ID with CME Sampler 10/01/7001 END 10/05/2001 LOGGER	Jay Parker (Jacobs)
		JRFACE (STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERVA			PENETRATION		
!		RECOVE	RY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
!	ŀ	ļ	s/TYPE	RESULTS	MOISTURE CONTENT. RELATIVE DENSITY	DRILLING FLUID LOSS
1		1		666.	OR CONSISTENCY SOIL STRUCTURE	TESTS AND INSTRUMENTATION
├				(N)	MINERALOGY	Corrected FID (opm)
1	!	!		11 . 45 . 8		
] -	i .	i		Used hollow stem		_
i 1	i	Ì		auger drilling method		
					Same as above with gravel	
1		1		results		_
]		Ì		i		
145 _						_
_		50				
	!	!				<u>i</u> -
						j
	i	i		i	Gravetty SAND approximately 4 to 6* CLAY dense gray	_
					Prince Age 1	
-					BORING TERMINATED @ 148 FEET BK/S	
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PROJECT NUMBER	BORING NUMBER		
160492.SA.03	MW-99		
	SOIL BORING LOG		

PROJECT Long Term Operational Areas Memphis Depot LOCATION Memphs, Tennessee ELEVATION 285 33 feet MSL (TOC) 285 69 feet MSL (ground) DRILLING CONTI DRILLING MFTHOD AND EQUIPMENT USED Hollow Stem Auger 4 25 such ID with CME Sampler DRILLING CONTRACTOR Tri-State Testing Services, Inc. WATER LEVFLS 89 60 feet BTOC (11/2001) START 10/05/2001 END 10/08/2001 LOGGER Adam Kaiser (Jacobs) DEPTH BELOW SURFACE (FE) STANDARD SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) TEST SOIL NAME USCS GROUP SYMBOL COLOR DEPTH OF CASING DRILLING RATE RESULTS MOISTURE CONTENT. RELATIVE DENSITY DRILLING FLUID LOSS **2. 6. 6. 9.** OR CONSISTENCY SOIL STRUCTURE TESTS, AND INSTRUMENTATION MINERAL OGY (N) (Soil headspace) Used hollow ster auger drilling method no penetration les results 0 .. Zayey sift, brown firm dry 5 100 01 Clavery sell brown firm, dry 10 67 30 Clayey set brown firm, dry own gray (MI) 15 90 13 2 20 Sample collected for VOCs Soil sample (> 20 ppm) 312 90 withy ruley grey soft, moust Salty chay grey hard dry 25 100 10 7 Alayey salt, brown firm, damp 30 100 Sandy sitt gray/brown firm damp 35 65 10



PROJECT NUMBER	BORING NUMBER	
160492.SA 03	MW-99	
	SOIL BORING LOG	

Long Term Operational Areas Memphis Depot LOCATION Memphis Tennessee DRILLING CONTRACTOR Tri State Testing Services, Inc. ELEVATION 285 33 feet MSL (TOC), 285 69 feet MSL (ground) DRILL ING CONTR DRILLING METHOD AND EQUIPMENT USED Hotiow Stem Auger 4 25 inch ID with CME Sampler WATER LEVELS 89 60 feet BTOC (11/2001) START 10/05/2001 END 10/06 LOGGER Adam Kaiser (Jacobs) 10/08/2001 COMMENTS SOIL DESCRIPTION DEPTH BELOW SURFACE (FT) STANDARD INTERVAL (FT) PENETRATION TEST SOIL NAME USCS GROUP SYMBOL COLOR DEPTH OF CASING DRILLING RATE RECOVERY (%) MOISTURE CONTENT RELATIVE DENSITY DRILLING FLUID LOSS RESIDTS OR CONSISTENCY SOIL STRUCTURE TESTS AND INSTRUMENTATION 6.4.4.6. Corrected FID (ppm) (N) MINERALOGY Used hollow stem auger dinling method no penetration tes Sity sand red/grey dense fine damp 40 results Sand red med med dense most 70 Sand red med med dense most 45 0 1 65 Gravelly sand reddoch tan course med dense moist 50 0 9 90 Same as above: 10 to 15% gravel 1/4 to 3/4" Same as above with gravel up to 2" 55 11 dium to course gramed 85 Less to no gravel Sand medium to coarse med dense moist 60 5 5 100 65 land med Coarse gravelly medidense moist 19 95 Sand med med fine dense must no gravel 70 22 100 Same reddish (an line - (an some s#



PROJECT NUMBER	BORING NUMBER	
160492.SA 03	MW-99	
1	SOIL BORING LOG	

PROJECT Long Term Operational Areas Memphis Depot **LOCATION Memphis Tennessee** DRILLING CONTRACTOR Tri State Testing Services Inc. **FLEVATION** 285 33 feet MSL (TOC), 285 69 feet MSL (ground) DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4.25 inch ID with CME Sampler 10/08/2001 LOGGER Adam Karser (Jacobs) WATER LEVELS 89 60 feet BTOC (11/2001) START 10/05/2001 END DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) 11-51 SOIL NAME USGS GROUP SYMBOL COLOR DEPTH OF CASING DRILLING RATE MOISTURE CONTENT RELATIVE DENSITY RESULTS DRILLING FLUID LOSS OR CONSISTENCY SOIL STRUCTURE, 6-6-6-6 TESTS, AND INSTRUMENTATION (N) MINERAL OGY Corrected FID (ppm) Used hollow stem ame reddish tan fine tan some sill auger dolling method no penetration tes 18 65 results 80 2 2 65 Gravelly sand brown coarse most gravel 1/4 to 1/4" munded score sit 85 25 60 Less gravel no set wet 90 Water Table 40 Sample collected for VOCs velly sand brown coarse saturated Water 95 Sample collected for TOC 50 elly sand tan coarse saturated gravel: 40% 1/2 to 1 1/7 angular 100 65 elly sund tan barse saturated small gravet - 1/4 to 1/2" 105 100 and tan medicoarse saturated no gravel and (an medicolarse saturated no gravel 110 85

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PROJECT NUMBER 160492.SA.03	BORING NUMBER MW-99	
	SOIL BORING LOG	

PROJE	CT	Long To	em Operation	al Areas Memphis		
ELEVA		285 <u>33</u>	feet MSL (TO	C), 285 69 feet MSL	(ground) DRILLING CONTRACTOR—Tri State Testing Services	<u></u>
					tem Auger 4 25 inch ID with CMF Sampler	
WATER	RLEVEL	S 89 60	feet BTOC (1	1/2001) START	10/05/2001 END 10/08/2001 LOGGER	Adam Kaiser (Jacobs)
DEPTH		URFACE	(FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
	WIERV	L (FT)		PENETRATION		
Į .	ľ	RECOVE		TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
ŀ	1	1	#/TYPE	RESULTS	MOISTURE CONTENT: RELATIVE DENSITY	DRILLING FLUID LOSS
l	i		1	6. 6. 6. 6.	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
			<u> </u>	(N) .	MINERALOGY	Corrected FID (ppm)
	Ī	1		Used hollow stem		
	Į.	!		auger dniling method	111.5 Clay brown hard dry	<u>-</u>
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		I	1	results	BORING TERMINATED (§ 113 FEET BUS	
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PROJECT NUMBER
160492.SA.03
BORING NUMBER
MW-100

SOIL BORING LOG

PROJECT Long Term Operational Areas Memphis Depot LOCATION Memphis Tennessee ORILLING CONTRACTOR Tri-State Testing Services Inc. ELEVATION 291 16 feet MSL (TOC), 291 54 feet MSL (ground) DRILLING METHOD AND FOUIPMENT USED Hollow Stern Augor 4.25 inch ID with CME Sampler WATER LEVELS 92.95 feet BTOC (11/2001) START 10/05/2001 END 10/00 10/08/2001 LOGGER Jay Parker (Jacobs) DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) TFST SOIL NAME USCS GROUP SYMBOL COLOR DEPTH OF CASING DRILLING RATE MOISTURE CONTENT RELATIVE DENSITY RESULTS DRILLING FLUID LOSS 6.6.6.6 OR CONSISTENCY SOIL STRUCTURE TESTS, AND INSTRUMENTATION (N) MINERALOGY Corrected FID (ppm)
(Soil headspace) 6" asphalt and gravel Clayey silt dark reddish brown 5YR 3/4 med stiff nonplastic damp Used hollow steer auger drilling method no penetration les results 100 3 6 Clayey SILT dark reddrsh brown 5YR 3/4 med stiff damp nonplastic 100 24 Clayey SILT reddish brown med stiff dry nonplastic more sit interil than above 10 100 36 Clayey S1LT 7 5YR 4/3 brown with yellow 10YR 7/6 mostles, salty ned stiff dry 15 100 00 As above to 18.5 Sity SAND yellowsh brown 10YR Si6 fine moist soft, stightly plastic 20 100 00 Sifty SANO strong brown 7.5 YR 5/6 fair stiff pobbles 25 At 25 feet, sifty SAND, red 10R 4/8 stiff, fine, some gravel and peobles. 60 19 SAND red 10R 4/6 fine loose dry 30 60 24 Grawelly SAND 2 5YR 4/6 red same sand as above, becoming more ively with depth, gravel up to 2" sublingular approximately 20% gravel 35 50 00

CH2MHILL

PROJECT NUMBER 160492 SA 03	BORING NUMBER MW-100		
	SOIL BORING LOG		

LOCATION Memphis Tennessee PROJECT Long Term Operational Areas Memphis Depot DRILLING CONTRACTOR Tri State Testing Services Inc ELEVATION 291 16 feet MSL (TOC), 291 54 feet MSL (ground) DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4 25 inch ID with CME Sampler WATER LEVELS 92 95 feet BTOC (11/2001) START
DEPTH BELOW SURFACE (FT) STANDARD LOGGER Jay Perker (Jacobs) 10/05/2001 FND 10/08/2001 COMMENTS SOIL DESCRIPTION PENETRATION INTERVAL (FT) DEPTH OF CASING DRILLING RATE RECOVERY (%) TEST SOIL NAME LISCS GROUP SYMBOL FOLOR DRILLING FLUID LOSS RESULTS MOISTURE CONTENT. RELATIVE DENSITY. OR CONSISTENCY SOIL STRUCTURE TESTS AND INSTRUMENTATION 6" 6"-6"-6" Corrected FID (ppm): MINERALOGY (N) Used hollow sten SAND reddish yellow 7.5YR 6/6 fine loose some pebbles subrounded dry auger drilling method 40 results 00 50 SAND with gravel as above approx 5% gravel 45 00 75 Gravety SAND reddish yellow 7 SYR 6/6 fine to med loose dry approx 20% ubrounded and subangular glavel few peobles 50 0.5 75 Grades to trace pebbles at 53 feet Gravelly SAND as above, sand grades coarser at 55.5 feet 55 00 75 ack to fine by 58 feet SAND with peobles 7 5YR 5/6 strong brown medium loase dry few peobles or rie gravel 60 00 65 60 5 to 63 feet, getting coarsers, med to coarse, and moist SAND strong brown: 7 SYR 5/8 med well sorted toose damp grading coarser to med to coarse trace rounded peobles. 65 _ i 00 75 lost to well by 68 feet SAND with gravel light brown: 75 YR 6/4 coarse loose moult to well subangular ligavel - 15% fine gravel 70 0.0 50 ung more gravefly at 72 feet ~ 25% SAND with gravel light brown as above with gray motifies. fine to coerse in interbeds: 25% gravel loose, damp.



PROJECT NUMBER	BORING NUMBER	
160492 SA 03	MW-100	
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FROJE		Long 10	mm Operation	ar Areas Memphis	Depot LOCATION Memphis Tennes	.s ee
ELEVA	TION	291 16 1	eet MSL (TO	C), 291 54 feet MSI	(ground) DRILLING CONTRACTOR Yn Stale Testing Sitem Auger 4 25 inch ID with CME Sampler	Services, Inc
MATER	NO MET	OO ANI	1 DYOC 11	USED Hollow S		
WATER	BELOW S	9295	TOOL BLOCK	1/2001) START		GGER Jay Parker (Jacobs)
DEPTH			<u>- (T) </u>	STANDARD	SOIL DESCRIPTION	COMMENTS
1	INTERVA			PENETRATION		
1	}	RECOVE		IEST	SOR NAME USGS GROUP SYMBOL, COLOR	DEPTH OF CASING ORILLING RATE
		1	#/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS
		l		6.6.6.6	OR CONSISTENCY SOIL STRUCTURE	TESTS AND INSTRUMENTATION
	<u> </u>		<u> </u>	(N)	MINERAL OGY	Corrected FID (ppm)
75 _	!	!	i		Aa.	-
'' -	!	!		auger	SAND with gravel light brown us above with gray mottles, line to coarse in interbeds, 25% gravef loose, damp.	
l _	1	50		drilling method	and dealer some damp	• • •
	i	i		no penetration tes	4	-
-	İ	i		results		_
I .	l	ı	1			
1	[!	ŀ		ŀ	-
	!	!				<u> </u>
80						
∞		1				
l j	i	60	Į.		Same as above, gravel becomes larger and more at 80.5 feet, gravel up to 2 incl	No. 1
1 7	į	į	1			
1 ⊸		1		İ	[
!	!!	ļ		I		
		ļ .				
_		!	1			1
l		1			As above gravel grades out to few keice probbles at 84 feet	-
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	i i	75				0.0
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90 —i	i					1
!	l 1	90			CAND THE RESIDENCE OF THE CANDES OF THE CAND	00
!!	į	~			SANE) pale yellow 2.5Y 8/3 fere well sorted loose dry trace rounded pebbles grades back to Gravelly SAND at 90.5 feet.	-
!!	!				The same of the sa	
i :						
l ∹i	;				Wet at 93 feet Same as above, saturated	Sample collected for VOCs Water Table
į į	i				Committee as according to the committee of the committee	AA 9164 1 9 DHG
⁻	1					-
95 _ I	ļ				 .	_
!		20			20% recovery sample so wet most falls out	1
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l i	i			i		-
i	i				SAND uniform 10YO 745 fine have approved to the control of the	Complete and the state of the s
ļ	ı	1			SAND yellow 10YR 7/6 fine base saturated some gravel ~ 10%	Sample collected for TOC
. !	į					
100 _	!					, ,
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- <u> </u>	i			-		_1
!	!		ı		Same as above with more gravel and rounded pubbles, grading to SAMD	Į l
		- 1	i		light grey 10YR 7/2 very fine loose saturated at 104.5 feet	-
105 _	i	١ ,	ı		·	1
i	ì	50	, i			
-j	i		i	į		_!
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بد	!	i	1	ŀ		<u>. j</u>
!	!	- 1	1	ı	Same as above, with some gravel saturated]
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110 _	i	j	ı	l		
i	i	50	J	J		_
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PROJECT NUMBER 160492 SA.03	BORING NUMBER MW-100	
	SOIL BORING LOG	

PROJE	CT	Long Ter	rm Operationa	l Areas - Memphis	Deput t OCATION Memphis Tennessee	
FLEVA	TION	291 16 k	eet MSL (TOC), 291 54 feet MSL	(ground) DRILLING CONTRACTOR In State Testing Services	lnc
					Iom Auger 4.25 inch ID with CME Sampler	
				1/2001) START	10/05/2001 FND 10/08/2001 LOGGER	Jay Parker (Jacobs) COMMENTS
DEPTH	BELOW S		FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERVA			PENETRATION	CONTINUE LIBOR CHAND CAMBON COLOR	DEPTH OF CASING DRILLING RATE
[1	RECOVE	RY (%) B/TYPE	TEST RESULTS	SOIL NAME USCS GROUP SYMBOL COLOR, MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS
1	1			5° 6" 6"	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
1				(N)	MINERAL OGY	Corrected FID (ppm)
-	<u> </u>					-
_	i	i i	i	Used hollow stem auger		•
	!	!		drifting method		
_	!	}		no penetration les	Same as above	•
-	j	i		results		<u> </u>
115	i]	i I			_
	:	50				<u>_</u>
-	i	i				
-	!			,		-
	!	1				
	i	i .				
	!]		j	Same as above to 119 Inel	-
120 _	! .				SANDY CLAY grey	_
'20 _	i ,	100				_
	į į					_
_	!				Slowly grades to SILTY SAND with clay light grey	
_	;				10YR 7/1 with tan motiles dense damp fine	-
	į i					
	! ! — — — !					-
	i				CLAYEY SAND interbedded light grey as above, some bluck brinds	
	•				moist to will but doesn't appe it to be permeable, dense to very dense, non	-
	1				plastic, high fines conent	
125 _	•	50				-
	İ	. 30		•	CLAY layer 6' grey	_
-	1				CLAYEY SAND Right grey	
Ì	i					_
	!			ĺ	SANDY CLAY grey dense to very dense non plastic	
_	! !					-
	i	i	i		Same as above	
_	!					-
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PROJECT NUMBER	BORING NUMBER
160492.SA.03	MW-101B (Replaced SB-101)

								
PROJE				nal Areas Memphis		LOCATION Me	mphis Tennessee	
EL EVA	TION	291 70	feet MSL (TO	C). 291 99 feet MSL	L (around)	DRILLING CONTRACTOR To		s inc
DRILLIN	NG MET	HOD AND	D EQUIPMENT	T USED Hollow St	tem Auger 4 25 ind	h ID with CMF Sampler		
WATER	RLEVELS	S 93 32	Pleet BTOC (1	11/2001) START	10/19/2001	END: 10/19/2001	LOGGER	Jay Parker (Jacobs)
		URFACE ((FT)	STANDARD		SOIL DESCRIPTION		COMMENTS
	INTERVA			PENETRATION				1
		RECOVE		12.57	SOIL NAME USCS	GROUP SYMBOL, COLOR		DEPTH OF CASING DRILLING RATE
J		1	WIYPE	RESULTS		ENT RELATIVE DENSITY		DRILLING FLUID LOSS
, '	1	•	1	6. 6. 6.		Y SOIL STRUCTURE		TESTS, AND INSTRUMENTATION
Ц		<u> </u>	1	(N)	MINERALOGY			Corrected FID (ppm)
	ī	ī	T		6" asphall			(Soil headspace)
-7	į	İ	1	Used hollow stem auger	Clayey Sit 1 brown	soft, damp med plasts,		1
	!	į	ľ	drifting method				
, '	!	!		no penetration test	1			
,	:	100		results	İ			
	i	100		·				1
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5 _i	į į	į		!	j			0 0
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· -!	!	!	· [1 1	ĺ			
•		;	1	'				1
į	i	i	1	1 <i>i</i>	Same as above nedo	dish brown med stiff to stiff damp med pla	sbc	I -
-1	i i	i	1	1 1	į			l .
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l į	i i	. '	i j	i j	CLAYEY SILT			ſ
į	ı į	í I	(<u> </u>			AYEY SAND brownshired very fine med	বার্শ	- 1
20 _	i f	é '	i p		slightly plastic to med			02 _
	i F	i I	i j	1 ,			ĺ	_
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i ;	. ;	! !	í j	1 1	l			1
i j	į	i 1	i j	1 1				
Ī	į	i 1	1 1	1 1			I	Sample collected for VOCs (MW 101)
-	. 1	i l	1 1	i j	 Grading to a StLTY S	AMD with risy	I	1
25		1 1	i j	í j	3 H	rems was cary	I	00
!	. ,	1 1	i j	1 1			İ	-1
-:	. ;	! !	i j	<i>l</i> .				I
	. ;	: 1	i j	l t	SAND red very some a diamon traca designal at	to fine: stiff: some clay in matrix, grading co. 27 feet becoming more gravelly to 37 feet.	arser with depth	
-1	;	i j	i j			fine to medium, loose, dump	Ī	-
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35	- 1	. 1		i [1	00
	- 1			· •	6" of Citay at 35 feet			_
ï	i		. [ore yellow at 35 feet after the clay seam. Gr	rivel up to	



PROJECT NUMBER

160492.SA 03

BORING NUMBER

MW-101B (Replaced SB-101)

SOIL BORING LOG

Long Term Operational Areas Memphis Depot 291 70 feet MSL (TOC) 291 99 feet MSL (ground) PROJECT LOCATION Memphis Tennessee DRILLING CONTRACTOR In State Testing Services, Inc. ELL<u>VATION</u> DRILLING METHOD AND EQUIPMENT USED Hollow Stem Augor 4 25 inch ID with CME Sampler WATER LEVELS 93 32 feet BTOC (11/2001) START 10/19/2001 END 10/11 LOGGER Jay Parker (Jacobs) 10/19/2001 COMMENTS DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION INTERVAL (FT) PENETRATION DEPTH OF CASING DRILLING RATE RECOVERY (%) TEST SOIL NAME USCS GROUP SYMBOL COLOR DRILLING FLUID LOSS MOISTURE CONTENT. RELATIVE DENSITY RESULTS P. E. E. E. OR CONSISTENCY SOIL STRUCTURE TESTS, AND INSTRUMENTATION Corrected FID (ppm) MINERALOGY (N) Used hollow stem auger dniling method no penetration les 08 40 results Gravely SAND reddish yellow to pale yellow fine loose damp gravely in zones from fine pebbles to 1 inch subrounded to subangular. 100 00 45 0 5 100 00 55 ne as above, damp to most, gravel up to 2.5 inches 60 60 100 00 65 eme as above 09 70 100



PROJECT NUMBER	BORING NUMBER
160492.SA 03	MW-101B (Replaced SB-101)

Long Term Operational Areas Memphis Depoil PROJECT LOCATION Memphis, Tennessee
 ELEVATION
 291 70 leet MSL (TOC), 291 99 feet MSL (ground)
 DRILLING CONTR

 DRILLING METHOD AND EQUIPMENT USED
 Hollow Stern Auger 4 25 inch ID with CME Sampler

 WATER LEVELS
 93 32 feet 8TOC (11/2001)
 START
 10/19/2001
 END
 10/19/2001
 DRILLING CONTRACTOR Tri State Testing Services, Inc. 10/19/2001 LOGGER Jay Parker (Jacobs) DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) TEST SOIL NAME USCS GROUP SYMBOL, COLOR DEPTH OF CASING, DRILLING RATE #/TYPE KESULTS MOISTURE CONTENT. RELATIVE DENSITY DRILLING FLUID LOSS e. e. e. e. OR CONSISTENCY SOIL STRUCTURE TESTS, AND INSTRUMENTATION MINERALOGY (N) Corrected FID (ppm) 75 Used hollow ster auger drilling method no penetration les results Same as above. Gravel zone from 77 to 77 5. Recoming a sandy gravel with depth then back to gravely SAMD by 86 set. 80 00 100 85 00 Sample collected for VOCs Gravelly SAND pale yellow to light grey fine loosi Gravelly zone at 68 feet 90 12 100 Water Table Sample collected for VOCs (MW 101) Wet @ 96 to 100 feet Hard to identify water tuble as most water runs out of sample before reaching the surface 100 100 105 Gravelly zone at 105 feet Sample collected for TOC SAND and gravelly SAND pale yellow line to med loose saturated Gravel zones at 107 to 108 feet. 110 __



PROJECT NUMBER	BORING NUMBER
160492 SA 03	MW-101B (Replaced SB-101)

PROJE	_			Areas Memphis		
PLEVA	TION NG METH	291 /0 (OD AND	FOUIPMENT	C) 2 <u>91 99 feet MSL</u> USED Hollow S	tom Auger 4.25 inch ID with CME Sampler	
WATER	LEVELS	93 32	feet BTOC (1	1/2001) START	10/19/2001 END 10/19/2001 LOGGER	Jay Parker (Jacobs)
DEPTH	BELOW S	JRFACE (FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
i	INTERVA			PENETRATION		
	ļ	RECOVE	RY (%) In/TYPE	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE DRILLING PLUID LOSS
1		1	D/TYPE	RESIMETS 6" 6"-6" 6"	MOISTURE CONTENT RFLATIVE DENSITY OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
	1	l	}	(N)	MINERALOGY	Corrected FID (ppm)
	i			Used hollow stem	C CA16	
		100		auger	Canvery Scort)	-
_	i	i		dnling method no penetration test		-
!!		!		results		_
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li	i i	i			Above the gravel zone: SAND yellowish red: coarse: louse: submated: trace gravel	
	. !				Gravel zone at 123 to 124 feet	_
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125						_
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!	!				Gravelly SAND	
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PROJECT NUMBER
160492.SA.03
BORING NUMBER
MW-101B (Replaced SB-101)

PROJE		Long To	em Operation	ial Areas - Memphs		
ELEVA	TION	_291 70	fred MSL (TO	C) <u>291 99 feet MS</u>	(pround) [WILLING CONTRACTOR To State Testing Secretar	s, Inc
DRILLIN	IG MET	HOD AN	D EQUIPMEN	TUSE <u>D Ho</u> llow S	Stem Auger 4.25 inch ID with CME Sampler	
WATER	LEVELS	93 32	feet BTOC (11/2001) START	10/19/2001 END 10/19/2001 LOGGER	Jay Parker (Jacobs)
DEPTHE	ELOW S	URFACE	(FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
ł	INTERV	(FT)		PENETRATION		
1]		RECOV	ERY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR,	DEPTH OF CASING DRILLING RATE
	1	l	BULLABLE	RESULTS	MOISTURE CONTENT, RELATIVE DENSITY	DRILLING FLUID LOSS
		1	1	6, 6, 6, 6,	OR CONSISTENCY SOIL STRUCTURE	TESTS AND INSTRUMENTATION
	Щ.	<u> </u>	↓	(N)	MINERALOGY	Corrected F1D (ppm)
1 !	!	!			CLAY	
1 4	! 	!		Used hollow stem		ł
1]		auger	BORING TERMINATED @ 142 FEET BG\$	1
I -ì		1	ļ	dratting method		1
		ŀ	ľ	no penetration tes		1
1 1				results	j	ļ
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PROJECT NUMBER 160492 SA 03	BORING NUMBER MW-102	
	SOIL BORING LOG	

PROJE	CT	Long Te	rm Operationa	al Are <u>as Memph</u> us		
ELEVA), 311 70 feet MSL		Inc
					tem Auger 4 25 inch ID with CME Sampler	
	BELOW ST			1/2001) START	10/09/2001 FND 10/10/2001 LOGGER SOIL DESCRIPTION	COMMENTS
DEFINI	INTERVA		<u></u>	PENETRATION	304 0434411 11644	
1	***	RECOVE	BY (NL)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
			#/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS
	i .		_	6. 6. 6. 6.	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
	i !			(N)	MINERALOGY	Corrected HD (ppm)
					6 inch grass and organics	(Soll headspace)
t '	!!!			Used hollow stem auger	Clayey SILT brown 7 SYR 5/3 slightly plastic med stiff damp	
	:	100	:	drilling method		00
	i			no penetration test results		
_	ii				Clayey SILT same as above	
1	!!					-
5	i					_
]	į	445				
[-	!!	100				1
	1					i -
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1 1	!!				Clayery SILT reddish brown 5YR 5/4 soft to med stiff damp slightly to non	
-				1	plastic	-
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-		ı			Clayery SILT yellowish brown 10YR 5/4 soft to med stiff dry nonplastic	<u> </u>
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1					Clayey SILT same as above med stiff to stiff	i -
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	i i					
i					SAND yellowish red. SYR 5/6 very fine to fine loose moist.	i
_	•					
25	i					
· · · - i	i					0.9
_!	!	60				-
1 1	1	1				
i	i		1		At 27 feet, grades to reddish yellow 7 5YR 6/6, fine to med	
ı !	!				Same as at 27 feet, very fine to fine stiff	_
1	: :		1			-
30	i					_
_ <u></u>	į			•		16
-		75				j '"
_ <u>.</u> i	i				At 31.5 feet clayery SAND yellowish red. 5YR 5/8 nonplastic dense/very stiff.	
į	. !	ļ			dry line Nearly 50% day	
	:				SAND durk red 2 5YR 3/6 with reddish yellow 7 5YR 6/6 mottles almost 50/50]
i	i				mix very line to line clease damp to dry	-
35_	. !		l			_
	ł	75				12
i	i	ł				
					At 37 feet fine well sorted med dense strong brown 7.5 5/8 day to damp	



PROJECT NUMBER	BORING NUMBER	
160492.SA.03	MW-102	
		-

PROJECT LOCATION Memphis, Tennessee Long Term Operational Areas - Memphis Depot ELEVATION 311 34 feet MSI (TOC), 311 70 feet MSI (ground) DRILLING CONTE DRILLING METHOD AND FOUIPMENT USED Hollow Stem Auger 4 25 mich ID with CME Sampler DRILLING CONTRACTOR Tri State Testing Services Inc. WATER LEVELS 110 66 feet BTOC (11/2001) START 10/09/2001 END 10/10/2001 LOGGER Jay Parker (Jacobs) DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) II ST SOIL NAME USCS GROUP SYMBOL COLOR DEPTH OF CASING DRILLING RATE RESULTS MOISTURE CONTENT RELATIVE DENSITY DRILLING FLUID LOSS 6.-6.-6. 6. OR CONSISTENCY SOIL STRUCTURE, TESTS, AND INSTRUMENTATION (N) MINERAL OGY Corrected FID (ppm) Used hollow ster auger drilling method no penetration tes SAND yellowish red 5YR 5/6 fine med dense dry 40 results 56 **6**0 Grades to med: to coarse at 42 feet with trace rounded pebbles 2.5 intervals 04 SAND brownish yellow 10YR 6/8 med to coarse loose dry trace rounded pebbles grades to yellow sand 10YR 7/6 at 46 feet fine to med trace gravel 60 SAND same as above more gravel - 10% 50 09 65 55 11 55 SAND same as above, only trace gravel of 57.5 feet, then gravel as above SAND yellowsh red SYR 5/8 line to med loose dry grades to reddish yellow 7.5 YR fine toose damp trace pubbles. 60 18 75 SANO same as above reddish yellow no gravel 65 00 15 SAND same as above 70 15 75 Cravely SAND yellow 10YR 7/6 line to coarse loose damp gravel up to 2 subves



PROJECT NUMBER 160492.SA.03	BORING NUMBER MW-102	
	SOIL BORING LOG	-

LOCATION Memphis, Tennessee Long Term Operational Areas Memphis Depot DRILLING CONTRACTOR Tri State Testing Services, Inc. LOGGER Jay Parker (Jacobs) 10/10/2001 SOIL DESCRIPTION COMMENTS DEPTH BELOW SURFACE (FT) STANDARD INTERVAL (FT) PENETRATION RECOVERY (%) SOIL NAME, USCS GROUP SYMBOL, COLOR DEPTH OF CASING DRILLING RATE TEST MOISTURE CONTENT RELATIVE DENSITY DRILLING FLUID LOSS 9/1 Y5% RESULTS TESTS, AND INSTRUMENTATION OR CONSISTENCY SOIL STRUCTURE 6.4.6.4. Corrected FID (ppm) (N) MINERAL OGY 75 Used hollow stem 00 auger drilling method no penetration tes 75 rosults Grading down to piribbles at 78 feet. SAND yellow 10YR 7/6 med to coarse loose dry. 75% but sample fell out on ground 80 00 75 SAND same as above trace large gravels up to 1 inch 85 00 60 At 88 feet, sand appears most Curvety SAND pale yellow 2.5Y 7/4 fere to coarse, very dense, dry, gravet up to 1 inch, 45% gravet. 90 18 50 Gravelly SAND same as above 95 06 Only 1 liner was placed in the 5 span Gravelly SAND sume as above 100 11 75 Gravelly SAND same as above 26 105 60 Sample collected for VOCs Gravelly SAND same as above strong brown 7 SYR 5/8 00 50 Vet at 110 feet Water Table

PROJECT NUMBER	BORING NUMBER	
160492 SA.03	MW-102	
	SOIL BORING LOG	

PROJECT			<u>al Areas Memphis</u>		_
FLEVATION_	311 <u>34 k</u>	em MSL (TO	C) 311 70 feet MSL	(ground)DRILLING CONTRACTOR Tri State Tirsling Service	s, Inc
DRILLING ME	HOD AND	EQUIPMEN	TUSED_ Hollow S	tem Auger 4.25 inch ID with CME Sampler	
			11/2001) START	10/09/2001 END 10/10/2001 LOGGER	Jay Parker (Jacobs)
DEPTH BELOW	AL (FT)	1)	STANDARD	SOIL DESCRIPTION	COMMENTS
INTER			PENETRATION		i
1 !	RECOVE	B/TYPE	TEST	SOIL NAME USCS GROUP SYMBOL COLOR,	DEPTH OF CASING DRILLING RATE
1 1		211172	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS
1 1	1 i	1	(N) 6-6-6-6-	OR CONSISTENCY SOIL STRUCTURE, MINERALOGY	TESTS, AND INSTRUMENTATION
	+		1 177	THE CTOLOGY!	Corrected FID (ppm)
-i	i		Used hollow stem		
1	į.	ŀ	auger drifting method		1
-!	-!		no penetration tes	Gravely SAND same as above zones of rounded publies saturated	Sample collected for TOC
l -i	i		results		_
115 İ	i 50		ľ		
I ⁻ !	!		1		-
-	;				<u>-</u>
l i	i				i
!	!				
-!	·!			Con-B. (Abit)	_
l i	i		<u> </u>	Gravely SAND same as above saturated	
-i	1				-
120	!				_
l :	60		i		
-i	i [1		-
!!	!				i
1 -	!!!				-
l i	i				4
71	·i [ľ	Frank (B. C. C. C.	-
!	!			Sample fell out, probably more of the same	
1 -	;				
125 i	i				
!					_
1 .	!				
1 7	i				-
_i	i j				<u> </u>
l !	!				-
I -i	.				
j i	i			SAND very pale brown 10YR 7/3 fine to coarse loose saturated few pebbles	_
<u>-!</u>	!				
l ;	: 1				
130 —	i				
į	50			i	
-!	!				
;	: !				
Ιi	i l		i		
!	!			+	
	{		 	Chy CAID Boby man 2 CV 7/1 unit hammalish and a state of	-
i	i l	į		Srilly SAND flight grey 2.5Y 7/1 with brownish yellow 10YR 6/8 mutitors very fine sitty morst med stiff nonplastic	
. <u>.</u> i	!			notions say in a say more, made sair nonpression	-1
135	!	ľ			
l i	50				
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	!	ł	· · · · · · · · · · · · · · · · · · ·	Sity SAND: same as above, grading to clay SAND at 139 feet	-
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140 _		J	·	i	
	100	İ	ļ.		l
_i	: I		K	rading to Sandy Ct.AY at 140.5 feet	



PROJECT NUMBER	BORING NUMBER MW-102
160492 SA.03	M144-102
	SOIL BORING LOG

PROJE	CT TION	Lang Te	m Operations	ol Areas <u>Memphis</u> C) 311 70 feet MSL	Depoi LOCATION Memphis Tennessee (ground) DRILLING CONTRACTOR To State Testing Services	
DRILLI	NG MET	HOD AND	EQUIPMENT	USED Hollow S	tem Auger 4.25 inch fD with CME Sampler	<u> </u>
WATER	RLEVELS	110 66	feet BTOC (1	1/2001) START	10/09/2001 END 10/10/2001 LOGGER	Jay Parker (Jacobs)
		URFACE (STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERVA	u (FT)		PENETRATION		
		RECOVE	RY (%)	TEST	SOR NAME USGS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
		!	#/TYPE	RESULTS	MOISTURE CONTENT. RELATIVE DENSITY	DRILLING FLUID LOSS
	ľ	i		6.4.4.4	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
	<u> </u>			(N)	MINERALOGY	Corrected FID (ppm)
	t	ļ		Used hollow stem		1
-	!			auger		
	i	:	i I	drilling method		
1	i	i	f I		Clay is bluish grey CEAY 51 hard damp	-
	i			results	BORING TERMINATED (§ 143 FFFT BGS	
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PROJECT NUMBER	BORING NUMBER		
160492.SA 03	MW-103		
	SOIL BORING LOG		

PROJ	PROJECT Long Term Operational Areas Memphis Depot LOCATION Memphis, Tennessee					
ELEV/	ATION	301 35 1	eel MSL (TO	C), 301 90 feet MSL	(ground) DRILLING CONTRACTOR To-State Texture Services to	kc
DRILL	ING METI	HOD AND	FOUIPMENT	TUSED Hollow S	Rem Auger 4 25 inch ID with CME Sampler	
				1/2001) START	10/15/2001 FND 10/16/2001 LOGGER	Adam Kaiser (Jacobs)
ULPIN	RHI OW S		<u>/ 1)</u>	STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERV		****	PENETRATION		ļ
	ŀ	RECOVE	MTYPE	TEST RESULTS	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
	ľ	ľ		6.6.6.6.	MOISTURE CONTENT RELATIVE DENSITY OR CONSISTENCY SOIL STRUCTURE.	DRILLING FLUID LOSS
ľ	Ì			(N)	MINERALOGY	TESTS, AND INSTRUMENTATION Corrected FID (ppm)
				1	Asohati	(Soll headspace)
1 .	-i	i		Used hollow stem	Clayey silt Brown hard-dry	1
	.!	100		auger dnilling method		13
	1	:	1	no penetration tes	1	1
	-i -	i		results		-
	!	!	ŀ			_
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-	-i	i				_
	1	100				113 _
	!	!	1			į.
	i	i	f	ŀ] -
1 -	-j	į	ľ	ľ	Clayey sit, grey hard dry	
1 .	.!	ļ]	Solvey Sac grey Table buy	
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ł	!	!			Claus	_
	<u> </u>	!			Clayery set, Grey soft	
٠.,	i	i				
15 _	į į	ļ .		ŀ		Sample collected for <u>VOCs</u>
_		85		[:		314
i	i	i		1		
-	į į	,				
	!				a	_
	i	1			Chyey silt brown hard dry	
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	i i			i	Clayey Sit Brown stiff moist	
l	!!!					1
²⁵ —	:					
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	ii					_
	į į	Ī			Sandy sill-brown stiff most	
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	!		į	i	Sand reddish tan lime medium dense moist	'1
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PROJECT NUMBER 160492 SA.03	BORING NUMBER MW-103		
	SOIL BORING LOG		

Long Term Operational Areas Memphis Depot **LOCATION Memphis Tennessee** DRILLING CONTRACTOR Tri-State Testing Services Inc ELEVATION 301 35 feet MSL (TOC), 301 90 fret MSL (ground) DRILLING CONTI DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4 25 inch ID with CME Sampler 10/16/2001 WATER LEVELS 69 43 feet BTOC (11/2001) START 10/15/2001 END LOGGER Adam Karser (Jacobs) DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) SOIL NAME USCS GROUP SYMBOL COLOR DEPTH OF CASING DRILLING RATE TEST #/TYPE MOISTURE CONTENT. RELATIVE DENSITY DRILLING FLUID LOSS RESULTS TESTS, AND INSTRUMENTATION OR CONSISTENCY SOIL STRUCTURE 6. 6. 2. 2. Corrected FID (ppm) MINERALOGY (N) Used hollow stem and reddichitan medium mediumidense moist Gravel 1/2: 3/4" (10% - 15%) auger drilling method no penetration tes 40 results 22 60 Selly Sand red dense most 2.5 intervals 45 85 Sand Ian medium, medium dense moist 50 0 0 60 2.5 intervals Sand red medium fine dense moist Acre coarse pravate 15 100 60 Sand and small gravel (1/4 - 1/2*). Sand red. medium fine: dense moist 100 Sample collected for VOCs Sand tan fine dense moist, subwated and Red-medium, medium-drinse: sulurated At 64 feet Dup Water at 64 feet 65 08 75 Sifty olay-gray stiff wet Water Table 70 Clary brown stdf Sand red medium coarse medium dense granually 20% (1/2" 3/4") wet, satural Sample co8octed for VOCs at 72 feet 2.5 intervals.



PROJECT NUMBER	BORING NUMBER	
160492.SA.03	MW-103	

PROJECT			al Areas Memphis	Depot LOCATION Memphis Tennessee	
ELEVATION DRILLING	N _ <u>301.35</u>	feet MSL (TO	C), 301 90 leet MSL	LOCATION Memphis Tennessee	<u>c</u>
WATER LF	VFIS 6943	feet BTOC (1	1/2001) START		Adam Karser (Jacobs)
	OW SURFACE	(FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
IN IN	TERVAL (FT)		PENETRATION		-
1 1	I RECOVI	F/TYPE	TEST RESULTS	SOIL NAME USCS GROUP SYMBOL COLOR MOISTURE CONTENT RELATIVE DENSITY	DEPTH OF CASING DRILLING RATE DRILLING FLUID LOSS
]	İ		6-6-6-6	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
-	!	}	(N)	MINERALOGY	Corrected FID (ppm)
75	25		Used hollow stem auger dnilling method no penetration tes results	Sand red, mindium coarse medium dense, granually 20% (1/2" 3/4") wet, satura	Sample collected for VOCs
80 _1	60		:	Sand red medium coarse medium dense - granually 20% (1/2° 3/4°) wet satura	- - - -
-1 -1 85				Sand very coarse modium dense saturated small grave	
	75			Sandy sit: fine very dense Subtrated wet	-
90 _			:	Clay brown to grey staff to hard dry	- - -
-	100				-
95				Clay brown grey stiff hard day BORING YERMINAYEI)	- -
100 _					- - -
-					-
105 _					- - -
-					-
110_			l.		



PROJECT NUMBER 160492 SA.03	BORING NUMBER MW-104	
	SOIL BORING LOG	

Long Term Operational Areas Memphis Depot LOCATION Memphis Tennesser 295 76 feet MSL (TOC) 296 13 feet MSL (ground) DRILLING CONTRACTOR Tri State Testing Services Inc. ELEVATION DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4.25 such ID with CME Sampler WATER LEVELS 63.01 feet BTOC (11/2001) START 10/15/2001 END 10/1 END 10/16/2001 LOGGER Jay Parker (Jacobs) DEPTH BELOW SURFACE (FT) SOIL DESCRIPTION COMMENTS STANDARD INTERVAL (FT) PENETRATION RECOVERY (%) DEPTH OF CASING DRILLING RATE TEST SOIL NAME USUS GROUP SYMBOL COLOR MOISTURE CONTENT RELATIVE DENSITY DRILLING FLUID LOSS #/TYPE RESULTS TESTS, AND INSTRUMENTATION 6*-6*-6* 6* OR CONSISTENCY SOIL STRUCTURE Corrected FID (ppm) (Soil headspace) (N) MINERALOGY 6* Asphalt and gravel CLAYEY S4L drown 7.5 YR 4/3 medium stiff non-plastic damp Used hollow stem auger draling method no penetration tes results 05 100 Clayey SILT brown 7 5 YR 4/5 with pinkish grey 7 SYR 6/2 mottles medium stiff non-plustic, dry 100 0.0 Clayey SILT brown 7.5YR 4/F medium stiff non-plastic dry 10 00 100 Clayey SILT same as above damp 15 0 0 100 Clayey SRL1 invitted again as the 3-8" zone with reddish black slumps of FeOi medium stiff damp more day content than above outside of sample wet. 20 0 0 100 JEG (1) 23 feet Clayey SILT same as above grading to silty same Perched water 25 Sity SAND reddish brown 2 5YR, 44 moist. 100 soft/medium dense, grading sandwr with depth 00 SAND very pale brown 10YR 7/4 loose, dry fine well sorted 30 0 0 50 SAND same as above 35 _i 00 50 SAND 5 YR 5/8 yellowish red. line to medium, loose, damp, three gravel



PROJECT NUMBER	BORING NUMBER	
160492.SA.03	MW-104	
		

- KUJE				as Areas Memphis		emphis Tenniessee	
ELEVA	TION	295 /6 I	eel MSL (TO	C), 296 13 leat MSL	ground) DRILLING CONTRACTOR In	State Testing Service	s, Inc
DRILLI	NG ME <u>T</u> E	100 AND	FQUIPMENT	LUSED Hollow S	em Auger 4 25 inch ID with CME Sampler		
WATER	RIEVELS	63 01	feet BTOC (1	1/2001) START	10/15/2001 END 10/16/2001	LOGGER	Jay Parker (Jacobs)
DEPTH	BELOW S	URFACE ((T)	STANDARD	SOIL DESCRIPTION		COMMENTS
	INTERVA	L (FT)	-	PENETRATION			
į.		RECOVE		1			
ł	1	MECOVE	B/TYPE	TEST	SOIL NAME USGS GROUP SYMBOL COLOR		DEPTH OF CASING DRILLING RATE
1	1	ŀ	MIANE	RESULTS	MOISTURE CONTENT. RELATIVE DENSITY		DRILLING FLUID LOSS
	ļ	l .	1	e. e. e. e.	OR CONSISTENCY SOIL STRUCTURE		TESTS, AND INSTRUMENTATION
	<u> </u>		<u>i</u>	(N)	MINERALOGY		Corrected FiD (ppm)
	i	i —					
	1	ĺ		Used hollow stem			_
	ı	ı		auger	SAMD same as above grading to SAND 5YR 5/8 yellowish red	i medium kose	1
	ı	ı		dolling method no penetration les	damp no gravel		· i
40	ļ	ţ		results			
	į	!		1030.13			00 -
I _		50					1 **
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l -		:					ľ
	:				SAND as above trace gravel		
l -	:	1	[Select as above mada graves		
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	!	}	l .	:	SAND, as above, trace gravel grades away by 48		-
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J -							1
1		i			AND 5YR 5/6 yellowish red medium to coarse, well sorted too	ози фитр	1
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55	i		ł l				
l ~ −i							1
l i	i	100					00
ŀi	į į						-
	1 (l .					
1 1					At 57' CLAY yellowish red. with yellow mottles, very plastic, sol	it damp	1
		l l					
!	!!!			i	Jav continues to 50°		
-!					Jay continues to 59" AND same as above		
60					SAND turns to yellow fine wer		1
-!					transport of the control of the cont		00 -
	!	70					
! !			1				
-	:				14815 4		
;					AND fine wet seam -1"		Sample collected for VOCs
i					AND 5YR 5/6 yellowish red medium to coarse saturated med	dum dense	Water Table
i	i						Sample collected for TOC
i	i	ŀ					· · · · · · · · · · · · · · · · · · ·
65_j	į		j		·]
l t	ĺ	I	· ·		andy Set very fine dense join clay slightly plastic		i –i
-1		75					_
ı	j	- 1	Į	ľ			
-i	- 1	1	ľ	ŀ	AND same color fine toose substated	····-	l
<u> </u>	!	l	- 1	J	The same was a second with the same of the		r i
į		l	i		AND as above grading to Pebbly SAND		-[
_!	ļ	ł			• •	;	
! پر	!	1	J	ŀ			-
⁷⁰ —	?	Į.	ľ	ļ			_
. !		50	- 1	į.	ANNA CANDBandah and annu to the		_
-1	!	~	- 1		abbly SAND yellowish-red coarse loose rounded to subround sturnled	and line gravel	Subjected sometal loci
		- 1			THE STEW	,	Saturated sample lost out bottom
-:	- ;	1		I			-1
_i.	;	[ŀ			
i	_;	I	ŀ	j _'	o sample recovered probably same loose, subtrated, pebbly S/	AND as above	-

CH2MHILL

PROJECT NUMBER 160492.SA.03	BORING NUMBER MW-104	
	SOIL BORING LOG	

PROJE	CT	Lana Te	m Operation	al Areas Memphis	Depot LOCATION Memphis Tennessee	
ELEVA"	TION	295 76 f	oel MSL (TO)	C), 296-13 feet MSL	(ground) DRILLING CONTRACTOR Tri State Testing Services	Inc
DRILLIN	NG METH	HOD AND	EQUIPMENT	T <u>USED</u> Hollow S	tem Auger 4.25 inch ID with CME Sampler	
				1/2001) START	10/15/2001 END 10/16/2001 LOGGER SOIL DESCRIPTION	Jay Parker (Jacobs) COMMENTS
REPIH	INTERVA	URFACE (STANDARD PENETRATION	TANK DESCRIPTION	Constitution
		RECOVE	RY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
			D/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY,	DRULLING FLUID LOSS
		İ	ŀ	6.4.4. 6.	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
	L	<u> </u>		(N)	MINERALOGY	Corrected FfD (ppm)
75	!	!		Used hollow stem		_
'' -	i	ľ		auger		
j -i	i i	i °		dolling method no penetration test		
l _	! ·	!		results		
	i	i				
	!!	!			No sample may 5% fines land in sampler saturated	
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60 <u> </u>	i i	į		į		-
	:	5		ł		
-	i					
-!	!!!	!				-
-		i			No sample again race clay at end at 88	•
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85 —	i į	j				_
-		5				-
l i	i i	i				
!	!!!	!				_
-:		}		:	Sand and gravel as above at 90.5	·
		!				
90		}				_
	į	100			CLAY dark greenish gray CLAY 4.1 very dense/stift damp	
_					,	
-i	į					-
-					BORING TERMINATED (4 93 FEFT BGS	
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PROJECT NUMBER	BORING NUMBER	· · · · · · · · · · · · · · · · · · ·
160492.SA.03	SB-105	
	SOU DODING LOG	

ELEVA		204.20	fnet MSL (gro	nus Areas Memphis	Depot	LOCATION Mem			
DBILLI	INC MET	100 VNI	DECHUDASE	JT IISED Hollows	10m A 4 35	DRILLING CONTRACTOR Tri S ID with CME Sampler	tate T <u>esting Service</u>	s inc	
WATE	RLEVEL	NOO AIR	DRY	START	AUGER 4 25 Incr			 	
DEOTH	BFLOWS	S ACE	(FX)		10/15/2001	END 10/15/2001	LOGGER	Jay Parker (Jacobs)	
100,17	MIERV		(+1)	STANDARD		SOIL DESCRIPTION		COMMENTS	
ł	THIERV.			PENETRATION					
i		RECOVE	E/TYPE	1551		GROUP SYMBOL COLOR		DEPTH OF CASING DRILLING R	AIE
	1		B/TYPE	RESULTS		INT RELATIVE DENSITY		DRILLING FLUID LOSS	
			1	666.		SOIL STRUCTURE		TESTS AND INSTRUMENTATION	4
<u> </u>	↓	 		(N)	MINERALOGY			Corrected FI	D (ppm)
1	!	!		Lhert hollow storn	Concrete Clay Sity most, me	dua dulia.		(Soll head	space)
1 -	-1	!	1	auger	Coay say Irange Ira	roum pusocaty			-
-	i	i	1	drilling method	J			1	
	i	i	1	no penetration tes results	1			ľ	-
1	F	100	1	Tersons	1			1	
	.!	!						1	
1 .	!	!	Ì					!	-
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	.i	i						<u> </u>	
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ĺ	1	i			L				_
	!	!			Cluy Sitty same as at	DOVE		There was apparently	
_	!	!	j					3' of slough in sampler barrel	-
-	i	į	ł	ſ	ł			i sompre operar	
10	i	i	ľ	1				l	
l " –	ì	i		1				19	
	1	İ							
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i	!	100	1	4	1				
	:	:							_
_	i	i			f				
	i	i]						
15	ĺ	j	1						-
13 -	ı	ı	ľ	1				00	
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	!	ł							-
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	i i	i			Sell with clay brown i	most medium plasticity			- 1
_	j i	j					;		-I
	<u>.</u> 1	١ .]	1					- 1
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!	¦ !				on very saintly with d	ay reddish brown moist medium plastic			ł
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PROJECT NUMBER 160492.SA.03	BORING NUMBER SB-105	
	SOIL BORING LOG	

PROJE	ct	Long Te	m Operation	al Areas Memphis I	Depo <u>t</u>		Memphis Tennessee	
FLEVA	TION	304 29 6	eet MSL (grou	und)		DRILLING CONTRACTOR	Tn State Testing Services	tnc
DRILLI	NG METH	OD AND	FOUIPMENT	TUSED Hollow St	tem Auger 4 25 inch ID			
	RLEVELS		DRY	START	10/15/2001	END 10/15/2001	LOGGER	Jay Parker (Jacobs)
DEPTH	BELOW S		п,	STANDARD	<u> </u>	SOIL DESCRIPTION		COMMENTS
1	INTERVA			PENETRATION	1			
	1	RECOVE		πετ		ROUP SYMBOL COLOR		DEPTH OF CASING DRILLING RATE DRILLING PLUID LOSS
	1	ı	SATYPE	RESULTS	MOISTURE CONTENT			TESTS, AND INSTRUMENTATION
	1	ı		6-6-6-6-	OR CONSISTENCY SE	OIL STRUCTURE		Corrected FID (ppm)
┝		<u> </u>	 	(N)	Same as above			
_	1	i	1	Used hollow stem				-
ļ	i	í		auger drilling method	l			
} -	į.	į	1	no penetration test	l			-
40		į		results	l			go _
	} `	•		į į	CANAL INC. Son with son	me soft, reddish brown with dark m		
i	i	i		ł ,	SAMU WHY site William	MB SOR, (EGOS) Drown was was seen	orang	
l _	į .	100		j	l			i
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-	:	<u> </u>	İ	l				-
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45	!	<i>!</i>						
	:	i		Į į				
	i i	j l					ı	
-	i	Į į		Į į	SAND as above becom	ing yellowish brown		
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!	į			j j	I			wet at app 60"
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	í		1	1 1	I			Spilled 1st 6 of 57 67 0 0
60 _	i i	. !	ĺ	i 1	I		i	5/8/
	!!			i I	I		i	
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-!	!	1	i	i				-
		J		i				<u> </u>
1		J	1	i j	SAND as above varying	yellowish to reddish brown moist	some gravel	
-i	į	J		i I				-
_!	1	J		i j			į	
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PROJECT NUMBER	BORING NUMBER	
160492.SA.03	SB-105	
	SOIL ROPING LOG	

PROJE	СТ	Long <u>Te</u>	rm Operation	al Areas Memphes	Depot LOCATION Memphis, Tennessee	-
ELEVA	TION	304 29 (eet MSL (gro	und)	DRILLING CONTRACTOR Tri State Tectors Service	s Inc
WATER	NG MET!	OD AND	PEQUIP <u>MENT</u> DRY	TUSED HOSOWS START	Rem Auger 4.25 Inch ID with CME Sampler	. =
	BELOW S			STANDARD	10/15/2001 END 10/15/2001 LOGGER SON DESCRIPTION	Jay Parker (Jacobs) COMMENTS
	MIERVA			PENETRATION	XX LESCRIPTION	CHAMPHIS
i i	1	RECOVE	RY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
1	i		s/TYPE	RESULTS	MOISTLIRE CONTENT: RELATIVE DENSITY	DRILLING FLUID LOSS
	l		1	666	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
<u> </u>	<u> </u>			(N)	MINERALOGY	Corrected FID (ppm)
75	:	ł		Used hollow stem		
1	ļ.	į		auger doffing method		1
	!	!		no penetration les		} -
-	i		1	results		i
	!	!				
(!] 	ŀ			ľ
	i i	i		<u> </u>		-
80 <u>_</u>		1				00 _
i i	i	! 	ļ		Sand gravely moist, brown firm grained	Į.
		100	ĺ	Ī		-
1 :		100]		
l -i	i					i
] !	!!!	ı				Sample collected for SVOCs
۱., ۱			•		Iron stone swam, 2" with cobbles and fine sand matrix, brown	1
85	i					• 0
	!!					_
li	;					_
. !)					-
li					Sand some gravel reddish brown moist line-grained	
l i	i i				Same and Angel 1900 m more marketing	
90						ĺ
- <u>- </u>	ì					_ 00 _
-!	!				Damp @ 91 - 92"	<u>-</u>
	:	100				Sample collected for SVOCs
l i	i				CLAY very sandy some quivrel/trown most plastic	_
!	!!					
	·				+	
95_	į					0.0
					SAND clayey most reddish brown matted yellowish brown, some gravel	_
i	i					-
!	!	1			SAND as above more day with some gravel	Sample collected for SVOCs
-1	i	Ī				Sample conecide for SVOCS
i	i			i		
_	!	i		L		0 0
¹⁰⁰ –	i	ľ		ľ	CLAY suff-monst, medium phisticity-medium brown-same sand/gravel	
_į	į		- 1			
- !		100				
-i	i					
- <u>!</u>	!		i i	ŀ	i	
-i		- 1		1		
105	i	i				
·!	. !			J		-
-i	i		I	}		. !
i	i	1	i	k	TLAY as above breaming gray	-
].]	ľ		k	SORING TERMINATED (\$) 107 FEET BGS	
-1			Į.	!	i	-!
-1		ļ	ł	ł	1	_1
110	J	- 1	- 1	i	 	1
- 1				ŀ	†	
				L		



PROJECT NUMBER 160492.SA.03	BORING NUMBER SB-106	
	SOIL BORING LOG	

PROJE				al Areas Memphis		
ELEAV.	TION	31181f	eet MSL (grou	##d)	DRILLING CONTRACTOR Tri State Testing Service tem Auger 4.25 inch ID with CME Sampler	s <u>inc</u>
	LEVELS		DRY	STARY	10/16/2001 END 10/16/2001 LOGGER	Jay Parker (Jacobs)
		JRFACE (STANDARD	SOIL DESCRIPTION	COMMENTS
•	NIFRVA			PENETRATION		
į.		RECOVE	RY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR.	DEPTH OF CASING DRILLING RATE
ı		[""	a/TYFE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS
1 .	ł	Ī	-	6-6-6-6	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
1 ;	ł	l	1	(N)	MINERALOGY	Corrected FID (ppm)
					6* Asphalt and gravel	(Soil headspace)
1 1	j		1 .	Used Indiaw stem	Clayey SILT drown 7.5 YR 4.3 medium saffnon plastic damp	
] !	!	!	!	drilling method		
1	ł	1	j	no penetration test results		1
l i	i	i	ŀ	resour		1
1 _{	ļ	100		·		
1.	!	!				00
°-	i	i		i		-
i i	j i	i	:			-
1 !	!!!	!				_
-					Clayey SiLT brown 7.5 YR 4/4 with piniush-grey 7.5YR 6/2 mortles, medium,	
I -i	i	i			suff non plastic dry	i -
l i	į l	1				
] -						
l 10 —						00 -
l i	į į	i				
]	ļ					1
1 -:	: :	100				1
l j	i i	i				i -
		1	i		Clayey SILT brown 7 SYR 4/5 medium stiff non plastic dry	1
15						00
l i	i i					
l - <u>1</u>	!!]
J -:					Ckeyey SILT same as above damp	-
i i	i				Carrier SIC1 Salies as applied county	4
	ı i					1
!!				1		1
20						0 ● _
<u> </u>	i					
l !	. !					1
l -¦						1
l i	i					JEG @ 23 feet
!	- {					Perchind water
1 :				l		
25 _	1			l		00 _
l!	ì				Sundy SILT strong brown 7 5YR4/6 soft, slightly plastic damp becoming]
!	. !				sandy with depth	1
1 !				1] _
li	i	100]
-i	į					1 1
!!						i -l
30	i					l 00 l
30	i				@ 30 feet, becomes moded dark red 2 SYR3/6 and reddish yallow stiff dry	
!					• •	į l
		- 1]			l l
- ¦	i	Į	1			j 1
i	i	ļ				į l
!	!	1				[j
	1	l	- 1			
35	i	l	l	1	@ 35 feet, dark rad salty SAND very fine damp stiff to very stiff	
!	į	- 1	l	i	Can the man and an area to have a section and and	j i
	i					



PROJECT NUMBER	BORING NUMBER	
160492 SA.03	SB-106	
	• · · · · · · · · · · · · · · · · · · ·	

PROJE				il Areas - Memphis		
ELEVA1			et MSL (grou		DRILLING CONTRACTOR Tri State Testing Se	rviors_inc_
					em Auger 4 25 inch ID with CME Sampler	SER Jay Parker (Jacobs)
	LEVFLS		DRY	START		COMMENTS
		JREAGE (• •)	STANDARD	SOIL DESCRIPTION	COMMENTS
I	INTERVA			PENETRATION		
	l	RECOVE	HY [%]	TEST	SOIL NAME, USGS GROUP SYMBOL, COLOR	DEPTH OF CASING DRILLING RATE
	l		#/TYFE	RESULTS	MOISTURE CONTENT. RELATIVE DENSITY	ORILLING FLUID LOSS
	l		1	6. 6. 6. 6.	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
L	<u> </u>		<u> </u>	(N)	MINERALOGY	Corrected FID (ppm)
	ı	t	İ	Used hollow stem	Clayey Sil T as above to 40"	
		!		auger		i -
_	ł	i E	1	drilling method		
l	i	i	ł	no penetration test		
40 _	í	į	1	results	SAND red 2 5YR4/8 fine loose damp	-—- "" -
1	1				South 160 2 3 11/4/0 lane tourse training	1
1 7	!	ļ .	i	•		
1	!	100	1			-
1	i	:				
f -	i	i				2 5 intervals
1 -	i	i	i			-
45	ļ	ļ	1	İ		0.0
1 3	!	!	1		Mortled SAND 5YR 5/8 yellowish red and reddish yellow 7 5YR 7/8	
1	ł		1		,	-
1	i	i]			
1 :	i	Í	1	•	SAND mottled as above time to medium loose dry	- 1
1 _	1	ſ	1]	or the manual of a decrease the second of th	! _j
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1 -	:	!)	1		
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	!	!				
		:				
	i	i		;		_
1 7	i	i		ľ	Gravelly SAND reddish yellow 7.5 YR 6/8 fine loose dry SOD angular	grave
1	ļ	ı		,	-15%	
	!	!]			
1 7	!			j		1 7
60 _	:					00 _
1 1	i	i				
1 i	1				Gravelly SAND: becoming less gravelly and redder color	-
1 _!	!	100		ì	,]
1]	!	!	ļ			1 .
1 :		!	ĺ			-
	í	•				
I . i	i	i			Sandy Gravet luose dry no color change	
65_	i	j				••
1 :	!	! .				
	. – – –					-
1 :	,				Sandy Gravel same as above	
I -i	i					-
Į į	1					
1 [ļ			[
70 _	!	[[00
1 :	!		,	,		
-:	i	:		i	SAND 10YR 6/8 brownish yellow line loose dry trace gravets	
l i	j .	75		:	SANDY GRAVEL same color fine to coarse loose	
i)			i	subround to sublingular gravel	
-!		!		į į		-1
					<u></u>	



PROJECT NUMBER
160492.SA.03
BORING NUMBER
SB-106

PROJE				af Areas _ Memotirs		
ELEVA	TION	311 81	feet MSL (gro	und) Tusen Hattaiis	DRILLING CONTRACTOR Tri State Testing Service from Auger 4.25 inch ID with CME Sampler	s, inc
WATER	RLEVELS	XVV M N	DRY	START	10/15/2001 END 10/16/2001 LOGGER	Jay Parker (Jacobs)
	RELOW S			STANDARD	SOR DESCRIPTION	COMMENTS
1	INTERVA		·	PENETRATION		COMMENTS
1	1	RECOVE	RY (%)] r⊵s⊤	SOIL NAME USOS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
i i]	İ	MTYPE	RESULTS	MOISTURE CONTENT: RELATIVE DENSITY	DRILLING FLUID LOSS
1	l	ı	ŀ	666-	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
└	Ļ	<u> </u>	ļ	(N)	MINERALOGY	Corrected FID (ppm)
75	1	<u>!</u>	ł	Used hollow stem		• •
1	i	i	J	auger		1
	! !	1		drilling method	SAND 10YR 6/8 brownish yellow fine louse dry trace gravets	-j
	 	ł		results		_i
1	i i	i	i		Gravetly SAND yellow 10YR 7/8 fine to coarse loose dry to moist gravet a zones up to 40% subangular to subrounded	
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.!	1				Gravelly SAND to 89 5	Sample collected for VOCs
i i	i			ľ		!
į	į			l l		1
-!	·					-
90 _	i				6* of reddish yellow CLAY	00
!	į			<u></u> !	CLAY firm interbeds of organics. Pear and CLAY clay is sandy sift pearly	
-1				ŀ	CLAY blush gray hard to ver stiff black in places	-1
i	i	100		ŀ		
!	!					_
i :	-			Į.		
j	j	ì		j.	PEAT sharp break at -94	
95 _!	!	ŀ	j			00 _
-i	i					
į	j			l:	*EAT and CLAY at 94" very organic looking black. Iofiated, fine beds of sitty grity. CLAYS, with fine sand.	1
-1		ľ	l l		SORUMG TERMINATED @ 97 FEET BGS	l i
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PROJECT NUMBER	BORING NUMBER	
160492 SA 03	MW-107	
	SOIL BORING LOG	

PROJEC	CT	Long Ter	rm Operations	al Areas Memphis I	Depot LOCATION Memphis Termissine	
ELEVAT	TION	304 92 %	eet MSL (TOO	C) 305 18 feet MSL	(ground) DRILLING CONTRACTOR Tri State Testing Servi	pes, Inc
	NG METH	HOD AND	EQUIPMENT	T USED Hollow St	tem Auger 4.25 inch ID with CME Sampler	
WATER	tt FVELS	114 43	feet BTOC (1	11/2001) START	10/17/2001 END 10/18/2001 LOGGEI	
DEPTHE	BELOW SI	URFACE (1	FT)	STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERVA	T (FT)		PENETRATION		
		RECOVE	BY (%)	TEST	SOIL NAME USCS GROUP SYMBOL, COLOR,	DEPTH OF CASING DRALLING RATE
!	1		#/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	DRILLING FLUID LOSS
	1	ĺ		6. 6. 6. 6.	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
	}	1		4	MENERAL OGY	Corrected FtD (ppm)
	ــــــــــــــــــــــــــــــــــــــ	<u>!</u>	├ ──	(N)	Fill Clayry St.T brown non-plastic damp 3.5 to 4.5 some CLAY gray slightly	(Soil headspace)
!	!	!		Used hollow stem	plustic damp medium stiff	1000,0000000000000000000000000000000000
- 1	! !	!		auger	,	
1	:	i		drilling method]
i	i	i		no penetration test results		· 1
-	i i	i		16-30-13		-
[į į	ĺ 100				_i
	•	ľ		<u> </u>		
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!	!	!		ļ '		
ا_ ا	!			Į '		
1	!	1		j '	Clayey SILT dark yellowish brown 10YR 4/4 slightly more clay than above	
i	i :	i		ļ '	medium stiff slightly plastic	
ì	i	i				<u>[</u>
i	i i	i		<u> </u>		-
10	i i	i		<u> </u>		0.5
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i i	i i	į	'	1		l l
, - ₁	j,	ĺ	'	[Citayiny SILT is ame as above idark yellowish brown 4/6 more sitty than above	1
<u> </u>	i I	ĺ		ļ ,	medium stiff damp	<u>_</u>
· -		ı	'	ļ ,		
[t ·	1	į į		_
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20!	!	į		l r		48 _
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!	!	!	4 '	1		
_;		100	i '	'		_!
;		<u> </u>		1		
;		:		1 /		JEG @ 23 feet _
l i	í i	í	,	1 1		Perched water
-j	í i	í)	1		-
25 İ	i i	<u>i</u>	j	1		31
I	i ı	j I		1 /		<u> </u>
	i I	j l		1 /		
	į į)		1 /	i	.
-	!!	! !] !	1 1	Clayey Sti T same as above to 28"	-
ļ	į	!	j !	1 1	CARPEY SHIT Same as accove in 20	
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-!	<u>!</u>	! !	l !	1 1	SANDY SILT brown 7 5YR 4/4 soft medium plestic	- ∤ -
35 _	!	! 1		1 1	damp to most grading coanser with depth	06
	!		! !			
		. I			SILTY SAND now color change, very fine to fine, medium dense/soft	_!
. ;	i	i I		1 1	morsi shightly plastic	



PROJECT NUMBER	BORING NUMBER	·	_
160492.SA.03	MW-107		
-		· · · · · · · · · · · · · · · · · · ·	_

PROJE				nal <u>Areas</u> Memp <u>h</u>		
ELEVA	TION	3 <u>04 92</u>	feet MSt_(70	C), 305 18 feel MS	L (ground) DRILLING CONTRACTOR To State Testing Service	es, Inc
DRILLI	NG MET	HOD AN	<u>D E</u> QUIPMEN	<u>IT U</u> SED Hodow	Stem Auger 4 25 inch ID with CMF Sampler	<u> </u>
				(11/2001) START	10/17/2001 END 10/18/2001 LOGGER	Jay Parker (Jacobs)
DEPTH		SURFACE	(F f)	STANDARD	SOIL DESCRIPTION	COMMENTS
1	INTERV	AL (FT)		PENETRATION		
1		RECOV	ERY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
1	1	1	#/TYPE	RESULTS	MOISTURE CONTENT. RELATIVE DENSITY	DRILLING FLUID LOSS
1	ŀ	1	Ī	6-6-6-6	OR CONSISTENCY SOIL STRUCTURE	
	ł		1	(N)	MINERALOGY	TESTS, AND INSTRUMENTATION
		i 	1 —	i —		Connected FID (ppm)
-	i !	į		Used hollow stem auger dnilling method	SAND strong brown 7 SYR 5/8 loose very wire to fine dry, become surnowhat redder and damp at 47"	-
آ ۱	1 1	!		no penetration ter		-
~~ -	!	!	i	results		00 _
l i	ì	i		1		_
i j	i	i 100	ľ	1		1
]	!	!	l	ł		1
	;	i	ł			2 5' intervals
<u> </u>	Ì	į	l	ł	i	2 3 uncerans
45	!	!		i		· -
	·	i	i			13
-i	i i	i		i		1
!	!!	ţ		Į.		1
ľ		:	1	{	Gravelly SAND strong brown 7 SYR 5/6 fine to coarse pebbles to the gravel	1
- <u>;</u>		i			-15% loose wast	
_i	ĺ	i	i	ŀ		1
. !	' !	!	İ	ł		l I
50 _		Ī		ŀ		00 _
	i	i				
i	i			1	SAND strong brown fine to medium some petities loose damp grade finder with	-1
-1		100			depth	
_!						
-:	- :					ŀ
-i	i					_
55 Î	i					1 1
j	ţ				SAND: fine to very fine, no gravel	31
-!	!				•	_
;	i		ĺ			<u> </u>
i'	í				SAND reddish yellow 7 5YR 6/8 fine lonse dry trace pebbles grading coarsi	
-1	ĺ				line to medium at 60' and color change to 10YR 7/6 vellow grades hack to	
. !	ļ.				1st color, medium, more gravel 5% to 10%, up to 2" in size, sub angular grave	
-1						-1
60 —	i	ľ				00
İ	i	J]
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-	ļ	100				í
- 1	i		ļ	1		i I
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	- 1	1		j		°⁴
i	i	j	ŀ			į l
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i		- 1	ļ	J.	cravelly SAND yellow 10YR 7/ti fine to medium toose, dry	j f
4	- 1	- 1]	1	· · · · · · · · · · · · · · · · · · ·	
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-!	!	- 1	!			-1



PROJECT NUMBER 160492.SA 03	BORING NUMBER	MW-107	
	SOIL BORI	NG LOG	

LOCATION Memphis Transesee PROJECT Long Term Operational Areas Memphis Depot
 ELEVATION
 304 92 feet MSL (TOC)
 305 18 feet MSL (ground)
 DRILLING CONTE

 DRILLING METHOD AND EQUIPMENT USED
 Hollow Stern Auger 4 25 inch ID with CME Sampler

 WATER LEVELS
 114 43 feet BTOC (11/2001)
 START
 10/17/2001
 END
 10/11
 DRILLING CONTRACTOR To State Testing Services Inc. LOGGER Jay Parker (Jacobs) 10/18/2001 DEPTH BELOW SURFACE (FT) STANDARD SOIL DESCRIPTION COMMENTS INTERVAL (FT) PENETRATION RECOVERY (%) TEST SOIL NAME, USCS GROUP SYMBOL, COLOR DEPTH OF CASING DRILLING RATE RESULTS MOISTURE CONTENT RELATIVE DENSITY DRILLING FLUID LOSS OR CONSISTENCY SOIL STRUCTURE TESTS, AND INSTRUMENTATION 6. 8. 6. 6. Corrected FID (ppm) MINERALOGY (N) 2 7 75 ._ Gravelly SAND medium moist to wit Used hollow stem auger drilling method no penetrabon les results 00 Same as above, gravelly zones, losse, damp to well 100 85 14 Gravety SAND same as above, some coarser sand zones, damp to moist 90 100 95 GraveBy SAND same as above 48 100 100 105 04 Gravelly SAND same as above

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PROJECT NUMBER	BORING NUMBER	
160492.SA.03	MW-107	
	SOIL BORING LOG	

PROJE	CT	Lang T	erm Operation	al Areas Memphe	Deport LOCATION I	femphis Tennassea		
ELEVA	TION	304 92	leet MSL (TO	C), 305 18 feet MS	(ground) DRILLING CONTRACTOR T	n-State Testing Service		
DRILLING METHOD AND FQUIPMENT USE		USED Fromow Stem Auger 4.25 mon ID with CML Sampler			· " <u>" </u>			
WATER	LEVE	5 1144	3 feet BTOC (11/2001) START	10/17/2001 END 10/18/2001	LOGGER	Jay Parker (Jacobs)	
ОСРТН		URFACE	(П)	STANDARD	SOIL DESCRIPTION		COMMENTS	
1	INTERV			PENETRATION				
	ļ	RECOVI		TEST	SOIL NAME USCS GROUP SYMBOL COLOR		DEPTH OF CASING DRILLING	RATE
ı	ľ	l	MTYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY		DRILLING FLUID LOSS	
	ļ			6-6-6-6	OR CONSISTENCY SOIL STRUCTURE		TESTS, AND INSTRUMENTATE	
 		-	 	(N)	MINERALOGY		Corrected	FID (ppm)
_	i	100	1	Used hollow stem			1	
ļ ;	ı	į	1	auger dritting method				-
1 7	!	!		no penutration tes			•	-
! ;	ľ	:	Į.	results	ł		ı	_
115 _	i	i		1	Sandy GRAVEL loose same color matrix gravel subangular o	up to 2*	Water Table 2	
]	ļ	!					Water Table 2	•
-¦	<u> </u>	:	1 .	j				
l ₋i		i		1]]	
	!	į			Sandy GRAVEL same as above		1	_
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!	!		i					
!	- 1							
i	i							
125 _							1 7	,
!							Sample collected for VOCs	
-i	i				∆ H ₂ O Sand starts			_
ŀ	į				SAND yellow 2 SYR 7/8 very fine to fine loose well sorted no	ogravel mosttowat		_
-1.	!							_
ì	i				SAND same as above. SAND yellow very line to fine loose of	well sorted wet		
-1	i							
!	!							
-:	i			i				
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PROJECT NUMBER 160492.SA 03	BORING NUMBER MW-107	
	SOIL BORING LOG	

PROJE				a Areas - Memphis		_		Mentions Leanies See	· ———————
ELEVA	TION	304 92 f	eet MSL (TOC	305 18 feet MSL	(ground)	DRILLING C	CONTRACTOR	Tn State Testing Services	inc
DRILLIF	IG METH	OD AND	EQUIPMENT	TUSED Hollow Si	tem Auger 4 25 inch fD	with CME Sa	mpler		
WATER	LEVELS	114 43	feet BTOC (1	1/2001) START	10/17/2001	END	10/18/2001	LOGGER	Jay Parker (Jacobs)
	SELOW SI			STANDARD		SOIL	DESCRIPTION		COMMENTS
	INTERVA			PENETRATION					
Ī				1		~ n n	CO1 OD		DEPTH OF CASING DRILLING RATE
		RECOVE		TES1	SOIL NAME USCS GR				
			#/TYPE	RESULTS	MOISTURE CONTENT				DRILLING FLUID LOSS
	l		1	6666.	OR CONSISTENLY SO	XII STRUCTU F	HE.		TESTS, AND INSTRUMENTATION
l	l	l	1	(N)	MINERALOGY				Corrected FID (ppm)
	•								
	i	í	1	Used hollow stem					
	i	i		1					-
	i	i		auger					1
I -	i	l		drilling method					-
	J	l	1	no penetration less					
I _	l)	l '	results					
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-	i	i							Sample collected for TOC
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	į	Ì		!					1
155		l							
i '	!	l							4
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•	!	!		ļ	SAND as above				
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	i	Ì	1		CLAY 2 8YR 6/3 light yes		aro damp verypta	ranc dusquid wags	i l
⊣	ı	1	1		depth to greenish gray. C	LAY S/1			i -
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PROJECT NUMBER
160492.SA.03

BORING NUMBER
MW-108

SOIL BORING LOG

PROJ	ECT .	Long T	erm Operatio	nal Areas Memphis	Depot LOCATION Memphis Tennessee	<u> </u>
ELEV/	ATION	303 07	feet MSL (TC	C). 303 25 feet MSI	(ground) / DRILLING CONTRACTOR In State Testing Superes	inc
DRILL	ING MET	HOD AN	D EQUIPMEN	TUSED Hollow S	lem Auger 4 25 inch ID with CME Sampler	
	BELOW			(11/2001) START	10/22/2001 END 10/23/2001 LOGGER	
LEPIN	INTERV		(F1)	STANDARD	SOIL DESCRIPTION	COMMENTS
	PATERV		FRY (%)	PENETRATION TEST		1
		KECO	A/TYPE	RESULTS	SOIL NAME USCS GROUP SYMBOL COLOR MOISTURE CONTENT RELATIVE DENSITY	DEPTH OF CASING DRILLING RATE
	1	ı	J	6666	OR CONSISTENCY SOIL STRUCTURE	DRILLING FLUID LOSS
		1	1	(N)	MMERALOGY	TESTS, AND INSTRUMENTATION Corrected FID (pgm)
	i 	i	 		Causs clayey SILT brown not slightly plastic damp	(Soil headspace)
	İ	į	1	Used hollow stem auger		
		!		drilling method .		i
	i	i	1	no penetration test results		
	į	100	ľ	resons		ŀ
-	.!	!		i I		
5	:	:	i			1
-	i	i		1 1		18 _
-	.!	!	i]
_	.i	1	ŀ			i
	i	i	l	1	Clayery SILT: same as above most to well, slightly plastic to medium plustic,	1
	ļ.	ļ	1		high clay content	
_	!]	ŀ			
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ľ						JEG @ 23 feet
i	i			ļ		Perched water
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PROJECT NUMBER	BORING NUMBER
160492.SA 03	MW-108

PROJE	CT	Lang Te	m Operation	al Areas Memphis	Depot LOCATION Memphis Tennessee	•
ELEVA	TION	303 07 f	eel MSL (TO	C), 303 25 feet MSI	(ground) DRILLING CONTRACTOR To State Testing Services,	<u>Inc</u>
				TUSED HOROWS	tem Auger 4 25 inch ID with CME Sampler 10/22/2001 END 10/23/2001 LOGGER	 Jay Parker (Jacobs)
	LOW SI			STANDARD	SOIL DESCRIPTION	COMMENTS
	INTERVA			PENETRATION		
	l	RECOVE	RY (%)	TEST	SOIL NAME USCS GROUP SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
ł	l	1	s/TYPE	RESULTS	MOISTURE CONTENT: RELATIVE DENSITY	DRILLING FLUID LOSS
1	l	Į.		ଟ-ଟ-ଟ-ଟ	OR CONSISTENCY SOIL STRUCTURE	TESTS, AND INSTRUMENTATION
—	<u></u>	<u> </u>	<u> </u>	(N)	MINERAL OGY	Corrected FtD (ppm):
		:		Used hollow stern	C'trysry SILT, same as above	
i	i	i	l	auger	Gradas quickly to SILTY SAND (\$38" SYR 5/6	1
1 -	!	<u>!</u>	ŀ	drilling method no penetration less	yellowish red fine dense damp slightly to non plastic matrix holding line sand together seen somewhat clayey/sity	-:
40 _		!		results	•	00
1 i	i	i				<u> </u>
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1 -		!	1			-
1 -i	i	100	1		7. V. S. V. S. V. S. A. Z. V. V. S.	j _
i	i i		i :		SAND rinklish yellow 5YR 6/8, fine to medium loose, damp to moist, well sorted gravel in the beds further down	som:
1 !					•	<u> </u>
1 1		!				
50i	i	i				
1 1			j	r		i -
I -			1		SAND: turns yellow 2 5YR 8/6 with trace grand/small rounded pebbles	
l i	i				,	_l
!!						1
-;						1
-i	i		1			1
55 _!	!					26
! !			l			
J ⁻i	i				i	l
ו ו	!					
1 !	!				SAND 2 5YR 8/6 yellow fine loose damp some to trace fine gravely/petibles at above zones of more grave up to 60 = 15%	1
I -ï	i				accord Lands of those grave up to do_ 15 m	i
-i	i					
60	ļ					I
1 1	i					-
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!	!	J		ľ		
65	ŀ	ì]			!
i i	i	ŀ			CLAY, 6" thick motified gray and red, very plastic	. 7
-!	!			ĺ	SAND 2 5YR 6/6 yellow fine loose damp some to trace fine gravels/probbler	-1
	{	J		ļ		
l i	i	1		İ		Sand at so loose ears: 4:#
-	į	ŀ		ł		Sand is so loose some felt out as sampler was about
-¦	1	l		i		to take sample
70 _i	i	l	Į	l		0.6
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PROJECT NUMBER	BORING NUMBER	
160492 SA.03	MW-108	
		•

PROJE				nal Areas Memphis		
				C) 303 25 feet MSL		inc
				ITUSED HollowSI 11/2001) START	Stern Auger 4 25 inch ID with CME Sampler 10/22/2001 END 10/23/2001 LOGGER	Jay Parker (Jacobs)
	BELOW SI			STANDARD	SOIL DESCRIPTION	COMMENTS
ł	INTERVA	AL (FT)	_	PENETRATION		
1	1	RECOVE		1651	SOIL NAME USCS GROUF SYMBOL COLOR	DEPTH OF CASING DRILLING RATE
		1	#/TYPE	RESULTS	MOISTURE CONTENT RELATIVE DENSITY	ORBLEING FLUID LOSS
		1	Į į	(N) 6666.	OR CONSISTENCY SOIL STRUCTURE MANERALOGY	TESTS, AND INSTRUMENTATION Corrected FID (ppm)
$\vdash \vdash$	₩	 	 			
75	;	i]	Used hollow stem	<u>. </u>	14
,	į į	į '		augre drilling method	SAND same as above turns redder	İ
['	1			no penetration test	•	1
-1	i	i	1	results	Gravelly SAND yellowish brown 10YR 5/6 medium to coarse loose damp to m	l norst
<u>'</u> -		1	1 /	,	fine to coarse gravets rounded to sub angular	
į j	i i	í I	1	1 '	1	Ι,
'	į į	į i	[1 '	1	1
80 [1 7	<u> </u>] /	4 '	,	06 _
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!!!	į į	į į	1 !	1 1	1	f -
-		<u> </u>	1 /	i i	Black stained area loey slight hydro-carbon order 6° band	At 83 5 readings were 0 0/0 0
85	i j	i j	1 /	1 1	1	10
	! !	! !	1 /	1 1	1	1
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<u> </u>	!!	1	l j	1 1	<u> </u>	ĺ
1 ;		; !	1 1	1 1	Fine SAMD at 87 to 89	1
i	i j	i 1	1 1	1 1	1	1 -
- !	! !	! !	i 1	1 1	Stry Clayey SAND very pale brown 10YR 7/4 motiled with white very fine well to	1
90 _	i j	i J	1 1		most, slightly plastic medium stiff	_ 00 _
l ļ	, ,	<i>!</i>	í j	i j	l I	i
1 ;			i 1	1 1	1	ĺ
i -j	į	100	i 1	1)	1	-
!	! }	: J	i 1	1 1	A TOTAL TO A LOCAL TO	- 1
ز ا	i	, J	i	1)	SAND with gravel strong brown 7 SYR 5/6 loose moist to wet line to medium gravel = 5% up to 2*	l
	, ,	, J	i j	1 1	1	1
95_		i J	i J	i 1	1	1.4
_	į	, 1	i	1 1	1	-
_ !	!!	.)	i J	1 1	1	Sample collected for VOCs
i	i	. !	i J	1 F	Gravelly SAND: pale yellow 2:54.7/4 medium to coarse, loose wet.	1
- <u>i</u>	. !	.]		1 1		Sample fell out while bringing it to
-	. 1			i j	l l	the surface. Sample lost at
100 _	į	. 1		ı J		H2O Contact, guess ∆ to be at = 100' 0 0
,``` -	. !	.]		ı J	1	1
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<u>-</u> !	į	60	. 1	ı J	1	1
	. :	. 1			1	_
ì	i	1	Ī	ı J	1	1
-!	. !	1	I	ı J	ı J	1
105	· i	}	Ī	ı J	1	<u> </u>
<u>.</u>	į	1			ı J	1
	. !	- 1	. 1	ı [,	1
i	i	1	. [ı	-
. 1	i	l		. ! '	SAND light olive brown 2 5YR 5/6 fine loose wet trace gravet up to 2"	ı
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i.	į			ı	,	-
110	!	[, <u>†</u>	ı	-
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PROJECT NUMBER 160492.SA.03	BORING NUMBER MW-108	
	SOIL BORING LOG	

PROJE	CT	Long Te	m Operation:	ol Areas Memphis	DepotLOCATION Memphis Terr	M-2-24-6	
ELEVA	TION	303 07 1	ect MSL (TOC), 303 25 feet MSL	(ground) <u>DRILLING CONTRACTOR</u> Tri State Tester	g Services, I	nc
		IOD AND	EQUIPMENT	USED Hollow Si	tem Auger 4 25 inch ID with CME Sampler		
				1/2001) START	10/22/2001 END 10/23/2001	LOGGER	Jay Parker (Jacobs)
		URFACE (STANDARD	SOIL DESCRIPTION		COMMENTS
	INTERV			PENETRATION			
[1	SOIL NAME, USCS GROUP SYMBOL COLOR		DEPTH OF CASING DRILLING RATE
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	ļ	ļ	1		nonplastic stiffidense wet, high day content		
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PROJECT NUMBER	BORING NUMBER	
160492.SA.03	MW-108	
	SOIL BORING LOG	

								
PROJE				<u>nal A</u> reas M <u>rmph</u>		LOCATION Mem	phis, Tennessee	_
E LEAN	TION	_ 303 07	frei MSL (TC	C) 303 25 feet MS	L (ground)	DRILLING CONTRACTOR In St	ate Testing Services	Inc
DRILLII	NG MET	HOD AN	D EÖNI SM EN	IT USED <u>Holkow</u>	Stem Auger 4 25 incl	h ID with CME Sumpler		
WATER	RLEVEL	S 1132	1 feet BTOC	(11/2001) START	10/22/2001	END 10/23/2001	LOGGER	Jay Parker (Jacobs)
		URFACE	(FT)	STANDARD		SOIL DESCRIPTION		COMMENTS
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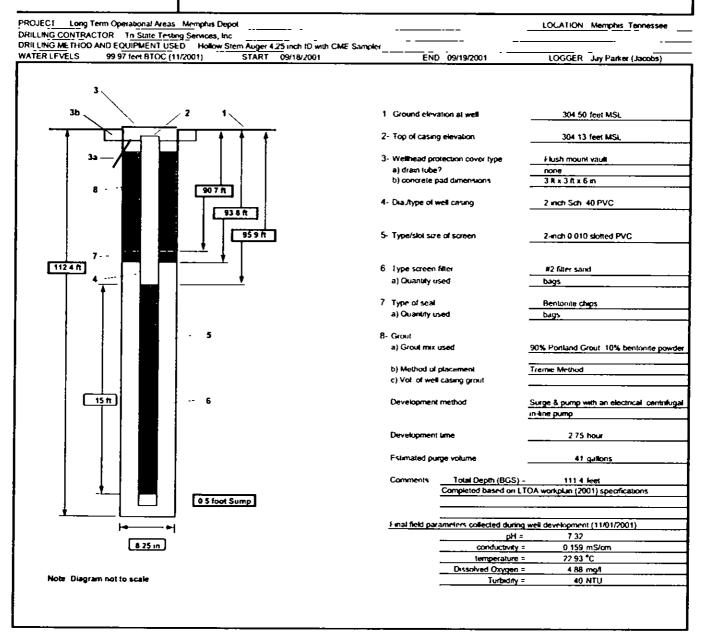
PROJECT NUMBER	BORING NUMBER	
160492.SA 03	MW-108	
	SOIL BORING LOG	

PROJECT	Long To	m Operation	al Areas Memphis			komphis, Te <u>nnessee</u>	
ELEVATION	303 07 9	leet MSL (TO	C), 303 25 feet MSI	(ground)	DRILLING CONTRACTOR TO	n-State Testing Services	hnc
DRILLING ME	THOD AND	EQUIPMEN	TUSED Hollow S	Stem Auger 4.25 inch ID	with CME Sampler		
WATER LEVE	LS 113 21	l feet BTOC (11/2001) START	10/22/2001	END 10/23/2001	LOGGER	Jay Parker (Jacobs)
DEPTH BELOW	SURFACE (FT)	STANDARD	T	SOIL DESCRIPTION		COMMENTS
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Attachment 2 – LTOA Well Completion Diagrams



PROJECT NUMBER	WELL NUMBER	
160492.SA.03	MW-85	SHEET 1 OF 1
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PROJECT NUMBER	WELL NUMBER	
160492.SA.03	MW-86	SHEET 1 OF 1

WELL COMPLETION DIAGRAM

PROJECT Long Term Operational Areas Momphis Depot DRILLING CONTRACTOR Tri-State Testing Services Inc. LOCATION Memphis Tennessee | DRILLING CONTRACTOR | TIPSCHIE | TESANS SERVICES | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 --END 09/21/2001 LOGGER Adam Kaiser (Jacobs) 3 304 89 feet MSL 3Ь 1- Ground elevation at well 2- Top of casing elevation 304 35 feet MSL 3- Wellhead protection cover type Flush mount vault a) dram tube? 3 ft x 3 ft x 6 m b) concrete pad dimensions 92 ft 4- Dia/type of well casing 2 ench Sch. 40 PVC 95 5 R 97 S ft 5- Type/slot size of screen 2-mch 0 010 slotted PVC 118 N 6- Type screen Atter #2 filter sand a) Quantity used bags 7- Type of seal Bentonite chips a) Quantity used bags 8 Grout a) Grout mux used 90% Portland Grout 10% bentonite powder Tremie Method b) Method of placement c) Vol. of well casing grout 20 ft Development method Surge & pump with an electrical centrifugal in line pump Development time 2.5 hour Estimated purge volume 38 gallons 117 5 feet Total Depth (BGS) = Comments Completed based on LTOA workplan (2001) specifications 0 5 foot Sump Final field parameters collected during well development (10/31/2001) pH r 6 38 8.25 in 0 139 mS/cm conductivity = 27 58 °C lemperature = Dissolved Oxygen # 5 54 mg/l Note Diagram not to scale Turbidity = 22 NTU



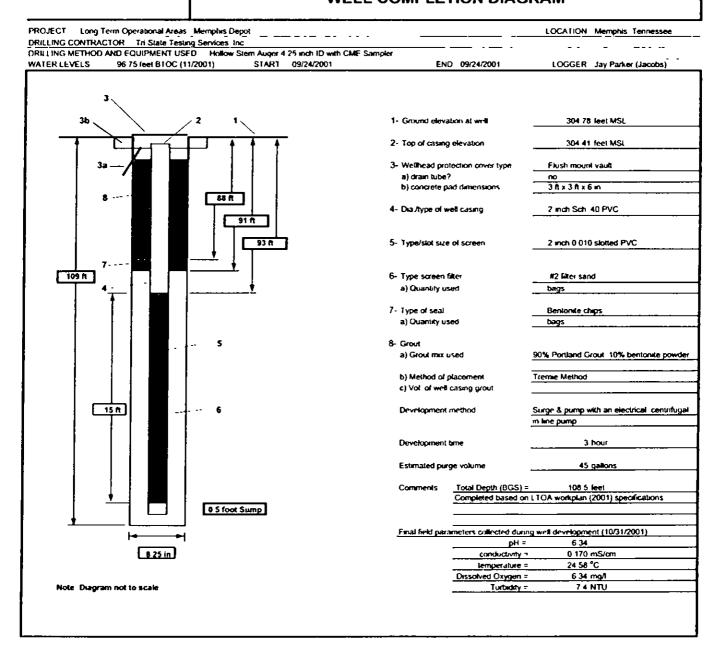
PROJECT NUMBER
160492.SA.03 WELL NUMBER
MW-88 SHEET 1 OF 1

WELL COMPLETION DIAGRAM

PROJECT Long Term Operational Areas Memphis Depot
DRILLING CONTRACTOR Tri-State Testing Services Inc
DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4 25 inch ID with CME Sampler LOCATION Memphis, Tennessee LOGGER Jay Parker (Jacobs) WATER LEVELS 80 98 feet BTOC (11/2001) START 09/20/2001 END 09/21/2001 3 36 305 47 feet MSL 1- Ground elevation at well 2- Top of casing elevation 305 15 feet MSL 3- Wellhead protection cover type Flush mount vault a) drain tube? b) concrete pad dimensions 3 ft x 3 ft x 6 m 4- Dia /type of well casing 2-inch Sch. 40 PVC 79 8 R 82 ft 5- Type/slot size of screen 2 inch 0 010 slotted PVC 98 2 ft 6- Type screen filter #2 filter sand a) Quantity used bags 7- Type of seal Bentonie chips a) Quantity used bags 8- Grout a) Grout mix used 90% Portland Grout, 10% bentonite powder b) Method of placement Treme Method c) Vol. of well casing grout 15 A Development method Surge & pump with an electrical centrifugal in tine pump Development time 8 hour Estimated purge volume 48 gallons Comments Total Depth (BGS) = 97 5 feet Completed based on LTOA workplan (2001) specifications 0 5 foot Sump Final field parameters collected during well development (11/02/2001) ρH ≖ 7 10 8 25 in conductivity = 0.280 mS/cm 26 33 °C temperature = Dissolved Oxygen # 5 18 mg/l Note: Diagram not to scale >1000 NTU Turbidity =

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ROJECT NUMBER	WELL NUMBER		
160492.SA 03	MW-92	SHEET 1 OF 1	
WE	COMPLETION DIAGRAM		





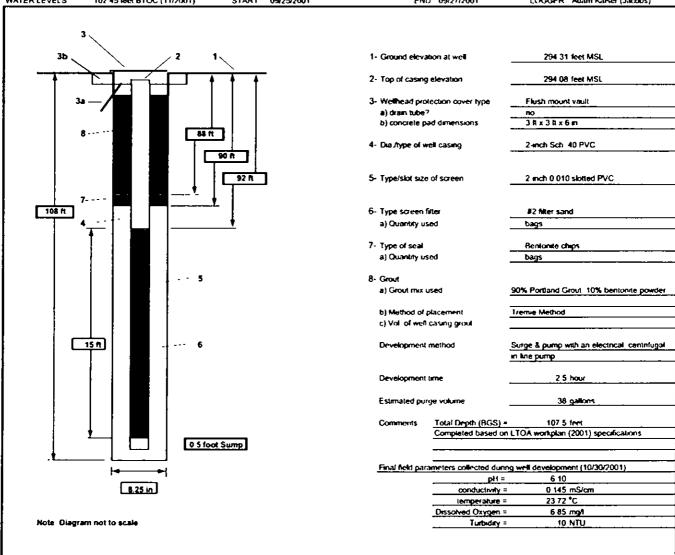
PROJECT NUMBER WELL NUMBER MW-93 160492.SA 03 SHFET 1 OF 1

WELL COMPLETION DIAGRAM

PROJECT Long Term Operational Areas Memphis Depot

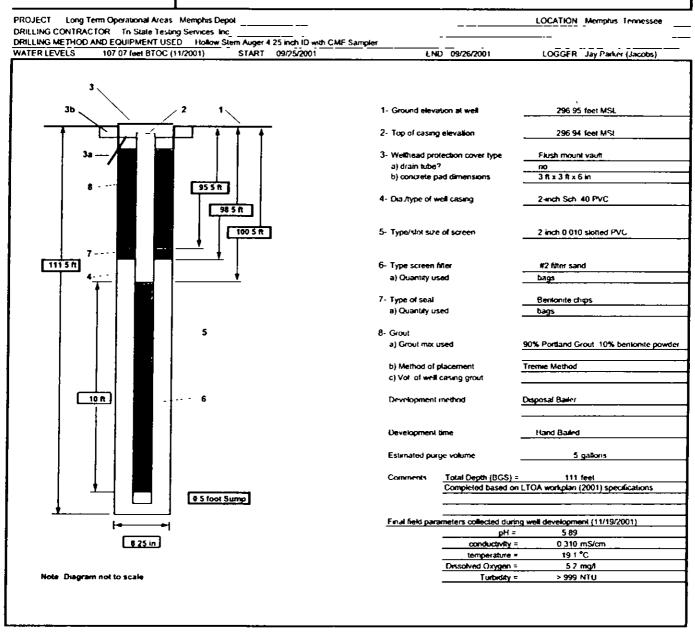
LOCATION Memphis Tennessee

PROJECT Long Term Operational events of the DRILLING CONTRACTOR Tri-State Testing Services Inc DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4.25 inch ID with CME Sampler 102.45 feet BTOC (11/2001) START 09/25/2001 END 09/27/2001 LOGGER Adam Kaiser (Jacobs)



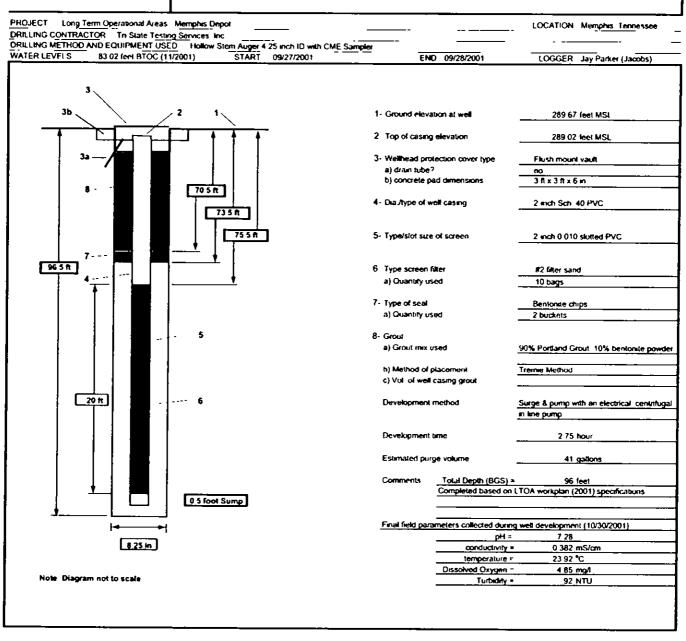


PROJECT NUMBER	WELL NUMBER		
160492.SA 03	MW-94	SHEET 1 OF 1	
WELL COMPLET	ON DIAGRAM		



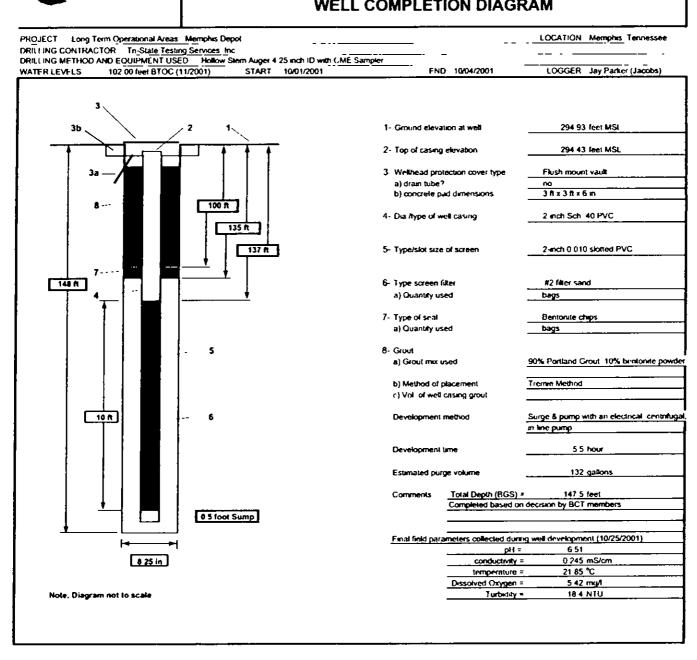


PROJECT NUMBER 160492.SA.03	WELL NUMBER MW-96	SHLET 1 OF	1
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PROJECT NUMBER	WELL NUMBER	
160492 SA.03	MW-98	SHEET 1 OF 1
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PROJECT NUMBER

160492.SA.03

WELL NUMBER

MW-97

SHEET 1 OF 1

WELL COMPLETION DIAGRAM

PROJECT Long Term Operational Areas Memphis Depot **LOCATION Memphis Tennessie** PROJECT Long Term Operational reader Services, Inc.

DRILLING CONTRACTOR Tri State Testing Services, Inc.

DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4.25 inch 1D with CME Sampler

401.25 feet RTOC (11/2001) START 10/01/2001 END 10/03/2001 LOGGER Adam Kaiser (Jacobs) 3b 1 Ground elevation at well 297 70 feet MSL 2- Top of casing elevation 297 44 feet MSL 3- Wellhead protection cover type Flush mount vault a) drain tube? по 3 ft x 3 ft x 6 m b) concrete pad dimensions 93.5 ft 4- Dia /type of well casing 2 mch Sch 40 PVC 95 5 ft 97 5 ft 5- Type/slot size of screen 2-inch 0 010 slotted PVC 118 5 ft 6- Type screen filter #2 filter sand a) Quantity used hags 7- Type of seal Bentonite chips a) Quantity used bags 8- Grout a) Grout mix used 90% Portland Grout 10% bentonite powder b) Method of placement Treme Method c) Vol. of well casing grout 20 ft Development method Surge & pump with an electrical centrifugal in line pump Development time 4 hour Estimated purge volume 72 gallons Total Depth (BGS) = 116 feet Comments Completed based on LTOA workplan (2001) specifications 0.5 foot Sump Final field parameters collected during well development (10/22/2001) 6 4 1 pH = 8,25 in conductivity = 0 162 mS/cm 21 14 °C temperature = Dissolved Oxygen = 5 mg/l Note Diagram not to scale Turbidity = **19 NTU**



PROJECT NUMBER

160492 SA.03 WELL NUMBER

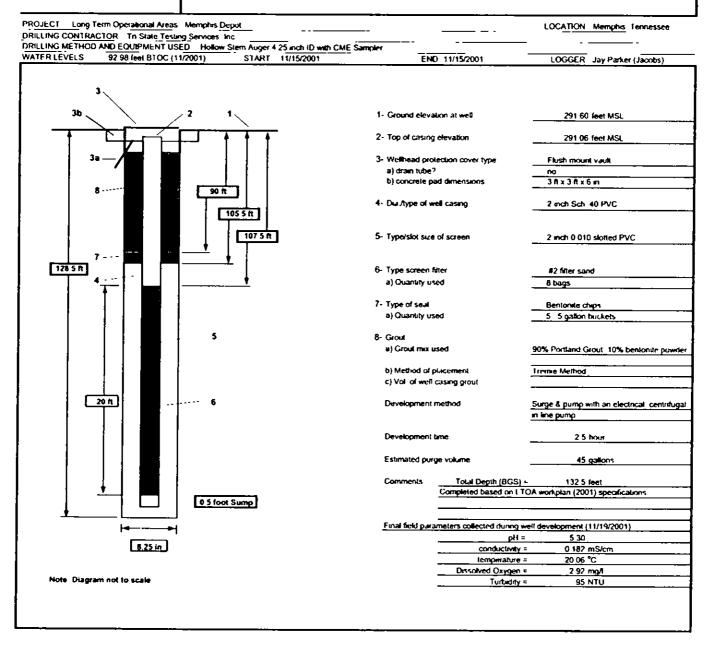
MW-99 SHEET 1 OF 1

WELL COMPLETION DIAGRAM

LOCATION Memphis Tennessee PROJECT Long Term Operational Areas - Memphis Depot DRILLING CONTRACTOR Tri-State Testing Services Inc. DRILLING METHOD AND EQUIPMENT USED Hollow Stem Auger 4 25 inch ID with CME Sampler WATER LEVELS 89 60 feet BTOC (11/2001) START 10/05/2001 END 10/08/2001 LOGGER Adam Kaiser (Jacobs) 3Ь 1- Ground elevation at well 285 69 feet MSL 2- Top of casing elevation 285 33 feet MSL 3- Wellhead protection cover type Flush mount vault a) drain tube? 3ft×3ft×6an b) concrete pad dimensions 87 5 N 4- Dia Aype of well casing 2-inch Sch. 40 PVC 89 5 ft 91 5 ft 5- Type/slot size of screen 2 mch 0 010 slotted PVC 112 5 H 6- Type screen filter #2 filter sand a) Quantity used 9 bags 7- Type of seal Bentonite chips a) Quantity used 4 5 gallon buckets, 2 5 bags 8- Grout a) Grout mix used 90% Portland Grout 10% bentonte powder 9 bags b) Method of placement Treme Method c) Vol. of well casing grout 20 ft Surge & pump with an electrical centrifugal Development method in line pump Development urne 4 5 hour 81 gallons Estimated purge volume Comments Total Depth (BGS) = 118 feet Completed based on LTOA workplan (2001) specifications 0 5 foot Sump Final field parameters collected during well development (10/23/2001) рН т 6 57 8,25 in conductivity = 0 173 mS/cm 20 13 °C lemperature = Dissolved Oxygen -506 mg/l Note: Diagram not to scale Turbidity = 7 9 NTU

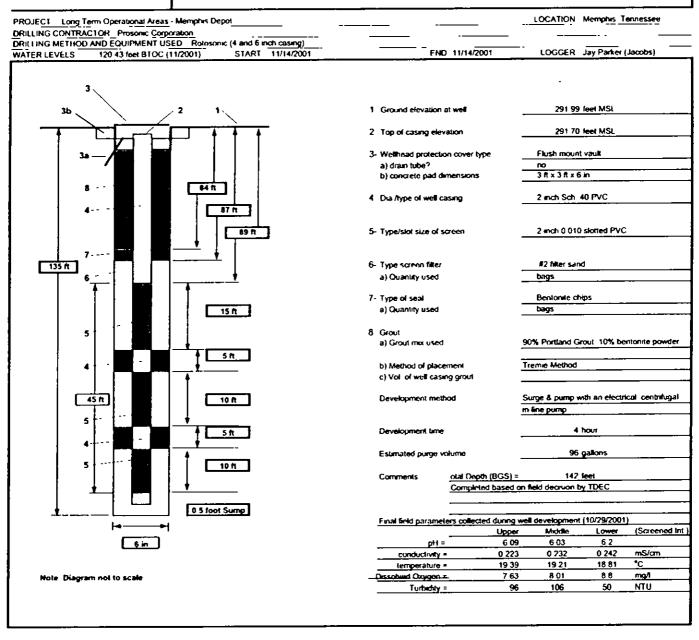


PROJECT NUMBER	 WELL NUMBER	
160492.SA.03	 MW-100	SHEET 1 OF 1



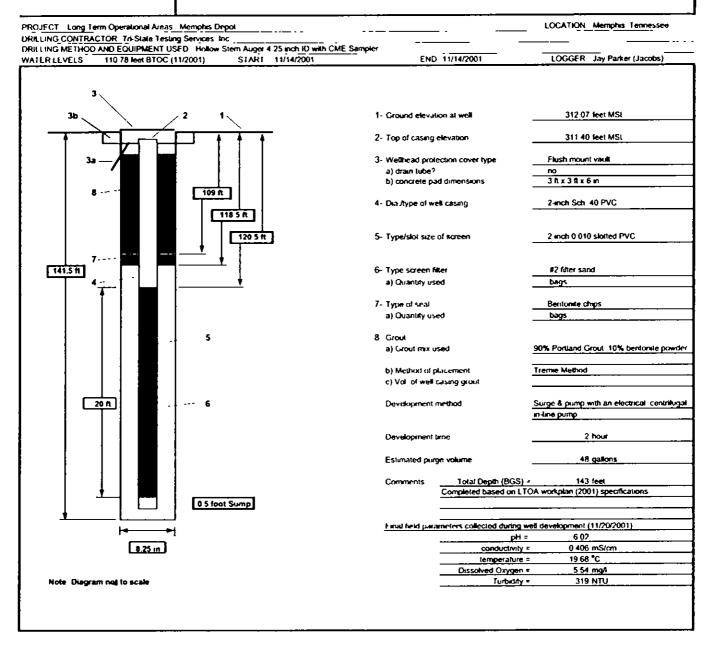
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PROJECT NUMBER 160492.SA.03	WELL NUMBER MW-101	SHEET 1 OF 1
WELL	COMPLETION DIAGRAM	





PROJECT NUMBER WI	ELL NUMBER	
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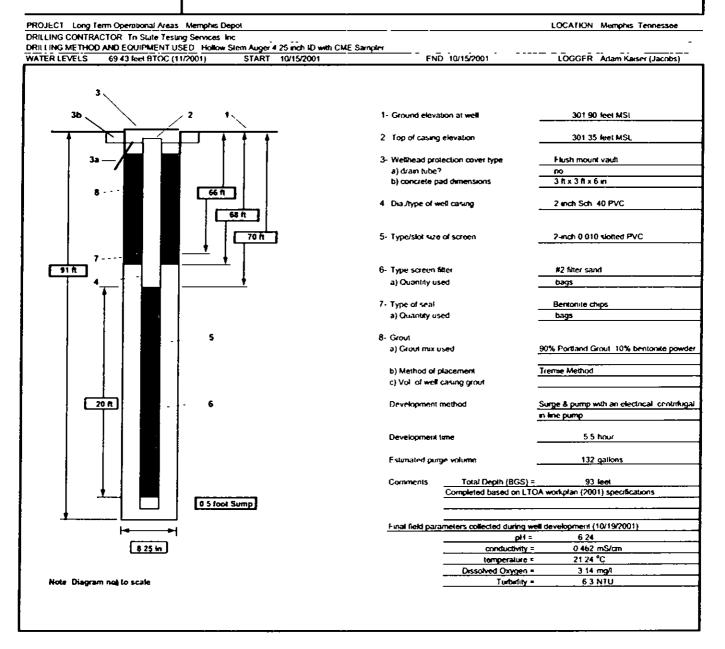




PROJECT NUMBER

160492.SA.03 WELL NUMBER

MW-103 SKEET 1 OF 1



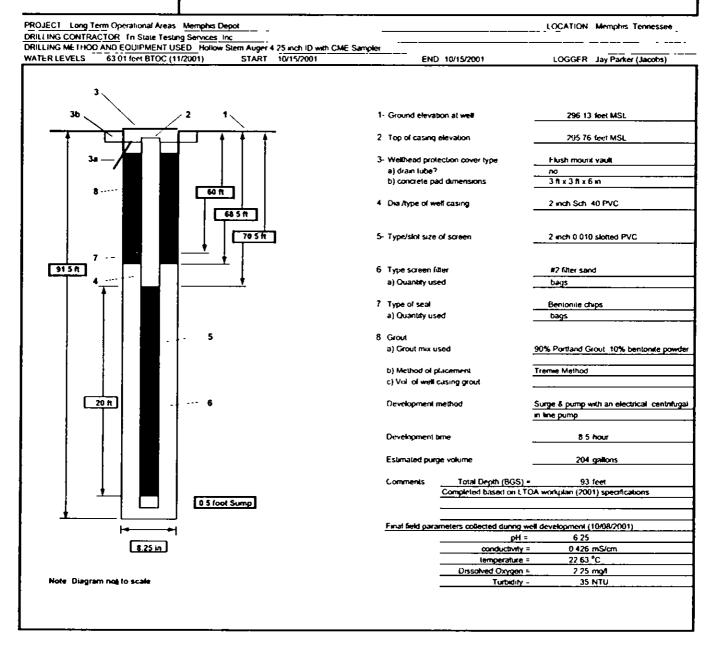


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160492.SA.03 WELL NUMBER

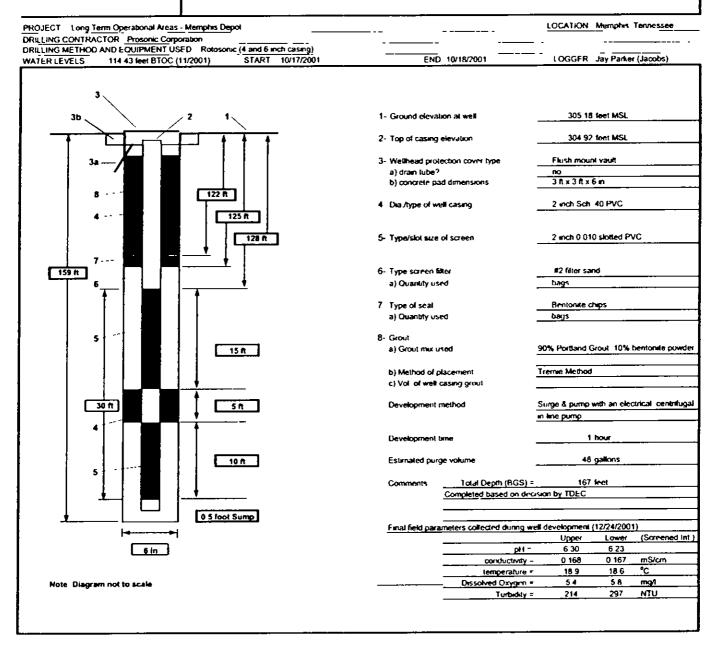
MW-104 SHEET 1 OF 1

WELL COMPLETION DIAGRAM





PROJECT NUMBER 160492.SA.03	WELL NUMBER MW-107	SHEFT 1 OF 1
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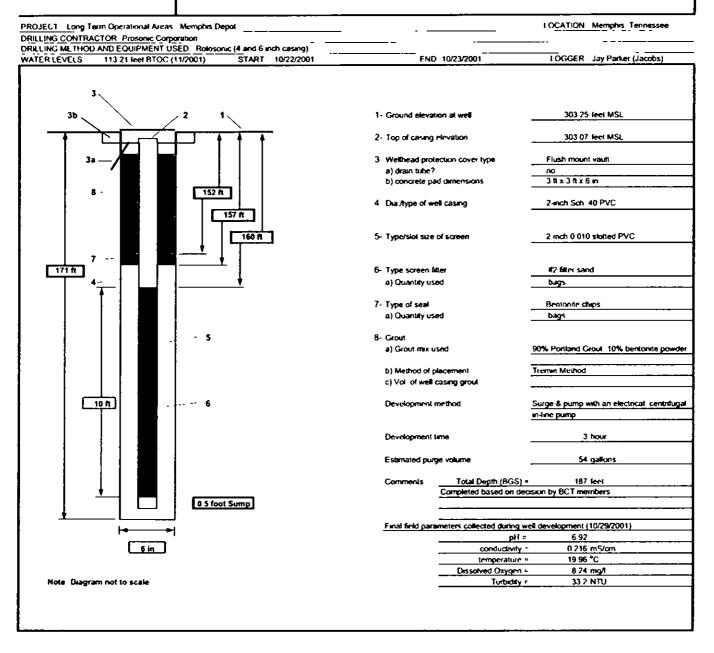
160492.SA 03

WELL NUMBER

MW-108

SHEET 1 OF 1

WELL COMPLETION DIAGRAM



Attachment 3 – Detected Soil Analytical Results Summary

Qualifier 8 8 ဗြ \circ 유민의 \mathbf{Q} UGWG UGWG UGWG UGWG **UG/KG** UG/KG LG/KG UGAKG SOKG. UQ/KG UCKG UG/KG UGAG UGAKG UGAKG UGVKG UGKG UGKG UGKG UGKG UGAKG UGAKG UG/KG UGAKG UG/KG UG/KG UG/KG UG/KG UG/KG UQVKG UG/KG UGAKG UG/KG UG/KG UG/KG UG/KG UGAKG UG/KG UG/KG UG/KG ONYON ONYOU Units Reporting Detection Limit 23. 0073. 0072. 0072. 0073. 00 Qualifier Fings Final Resuit 58 13 085 12 8 8 089 27 25 055 16 16 13 12 17 Laboratory Laboratory Result Qualifier Bromo'orm Carbon tetrachonde Chloro'orm as-12 Oichlorathana ds-1 2-Dichloroethene Acetone
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Tolvene
Acetone
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2 Butanone Carbon tetrachlonde Tetrachloroethene Tetrachloroethene Methylene chlonde Tetrachloroethene Carbon disulide Inchloroethene 2-Butanone Bromoform Toluene 2-Butanone Acetone Bromoform Acetone Bromoform Toluene 2-Butanone 2-Butanone 2-Butanore Chloroform 2-Butanone Parameter Bromoform Bromotorm Bromotorm Bromotorm Bromcform Bromoform Bromo'srm Toluere Tokuene Toluene Toluere Toluene Bromo'orm Acetore Acetore Toluene Acetone Analytical Method SW8260B
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Laboratory	Laboratory Qualifier Description
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	PERCENT
·	Less Than
= = = = = = = = = = = = = = = = = = = =	Equal to
>	Greater Than
CE	Co-elution
EV	Estimated Value Above Detection Limit
<u>-</u>	Interference present
IV	Indeterminate - Indicates a significant difference
j	Estimated Value Above Detection Limit
ND	Not Detected
PV	Probable-Denotes similarity between chromatograms
	Indicate the Melanic Data and
<u>S</u>	Indicates the Value is Determined by the Method of
TI	Tentatively Identified Compound
TR	Trace
U	Not Detected
UR	Unresolved Peaks Due to Matrix Interference or Imp
Project	Project Qualifier Description
Qualifier	·
=	Detected
	Estimated
R	Rejected
J ii -	Undetected
	Undetected, Reporting Limit Estimated
Sample Type	
AB	Sample Type Description Ambient conditions blank
BD · -	T
1	Blank spike duplicate
BS	Blank spike
EB	Equipment blank sample
FB	Field blank sample
FD	Field duplicate sample
FR	Field Replicate
FS	Field Spike
KD	Known (External Reference Material) Duplicate
LB	Laboratory method blank
LR	Laboratory replicate
MB MB	Material Blank
MS	Matrix spike
<u> -</u>	Normal environmental sample
NC	Normal, co-located sample
NS	Normal, QC split sample
	Matenal Rinse Blank
RD	Regulatory Duplicate
	Reference material
	Matrix spike duplicate
TB	Travel or tnp blank

Attachment 4 – Detected Groundwater Analytical Results Summary

Qualifier Code ဗြ Units Reporting -88888----888888----8-88888-Detecton 011 011 018 013 Final Qualifier Final Resut 0018 0023 0033 0023 Laboratory Qualifler Laboratory Result 0018 0023 0012 0013 1 2 2-Tetrachloroethane trans-: 2-Dachloroethene trans-1 2-Orchloroethene trans-1 2-Dichloroethene trans-1 2-Dichloroethene cis-1 2-Dichloroethene cis-1 2-Dichloroethene crs-1 2-Drchloroethene crs-* 2-Dichlaroethene Carbon terrachlonde 1 2-Dichlompropane Carbon tetrachlonde 1 2-Dichloropropane Carbon tetrachloride 1 2-Dichloropropene Carbon tetrachlonde Carbon tetrachonde 1 2-5 chloroethane 2-Dichloropropane Chlorobenzene Tetrachloroethene 1 2-Dichloroethane Wethylene chloride Tetrachloroethene 1 2-Dichloroe/hane Methylene chloride Tetrachloroethere 1 2-Dichloroethane Tetrachloroethene 1.2-Dich proethane Methylene chlonde Trich.oroethene Trichlorcethere Inchloroethene Chloromethare Trichloroethene Bromomethane Chloroberzene Chlorobenzene Chloromethane Chloroberzere Ethylbenzene m-p-Xylene m. p. Xy ene Chloroform Chroraform Chloroform H- p-Xylene Chloroform Parameter o Xylene Benzene Analytical Method SW82608 SW82608 SW82608 SW82608 SW82608 SW8260B SW8260B SW8260B SW8260B SW8260B SW82603 SW82609 SW82609 SW82608 SW82609 SW8260B SW826CB SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B SW82609 SW8260B SW82609 SW8260B SW8260B SW8260B SW8260B Sw82608 SW82609 SW8260B SW82609 SW8260B SW82609 SW8260B SW8260B 11/30/01 11 nn 11/30/01 11 nn 11/30/01 11 nn 11/30/01 1: nn 11/30/01 1: nn 11/30/07 1: nn 11/30/07 1: nn Sample Date 11/30/0: *1 nn 11/30/01 :1 nn Ę ٤ ۶ Ę 11/36/01 *1 nn 11/30/01 11 nn 11/30/01 11 nn 11/30/01 11 nn 11/30/01 11 nn 11/30/01 11 nn 11/30/01 11 nn 11/30/01 11 nn 11/30/01 11 rn 11/30/01 11 p.n 11/30/01 11 rn 11/30/01 11 rm 11/30/01 11 rm ٤ 11/30/01 11 nn 11/30/01 11 nr 11/30/01 1: nn 11/30/01:1 nn 11/30/01 11 nn 11/30/01 11 nn 11/30/01 *1 nn 11/30/0* *1 nn 11/30/01 *1 nn 11/35/01 *1 nn 11/35/01 *1 nn 1,30/01 11 nn 1730/0° 11 nn 1730/01 11 nn 11/30/01 11 nn 11/30/01 11 nn 11/30/01 11 nn 11/30/01 11 nn 11/30/01 11.nn 11/3C/01 11 nn 11/3C/01 11 nn 1/30/01 11 nn 11/20/01 11 11/30/01 11 :1/30/01 11 11/30/01:11 11/30/01 11 MW-85-2DL MW-85-2DL MW 85-3 MW-85-3DL MW-85-3DL MW-85-3DL MW-85-3DL MW-85-4 MW-85-40L NW-85-5 WW-85-2DL MW-85-2DL MW-85-3 MW 85-3 MW-85-3 Semple ID MW-85-1 MW-85-1 MW-85-1D! MW-85-102 MW-85-1DL MW-85-1DL WW-85-2DL MW-85-30L MW-85-40L MW-85-40L MW-85-40L MW-85-40-WW-85-5DL MW 85-4 MW-85-4 VW 85-4 MW-85-3 N-W-85-2 WW-85-2 MW-85-2 MW-85-2 MW-85-2 MW-85-2 MW-85-2 MW-85-2 MW-85-2 MW-85-2 MW-85-3 WW-85-4 VW-85-5 WW-85-5 Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwa'er Groundwa'er Groundwater Groundwater Groundwater Groundwa'er Groundwa'er Groundwa'er Groundwa'er Groundwater Description Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwate Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater

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Attachment 4

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Ougsifier Code Š Reporting 22222 ----88888 - 88888----88888----888888 Detection 0.15 Ocalifie Final Final Result Leboratory Oughfier 00000 # Laboratory trans-1 2-Dichlorcethens trans-1 2-Dichioroethene trans-1 2-Dichloroethere trans-1 2-Dichloroethers trans-1 2-Dichloroethene as-12 Dichloroathene cis-1 2-Dichloroethene CS 12-Dichloroethene as-1 2-Dichloroethere cus-1 2-Dichloroethene as-1 2-Dichloroe/hene Carbon tetrachlonde 1.2 Dichloropropane Carbon tetrachlonde 1 2-Dichloropropane Carbon tetrachlonde 1 2-Dichloropropane Carbon tetrachloride 1 2-Dichloropropane Carbon tetrachlonde Carbon tetrachloride 1.2 Dichloropropane * 2 Dichloroethane 1 2-Dichloroemane Tetrachloroethene Tetrachlorcemene 1 2-Dichloroethane Tetrachloroethene Tetrachloroethene 1 2-Dichloroethane Tetrachloroethene 2-Dichloroethane Vethytene choride frich'aroathere Chlorobenzene Trichloroethene Chlorobenzere Trichloroethene Chloroberzene Trichloroethane Inchloroethene Trichloroethene Ethylbenzene Chloroform Chloroform Choro'orm m. p.Xylene Chloroform Chloraform Chloroform o-Xylere Toluene Aralytical Method SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B SW82608 SW8260B SW6260B SW6260B SW8260B SW8260B SW6260B Sw82603 SW-826CB SW826CB SW8260B SW8260B SW8250B SW82608 SW8260B SW82508 SW826CB SW8260B 11/30/01 10 nn 11/30/01 10 nn 11/30/01 10 nn 11/30/01 10 nn 11/30/01 10 nn 21/30/01 10 10 11/30/01 10 hr nr 01 10/05/11 11730/01 10 nn 11/30/01 10 nn 11/30/01 10 mm 11/30/01 10 rn 1/30/01 10 nn 1/30/0° 10 nn 11/30/0° 10 nn nn 0: 10/05/11 nn 01 10/05/11 11/30/01 10 nn 11/30/01 10 nn 11/30/01 10 rn 11/30/0' 10 rn 11/30/01 10 nm 11/30/01 10 nm 11/30/01 10 nn 11/30/01 10 rm 11/30/01 10 cm 11/20/01 10 rn 11/30/01 10 nn 11/30/01 10 nn 11/30/01 10 nn 1/30/01 10 nn 1/30/01 10 nn 11/30/01 10 nn 11/30/01 10 nn 11/30/01 10 nn 11/3C/01 10 nm nr 01 1005/11 11/30/01 10 nn 11/30/01 10 nm 11/30/01 10 nm 11/30/01 10 nm 11/30/01 10 nm nn 01 10/05/11 1730/01 10 rn 11/30/0° 10 rn 11/30/0° 10 rn 11/30/0° 10 rn 11/30/01 10 rn 11/30/01 10 nn Sample Date 11/30/01 10 01 11/30/01 10 nn WW-86-5DL WW-86-5DL WW-86-5DL WW-86-5DL WW-86-5DL WW-86-5DL MW-86-4D. MW-86-4DL MW-86-60L WW-86-60L WW-86-60L WW-86-60L WW-86-60L MW-86-7Dt. MW-86-7DL WW-86-80L WW-86-80L MW-86-70L MW-86-70L MW-86-4DL MW-86-4DL MW-86-4DL Sample ID MW-86-7DL MW 86-8DL MW-86-BDL MW 86-5 MW-86 S MW-86-5 MW-86 5 WW-86-6 MW-86-6 MW-86-6 MW-86-8 MW-86-8 MW-869 MW-86-7 MW-86-7 MW-86-7 WW-86-7 WW-86-8 MW-86-9 Groundwater Groundwater Groundwater Groundwater Groundwater Groundwaler Groundwater Groundwaler Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater G'oundwater G:oundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater. Groundwater Groundwater Groundwater Description Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater

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Tetrachicrethene
Tolliene
Trichloroethene
Carbon tetrachlorde
Chloroform Choroform cs-1 2-D choroethere cts-1 2-Dichloroethene cs-1 2-Dichloroethens as-1 2-Dichloroethens Ethylbenzene Tetrachloroethene Totuene Carbon tetrachlonde Carbon tetrachlonde m- p-Xylene Tetrachloroethene Trichloroethene Carbon tetrach onde Carbor te'rachtoride Tetrachloroethene o-Xyane Tetrachloroethene *etrachloroethene etrachloroethen Trichoroathene Trichtoroathere Trichloroethere Ethylberzene m. p.Xylene Enybenzene Ethylbenzene m. L.Xylene Chloroform m- p-Xylene Chloreform Chloroform Toluene Toluene o-Xylene Toluene Paramete Analytical Method SW8260B SW8260B SW826CB SW8260B SW8260B SW82608 SW8260 SW82608 SW82608 SW82608 SW82608 SW82608 SW82608 SW82608 SW82608 SW82608 SW82608 SW82608 SW82608 SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B SW8260B 3W8260B 11/30/01 09 nn 11/30/01 09 nr 11/30/01 09 nr 1130/01 09 nn 1130/01 09 nn 1130/01 09 nn 1130/01 09 nn 1130/01 09 nn 1130/01 09 nn 1130/01 09 nn 1130/01 09 nn 1130/01 09 nn 1130/01 09 nn 11/30/01 (59 rm 11/30/01 09 rm 11/30/01 09 rm 11/30/01 09 rm 11/30/01 09 rm 11/30/01 09 rm 11/30/01 09 rm 11/30/01 09 rm 11/30/01 09 rm 11/30/01 09 rm nn 60 10/06/11 nn 60 10/06/11 nn 60 10/06/11 nn 60 10/06/11 nn 60 10/06/11 nn 60 10/06/11 7.730/01 C9 rn 11/30/01 09 rn 11/30/01 09 rn 11/30/01 09 nm 11/30/01 09 nm 11/30/0* 09 nm 11/30/01 09 rn ٤ ٤ 11/30/01 09 rn 11/30/01 G9 nm 17/30/01 C9 nm 11/30/01 C9 rn Sample Date 11/30/01 09 n Sample 10 VW 88-5 MW-88-6 MW-88-6 MW-88-6 MW-88-8 MW-88-6 MW-88-6 Groundwater Groundwate Groundwater Groundwater Groundwate Groundwate Groundwate Groundwate Groundwater Groundwate Groundwater Groundwate Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater oundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater

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Attachment 4
Detected Groundwater Analytical Results Summary
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Qualifier Code ខ ဗ္ပ ខ ႘ ខ្លួ ន 8888 ပ ပ္ ក $^{\circ}$ $\bar{\Omega}$ ç កកកក \mathbf{c} Unds ত্ত্বলিক ক্ষেত্ৰৰ প্ৰত্নি কৰিছে বিষয়ে প্ৰতিপ্ৰতি কৰেছে বিষয়ে প্ৰতিপ্ৰতি কৰিছে বিষয়ে স্থা কৰিছে বিষয়ে স্বিত কৰিছে বিষয়ে স্বিত কৰিছে বিষয়ে স্বিত কৰিছে বিষয়ে স্বিত কৰিছে বিষয়ে স্বিত কৰিছে বিষয়ে স Reporting Detector 0 12 0 12 0 14 0 15 0 13 Qualifie Final Result 12 056 056 1900 017 56 56 053 003 100 003 1300 003 1300 1300 003 1300 1000 1 840 46 031 013 014 018 Laboratory -aboratory Chloromethane Ethytbenzene m- p-Xylene Methylene chloride Ethy-benzere m. p-Xy-ene Methylene chlonde o-Xylene Chloroform
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Datected Groundwater Analytical Results Summary Mempits Depot Vair Inselation LTOA Technical Memorandum

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Description	Chemica: Group	Sample ID	Sample Da'e	Analytical Method	Parameter	5	Laboratory	Final Result	Final	۶	Reporting	Chits	Qualifier Code
Groundwater	VOC	MW-103-5	12/11/01 C8 nn	SW826CB	ds-12-Dichomethene	A PROJE		-	Qualmer	ž S	<u>E</u> ,		İ
Groundwater	voc	MW-100-5	12/11/01 08 rm	SW8260B	trans-1 2-Dichloroethene	. St 2	. ¬	. o	• -	2 :	- •	<u>ğ</u> §	
Groundwater	200	MW-100-5DL	12/11/01 08 nn	SW82608	Tetrachiproethene	65		99		-	- =	3 2	
Groundwater	200	MW-100-5D:	12/11/01 08 nn	SW8260B	Trichloroethene	97	٥	. 6	•	. 5	2 9	3 3	_
Groundwater	200	MW-00-6	12/11/01 08 nn	SW8260B	1.1.2.2-Tetrachloroethere	0 12	- -	0.5	7	80	· -	ğ	
Groundwater	2 5	9-00-MM	12/11/01 08 rn	SW8260B	1 2-Orchloroethane	110	,	;	7	110	-	J.	
Grandwater and	2 5		12/11/01 US FM	SW8260B	CIS+1 2-DicPloy0ethene	12	•	12		0 ,5	-	ฐ	
Groundwater	200	MW-100-6Dt	12/11/01 08 mm	SWOZOUB	rars-1 Z-Dichlorethane	G 15	¬ (0.15	7	:	-	JS N	
Groundwater	200	MW-103-8D.	12/1:/01 08 00	SW8260B	Trafficantina	. i	ه د	5 1	•	12	2	호 호	
Groundwater	200	MW-100-7	12/11/01 08 nn	SW4260B	TO STORESPORT	0	o ·	5 3	•	£ .	2	를	
Groundwater	200	KW.100-7	12/11/03/08/09	SINGSOND	1 . C. Leurachtoroemane	er 0	- -	0.5	-	800	-	Z Z	
Groundwater	8	MW-100-7	.2/1./01 08 nn	SWRZEOB	1 2. Octal contracts	0.0	, . _	20	, .	- :	-	 100	
Groundwater	000	MW-100-7	12/11/01 08 nn	SW8760B	result 3. Displayments	٠		, م	,	110	-	ฐ	
Groundwater	0 0 0	MW-100-7	.2/11/C108 nn	SW8260B	trans-1 2-Directors	31.0	- -	7 .		0 12		<u></u>	
Groundwater	, V	MW-100 7DL	12/1 //01 08 nn	SW8250B	Tetachlonetheon	2 4	· c	٠,	· ·	5 :	- ;	3	
Groundwater	8	MW-100-7DL	12/1 701 08 nn	SW8260B	Trathonthera	3 8	3 6	8 8	•	7 .	2 9	3	
Groundwater	202	MW-100-8	.2/1:/01 08 nn	SW8260B	1 1 2 2 Tetrachlomethane	, ;	- -	, ;		ۍ . د و	<u> </u>	ر ا	
Groundwater	X	WW-100-8	12/11/01 08 nn	SW8250B	1 *-Dichloroethene	2.5	, -	670	, -	500	- ,	g :	
Groundwater	8	MW-100-8	12/11/01 08 nn	SW8250B	1 2-Dichlocosthane	- 22	, -	7:	, -	: ;	- •	5	
Groundwater	000	MW-100-8	12/1-/01 08 nn	SW8260B	28-1 2-Dichloroetheos		, ,	· ·	, i	- :	- •	5 6	
Groundwater	00 V	MW-105-8	12/11/01 08 nn	Sw8260B	trans-1 2-Dichloroethene		-	· ;	, -	7:	- •	5 5	
Groundwater	8	MW-100-8DL	12/11/01 08 nn	SW8260B	Tetrachloroethene	ù	, ,	? *	וי		- ;	3 6	
Groundwater	00 V	MW-100-8DL	12/11/01 08 nn	SW8260B	Trichloraethene	26	0 0	6		7 -	2 5	3 5	
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Groundwater	00 00	WW-100-9	.2/1°/01 08 nn	SW8260B	1 *-Dichloroethene	0 18	_		, ¬	3 5	- •-	<u> </u>	
G'oundwater	VOC	WW-100-9	-2/1 /C1 08 nn	SW8260B	1 2-Dichloroethane	0 14	, ,	4.0	, 7		- •	3 5	_
Groundwater	00×	WW-100-9	12/11/01 08 nn	SW8260B	cis-1 2-Dichloraethene	12	•	12	•	0 12	-	3 5	
Groundwater	200	MW-100-9	.2.1.10108 nn	SW8260B	rans-1 2-Dichloroethere	0 17	¬	4.0	,		-	l So	
Groundwa'e'	200	MW-100-9DL	12/11/01 08 nn	SW8260B	Tetrachoroethene	63	٥	63		12	2	S S	
Groundwater	200	MW-100-90t	12/1*/01 08 nn	SW8260B	Trichloroethene	86	۵	86	•	13	2	NS.	
Groundware.	200	WW-101-109	12/21/01 15 nn	SW8260B	as-1 2-Dichloroethene	0.27	7	0.27	7	0 12	-	UG/L	
Groundwater	200	MW-101-109	12/2*/01 15 nn	SW8260B	Trichloroethene	0.87	¬	0.87	7	0 13	-	UGIL	
) () ()	MW-101-090L	12/2/1/01 15 nn	SW8260B	Tetrachloroethene	3	٥	85		40	Ç	정	
Groundwater	200	MW-101-122	12/21/01 15 an	21002000	Choraiom	0 42		0.42	7	0 12	-	ಸ ಶ	
Groundwater	200	MW-101-124	12/21/01/15 20	2007000	CIS-1 2-UCHIONOMINGNB	0.39	 	0.39	-	0 12	-	ಕ್ಷ	
Groundwater	000	MW-101-124DL	12/21/01 15 m	SWAZECB	Terrandometra	4 6	٠ ،	1 5	· •	0 13	. :	න් <u>දි</u>	
Groundwater	00A	MW-101-89	12/21/01 16 rn	SW8260B	Chloroform	3 %	-	3 6	, -	a ;	ş.) 	
Groundwater	0 V	MW-101-89	12/21/01 16 r.n	SW8260B	ds-1 2-Okchloroethene	75	, -	3 2	· -	3 5	- -	5 5	
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Groundwater	00 00	MW-101-89DL	12/21/01 18 r.n	SW82608	Tetrachloroethene	530	۵	530	- · ·	, 4 ; 40	. Q	- 5 5	
Groundwater	8	MW-102-1	12/11/01 08 rm	SW8260B	1.1.2,2-Tetrachloroethane	0.23	,	0 23	7	600	٠-	전	
Groundwater	0 9	MW-102-1	12/*1/01 08 nm	SW8260B	Carbon disulfide	0 33	¬	0 33	·	41.0	-	ğ	
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Croundwater	2 <u>9</u>	MW-102-2	12/11/01 08 nn	SW8260B	1 2 2-Tetrachloroethene	0 44	7	2	7	60 0	-	J.S.	
Groundwater	8 8	WW-102-2	12/11/01 08 nr	SW8260B	Carbon distrifide	0.28	<u> </u>	0 28	7	4.0	-	정	
Groundwater	8 8	WW-102-2	12/11/01 08 nn	SW8260B	Trichlorethene	0 33	,	0 33	7	0 13	-	J S	
Groundwater	35	WW-102-3	12/11/0' 08 nn	SW8260B	1 1 2 2-Tetrachloroethane	0.35	_	0.35	_	600	-	พูก	
Sround water	3 5	WW-102-3	00.00.1021	SW8ZEOB	Carbon distufide	021	¬	021	, ,	<u>*</u>	-	Jon Nor	
Groundwater) }	WW-102-5	12/1:M: 08 nn	SW6260B	Inchiprogramene	0.25	٦.	0.25	ر	0 13	-	รู	
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SW8260B SW8260B SW8260B SW8260B SW82608 SW82608 SW82608 SW82608 3W8260B SW8260B 1730/01 13 nn 1730/01 13 nn 1730/01 13 nn 11/30/01 13 nn 11/30/01 13 nn 11/30/01 13 nn 11/30/01 13 nn 11/30/01 13 nn 11/30/01 13 nm 1130/01 13 nn 11/30/01 13 nn 11/30/0° 13 nn 11/30/01 13 nn 11/30/01 13 nn 11/30/0° 13 nn 11/30/01 13 nn 11/30/01 13 nn 11/30/01 13 nm 11/30/01 13 nn 11/30/01 13 nn 11/30/0* 13 nn 11/30/01 13 nn 11/30/01 13 nn 11/30/01 13 nn Sample Date 11/30/01 13 rn 11/30/01 13 nn 11/30/01 13 nn 1/30/01 13 nn 11/30/01 13 nn 11/30/01 13 nn 1*,30xC1 13 nn 11/30/01 13 r.n 11/30/0" 13 nn 11/30/01 13 nn 11/30/01 13 nn 11/30/01 13 nn 11/30/01 13 nn 11/30/01 13 nm 11/30/01 13 rn 11/30/01 13 nn 11/30/01 13 nn 11/30/01 13 nn 11/30/01 13 nn 11/30/01 13 rr 1*/30/01 13 nn MW-103-10 MW-103-10 MW-103-10 MW-103-2 MW-103-2 MW-103-2 Avv. 103 1 MW-103-1 MW-103-1 MW-103-1 MW-03-1 MW 103-2 VW-103-3 MW 103-3 MW-103-3 Sample 1D MW-103-10 MW-103-10 MW-103-5 MW-103 5 MW-103-5 MW-103-5 WW-103-6 WW-103-6 MW-103-7 MW-103-7 MW-103-3 MW-103-3 MW-103-3 VW-103-3 WW-103 3 WW-1034 MW-103-4 MW-103-4 MW- 034 MW-103-4 WW-103-4 WW-103-5 WW-103-5 WW-103-5 VW-103-5 AW-103-6 9-60. WW Groundwater Groundwater Groundwater Groundwa'er Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Description Groundwater Groundwater Groundwa'er Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwater Groundwa'er Groundwa'er Groundwate² Groundwate*

Attachment 4 Detected Groundweter Analytical Results Summery Merons Datet Man kateleton LTOA Technisk Memoranum

Description	Chemical Group	Sample ID	Sample Date	Analyteal Method	Регателет	Laboratory	Laboratory	Final Result	Final	Detection Reporting	Reporting	ş	Qualifier Code
Groundwate ^r	200	MW 103-7	11/30/01/13 FP	SW8260B	1 1 Dichloroethene	7.		4.		0.23		J/S/	
Groundwater	8	₩-103-7	11/30/0° 13 nn	SW8260B	1 2-Dichloroethane	81.0	_	8.0	7	10	-	5	
Groundwater	8	VW-103-7	11/30/01 13 nn	SW8260B	Chloreform	17		٠.	• •	41.0		100	
Groundwater	8	WW-103-7	11/30/01 13 nn	SW8260B	cis-* 2-Dichloroethene	039	7	0 39	7	0 12	-	180	
Groundwaler	000	MW- 03-7	11/30/01 13 nn	SW8260B	Trichtoroethene	6 7		9	•	0.12	_	50	
Groundwater	200	MW-103-8	11/30/01 13 nn	SW8260B	1 1-Dichloroethane	17	•	17	Ħ	4.0	_	9	
Groundwater	200	MW-103 8	11/30/01 13 nn	SW8260B	1 1-Dichloroethene	12	•	12	•	0 23	-	200	
Groundwater	200	MW-103-8	11/30/01 13 nn	SW8260B	1.2-Dichloroethane	8:0	<u> </u>	0 18	7	-	-	3	
Groundwater	200	MW-103-8	11/30/01 13.nn	SW8260B	Chloroform	ě		16	•	0 14	-	절	
Groundwater	8	MW-103-8	11/30/01 13 nm	SW8260B	ds-1 2-Dichloroethene	0 36	¬	0.36	¬	0 12	-	50	
Groundwater	800	MW-103-8	11/30/01 13 pm	SW8260B	Trichloroalhana	6 7		6	•	0 12	-	8	
Groundwater	8	MW-103-9	11/30/01 13 nm	SW6260B	1 1-Dichloroethane	1.5	a	w)		41.0	_	S	
Groundwater	8	MW-103-9	11/30/01 13 nm	SW8260B	1 1-Dichloroethens	-	•	;=		0.23	-	1 2	-
Groundwater	8	MW-103-9	11/30/01 13 nn	SW8260B	1 2-Dichloroethane	0 .5	7	0.15	, _			2	
Groundwater	200	WW-:03-9	11/30/01 13 nn	SW8260B	Chloroform	17	. *	12		10	_	ž	•
Groundwater	200	MW-103-9	11/30/01 13 nn	SW8260B	cis-1 2-Dichloroethene	0 37	,	0 37	7	0 12		5	
Groundwa'er	200	MW-103-9	*1/30/01 13 nn	SW8260B	m. p-Xylene	0.27	ר	0 27	_	0 23	7	l de	
Groundwater	200	MW-103-9	*1/30/01 13 nn	SW8260B	Trchloroethere	56	•	5.6	•	0 12	-	2	
Groundwater	8	MW-104-1	11/30/01 14 nn	SW8260B	1 1-Dichloroethane	0 16	7	91.0	7	0 14	-	J.S	
Groundwater	8	MW-104-1	11/30/01 14 F1	SW626CB	Acetone	- 4	*		7	. .	'n	ğ	ე ე
Groundwater	8	WW-104 ·	1./30/0. 14 rn	SW8260B	Carbon disulfide	- 33	•	€,	•	0 22	•	UGIL	
Groundwater	Š	WW-104.	11/30/01 14 nn	SW8260B	Chhroform	•	•	4	•	*	-	1.GJ	
Groundwater	န ှ	VW-:04-1	11/3C/0* 14 nr	SW8260B	Ethylbenzene	C 61	7	061	7	0 12	-	UG/L	
Groundwater	٥ ٥	MW04-1	11/3C/01 14 nn	SW8260B	m. p-Xylene	18	7	80	7	0 23	~	ر ال	
Groundwater	00×	MW-104-1	*1/30/01 14 nn	SW6260B	o-Xyæne	0.57	7	0.57	¬	0 13	-	J/S/n	
Groundwater	ပ (MW-104-1	-1/35/01 14 nn	SW8260B	Toluene	045	7	0.45	¬	0.11	-	200	
Groundwa'er) VO	MW-104-1	11/30/01 14 nn	SW-8260B	Trichloroethere	0.89	¬	680	7	0.12	-	J.S	
Groundwater	8	MW-104-10	11/30/01 14 nn	SW8260B	1,1-Dichloroethane	0 54	7	\$	¬	0 12	-	ฐ	
Groundwater	8	MW-104-10	11/30/01 14 nn	SW8280B	1 1-Dichiproethene		n	e.	•	5	-	ng Ng	
Groundwa:br	8	MW-104-10	11/30/01 14 m	SW82608	Chloreform	50	•	8	•	0 12	-	કુ	•
Groundwater	ο <u>(</u>	MW-104-10	11/30/01 14 mm	SW82608	ds-1 2-Dichloroethene	0.46	7	0.46	-	0 12	-	ษั	
Groundwater	2 5	MW-104-100L	1./30/01 14 nm	SW82608	Trichloroethene	54	٥	24	•	0 26	7	ಕ್ಷ 2	
Groundwater	88	WW-104-2	1 730/01 14 nm	SW8260B	Acetone	95 .	*	9 .	ר	. ;	ro.	તું .	ပ္ပ
Goordwaler	3 6	7-901-A44	nn 41 10/06/11	SW8Z6UB	Carbon disuitida		•	٠,	u	•	_	5	
Goundwater	3 5	7-01-704	11/30/01 14 nn	SW8250B	Chororom	3 4 6	•	φ φ	•	0 12		5 5	
Promption of		100,101	11,30,011	0000000	BH92mpGm2	600	,	600	י ר	: 6		3 5	
Spending and		MW-104-2	11/2001 14 00	SW8260B		77		77		2 6	, .	3 5	
Groundwa'er	000	MW-104-2	11/30/01 14 nn	SW826GB	occupation of the contract of	9	, -	- 0	, -	3 5		3 2	
Groundwa'er	202	MW-134 2	11/30/01 '4 nn	SW8260B	Trichlorathere	-		3 :-	,,,	, 0		3	
Groundwater	٥ ٥	WW-104-3	1*/30/01 *4 rm	SW8260B	1 1-Dichloroethane	0 16	-	0.16	7	0 12	-	ď	
Groundwater	8	WW-104-3	11/30/0° 14 nr	SW8260B	Ace'one	•		4	· ¬	=	2	Jon Jon	20 00
Groundwater	200	MW- 04-3	11/30/01 14 nr	SW8260B	Carbon disu'fida	- -	•	1.5	•	•	•-	7SU	
Groundwater	000	MW-104-3	11/30/01 14 nn	SW8260B	Chloroform	*	•	44 80	•	0 12	-	ng/r	
Groundwater	ပ လ	MW-104-3	11/30/01 14 nn	SW8260B	Ethylbenzere	0 73	7	073	,	5	-	J S	
Groundwater	8	MW-104-3	11/30/01 14 nn	SW8260B	m- p-Xylere	24	•	54	*	20	~	ત્રું N	
Groundwater	0	MW-104-3	11/30/01 "4 mm	SW42608	O-Xylene	0 74	7	0.74	¬	0	-	J O C J	
Groundwater	န္	WW-104-3	11/30/01 14 nm	SW8280B	Trichloroethene	- !	•	- '		0 13	-	નું (
Groundwater	၌ နို	MW-104-4	11/30/01 14 nm	SW82808	1 1-Dichloroethane	0.16		0 16	-	0 12		ප් දි දි	
Sroundwater)))	MW-104-4	11/30/01 14 nr	BUSTANS	Carbon desurida	<u>.</u>		<u>,</u>		4 6		3 5	
Groundwater	3 S	MW-104-4	11/30/01 14 nn	SW8260B	Fibylbanzana	۰ ۲	-	v ,	<u></u>	0 12		<u> </u>	•
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Attachment 4
Detacted Groundwater Analytical Results Summary
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Qualifier Code						ပ္ပ											ပ္ပ																			-						<u>ပ</u> ပ									
SE SE	ള	Z Non	절 S	ই	ঠু	<u>§</u>	ই	절	ž	절	ନ୍ଧ	ই	УSV	ន្ត	ខ្ម	년 5	તું 5	헣	정 2	전 전	200	ъ́	절	S S	JSJ.	ฐ	UGI	ИSV	র S	NG/I	ig N	정	ğ	UG/L	Z Z	7	ğ	<u></u>	절 -	ថ្ម	3	g :	3	න් :	5 :	3 8	3 5	3 5	3 5	3 3	<u> </u>
Reporting	~	-	-	-	-	٠C	-	-	-	-	~	-	-	-	-	-	'n	-	-	-	2	-	-	-	-	-	-	-	-	7	_	-	-	-	-	-	•	~	-	-	- 1	ი •			- •	- •	- •	- •	- •		• -
Detection Reporting	0.2		0 13	0 12	5	=	2 0	0 12	0 12		0.5	90	5	0 13	0 12		-	0 12	0 12	110	0.5	90 0	5	0 13	0 12		0 12	0 12	-	0 2	0 13	0 12	011	0 18	0 12	0 12		0 2	n :	2:0	5 ;	. ;	710	21.0	610	5 6	2 0	2 0	2 5	? -	0 12
Final		״		7	7	7	7	•	7	7	7	7	7	•	7	•	7	•	7	7	7	7	7		7			7	7	7	и	7		•	ĮI	7	7	 -		-	•	- ·	, .	-		, -	, -	, -	7 6	, -	, ¬
Firal Result	22	990	13	0 37	0.48	31	760	ō	0 22	0.55	16	0.21	0 44	4.0	0 55	=	22	-11	40	0.36	13	0 12	03	16	0.65	14	\$0	0.47	910	0 39	5	0 49	12	1.5	4	0.36	.	0 48	<u> </u>	χ, ο '	÷ (7 9	2 4	2.5	₹ 5	7 2 0	2 2	2 6	. e.		0 16
Laboratory	•	7		7	7	7	7		7	7	7	7	7	•	7		- -	•		7	7	٦	7	ų	7		•	7	<u> </u>	7		7		•	н	7	7	¬		7 :		, i	, -	,		, -	, -	, -	, .		, ,
Laboratory	22	0 68	13	0 37	0 48	3.1	0.84	•	0 22	0.55	9	021	0 44	6.4	0.55	=	22		0	0 36	13	0 12	03	16	0 65	4	18	0.47	0 14	0 39	19	0 49	12	1.5	7	0 36	0 16	0 8	, (8.	უ (- (7 9	,	<u></u> 8	3 5	25.0		9 0			0 16
Parameter	m- p-Xylere	o-Xylene	Trichloroethene	1 '-Dichloroethane	1 *-Okthoroethene	Acetone	Carbon disurade	Chloroform	cis-1 2-Dichloroethere	Ethylbenzene	m- p-Xylere	Methylene chloride	O-Xylene	Trichlaroethene	1 1-Dichloroethane	1 1-Dich-proethers	Acatone	Chloroform	cis-1.2 Dichlorcethene	Ethylbenzene	m- p-Xyfane	Vethylene chloride	0-Xylene	Trichloroethere	1 1-Dichloroethane	1 1-Dichlaroethere	Chloro*orm	ds-1 2-Decharcethene	Ethybenzere	m- p-Xylane	Trichloroethene	1 1-Dichloroethans	1 1-Dichloroethere	Bromomethane	Chloreform	cis-1.2 Dichloroethere	Ethylbenzere	m- p-Xylare	nondroene	-Canacaman	-Changoomers	Acetorie		Tackless and Tackless	Branch Cetter C	Carlotte and Carlotte	Circulation of the contract	Tetrachicostheos	Tochlocoathera	Carbon teltachingde	Chloroform
Aralytical Method	SW8260B	SW82608	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW82608	SW826CB	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW\$260B	SW8260B	SW8260B	SW8260B	SW826CB	SW8Z6CB	SW8260B	SWGZBWS	2W6260B	24402600	SW8260B	24,0700	9005045	20028VS	SWBORDE	SWAZEOR	SWRZEOB	SW8260B	SW82808	SW8260B
Sample Date	11:30:01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 mn	11/30/01 14 nn	11/30/01 14 nn	11/3C/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	1*/30/31 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nm	11/30/01 14 nm	11/30/01 14 nn	11/30/01 14 m	11/30/01 14 nm	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nm	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	11/30/01 14 nn	A1730/01 14 no	11/30/01 14 nn	11/30/01 14 nn	1,000,11	11/30/01 14 00	2000	117000111	12/21/01 11 00	12/21/01 11 00	12/21/01 11 00	12/21/01 11 00	12/21/01 11 nn	12/21/01 12 nn	12/21/01 12 nn
2.	1	7	1	5.	9	ě	ς	ň	ě	č.	č.	š		ς.	φ	φ.	φ	9	٩	ኇ	æ	ģ	Ģ	φ	٠,	<u>~_</u>	٠.	۲.	^	۲.	۲.	ep	œ, ·	ę,		φ,	<u>ب</u>		o c						25.0	3 %	3 %	9 5	258	147	147

Attachment 4 Defected Groundwater Analytical Results Summary Mempis Depte Nen Inselevon LTOA Tectical Hemosingum

Description	Chemical	Sample ID	Sample Date	Analytical Method	Рагатете	Laboratory	Laboratory Laboratory	Firal Result	Firal	Detection Benedical	Pennsy		Charlet Cash
	Group					Result	Qualifier		S. Inc.			Š	BOS 161 1805
Ground-water	8	WW-107-147	12/21/01 12 pm	SW8260B	Oc.1 2.Dichlomethene	200	 -	5	5	11111			
,						6.4	•	670	,	200	_	5	
Frouncies et	3	WW-107-147	12/21/01 12 nn	SW6260B	Tetrachloroethene	0 67	,	0.67	_		-	Č	
Groundwater	ş	WW-107-47	12/21/01 12 nn	SW8260B	Trichloroethene	2.8		7.6			- ,	9 5	
Groundwater	Š	MW.108	1201011000			2 2		?;		2	_	900	
)	2		,		- P	,	R7.0	-	-	_	500	ü
Groundwater	8	MW-108	12/21/01 10 nn	SW8260B	Chloroform	64		5.4	•	51.0	_	0	}
Groundwater	ş	MW-108	12/21/01 10 nn	SW8260B	cs-1 2-Dichloroethene	81.0	_	, c	-			3	
Grandwater	ξ	1100-100	12271011010				•	2	,	¥	_	7	
500	3	001-8856	UU 01 10/13/21	"	Memylere chlonds	# 60	,	***********	-,	980	-	500	
Groundwater	8	MW-108	12/21/01 10 nn	SW8260B	Tetrachloroethans	5.6		2.6	*	5	-		
Groundwater	8	MW-108	12/21/01 10 nn	SW8260B	Tolugue	0.23	_		_			3 5	
Groundwater	8	MW-108	12/21/01 10 nn		Tdethorograps	7.4		2	, ,	7 .	- ,	ָּהָ בַּי	
Sem-Volatre Organic Compounts	Servic Compositio									210	-	750	
		ı											
Groundwater	SVOC	MW-108	MW-108 12/21/01 10 nn	SW8273	bis(2-Ethythexyl)phthalate	6	 -	σ	-	0.50	۶	5	
									,		?	ָ כֿ	

Labaratara	T
Laboratory	Laboratory Qualifier Description
Qualifier	
%	PERCENT
<	Less Than
=	Equal to
	Greater Than
CE	Co-elution
<u> </u>	
EV	Estimated Value Above Detection Limit
	Interference present
I IV	Indeterminate - Indicates a significant difference
J	Estimated Value Above Detection Limit
ND	Not Detected
PV	Probable-Denotes similarity between chromatograms
s	Indicates the Value is Determined by the Method of
-	
	Tentatively Identified Compound
TR -	Trace
U	Not Detected
ÜR	Unresolved Peaks Due to Matrix Interference or Imp
Project	Project Qualifier Description
Qualifier	·
=	Detected
j	Estimated
R	Rejected
'i	Undetected
- ··· - ŬĴ	
	Undetected, Reporting Limit Estimated
Sample Type	Sample Type Description
_ AB	Ambient conditions blank
BD	Blank spike duplicate
BS	Blank spike
EB	Equipment blank sample
FB	Field blank sample
FD	Field duplicate sample
FR	Field Replicate
FS	Field Spike
KD	
<u>- </u>	Known (External Reference Material) Duplicate
l —	Laboratory method blank
<u>LR</u>	Laboratory replicate
	Material Blank
	Matrix spike
N	Normal environmental sample
	Normal, co-located sample
	Normal, QC split sample
	Material Rinse Blank
	Regulatory Duplicate
· ~~~ · · - · - · · · · · · · · · ·	
	Reference material
	Matrix spike duplicate
ТВ	Travel or tnp blank

Attachment 5 – Detected Quality Assurance/Quality Control Analytical Results Summary

Ovakfier ႘ ပ္ပ Š ភ ន ပ္ပ ပ ပ ပ္ Units <u>इ</u> इ इ इ Reporting Ĕ 8 ~ 0 - 55 -Detection Ē 0 84 2 2 3 2 2 3 0 54 0 0 73 0 0 65 0 12 0 13 11 0 02 08 08 0 10 12 0 13 Qualifier Per Fxna Laboratory Final Result Quairfier 19 0 15 0 15 0 17 0 35 0 13 0 13 0 13 6.4 0.7 2.2 0000077# Laboratory Result 0 16 0 15 2200 0 17 0 35 67 0 13 64 0 7 1 2 - 22 25 -<u>6</u> trans-12-0-chloroethene rans-1 2-Dichloroethene c:s-1 2-Dichtoroethene cis-1 2-Dichloraethene cis-* 2-Dichlaroethere cs-1 2-Dichloroethene Carbon tetrachlonde 1 2-Dichloropropane Carbon tetrachlonde 2-Dichloroethane 12-Dichloropropane Carbon tetrachlonde 1.2.2 Tetrachloroetha 1.2-Orchloroethane etrachloroethene Totuene 2-Dichloroethane Tetrachioroethene Trichloroethene 1 2-Dichloroethane Carbon tetrachionds 1 1-Dichloroethane Tetrachloroethere Ferrachloroethene Methylene chlande Tetrachloroethere Inchloroethene Acetone Tetrachloroethene Chloroberzene Inchioroethene Trachoroethene Chloromethane Trchloroethene Trichloroethere Acetone 2-Butanone Bromoform Ethylbenzene **Ethy'benzene** Chloroform Chloroform Ch oratorm Chloroform m-p-Xy'ene Brompform m- p-Xylene Chloroform Chloro'orm Parameter Acetone o-Xylene Toluene Acetone Sample Date | Analytical Vethod SW8250B
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NW-101-994

NW-104-653

NW-88-786

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Detected QA/QC Analytical Results Summary Memoris Describen Instalation LTCA Technical Memoracian

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Attachment §
Detected OA/OC Analytical Results Summary
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Laboratory	Laboratory Qualifier Description
Qualifier	
%	PERCENT
<	Less Than
=	Equal to
>	Greater Than
CE	Co-etujion
EV	Estimated Value Above Detection Limit
1 1	Interference present
l iv	Indeterminate - Indicates a significant difference
l ;	Estimated Value Above Detection Limit
ND	Not Detected
PV	Probable-Denotes similarity between chromatograms
s	Indicates the Value is Determined by the Method of
Ťi	Tentatively Identified Compound
TR	Trace
ΰ	Not Detected
UR	Unresolved Peaks Due to Matrix Interference or Imp
	
Project Qualifier	Project Qualifier Description
Qualifier	Detected
1	
1	Estimated The analyte was present, but the reported value may not be accurate or precise
R	Rejected The data are unusable (NOTE Analyte/compound may or may not be present.)
U	Undetected Analyte was analyzed for but not detected above the method detection limit
UJ	Detection limit estimated. Analyte was analyzed for and qualified as not detected. The result is estimated.
Sample Type	Sample Type and Qualifier Code Description
and Qualifier	
Code	
2S	Second Source
AB	Ambient conditions blank
BD	Blank spike duplicate
BL	Blank
BS	Blank spike
CC	Continuing Calibration Ventication
DL	Dilution
	Equipment blank sample
	Field blank sample
FD	Field duplicate sample
	Field Replicate
FS	Field Spike
	Holding Time
iC	Initial Calibration
IS	Internal Standard
	Known (External Reference Material) Duplicate
LB	Laboratory method blank
	Lab Duplicate
	Laboratory replicate
: .	Matenal Blank
	MS/MSD or LCS/LCSD Precision
	Matrix spike
N	Normal environmental sample
	Normal, co-located sample
	Normal QC split sample
PD	Pesticide Degradation
PS	Post Spike
RB	Material Rinse Blank
RD	Regulatory Duplicate
	Re-extraction/Re-analysis
	Reference material
	Matrix spike duplicate
	Spiked Surrogate
	Travel or Inp blank
	Tune

Attachment 6 – LTOA Data Quality Evaluation

DDMT Initial Diffusion Bag Data Quality Evaluation (DQE)

ΤO

Steve Offner/ATL

Bryan Burkingstock/ATL

FROM

Kevin A. Sanders/GNA

DATE:

January 21, 2002

The purpose of the data quality evaluation process is to assess the effect of the overall analytical process on the usability of the data. The two major categories of data evaluation are laboratory performance and matrix interferences. Evaluation of laboratory performance is a check for compliance with the method requirements; either the laboratory did, or did not, analyze the samples within the limits of the analytical method. Evaluation of matrix interferences is more subtle and involves the analysis of several areas of results including surrogate spike recoveries, matrix spike recoveries, and duplicate sample results.

Introduction

Samples were collected from September 18, 2001 through December 21, 2001. Field QC samples collected included field duplicates, trip blanks (analyzed for VOCs only), and equipment rinsate blanks. The number of each type of sample is listed by analytical method in Table 1. The samples were analyzed for the following analytical fractions:

- Volatile organic compounds (VOCs) by SW-846 method 8260B
- Total Organic Carbon (TOC) by SW-846 method 9060
- Semivolatile organic compounds (SVOCs) by SW-846 method 8270C

Before the analytical results were released by the laboratory, both the sample and QC data were carefully reviewed to verify sample identity, instrument calibration, detection limits, dilution factors, numerical computations, accuracy of transcriptions, and chemical interpretations. Additionally, the QC data were reduced and the resulting data were reviewed to ascertain whether they were within the laboratory-defined limits for accuracy and precision. Any non-conforming data were discussed in the data package cover letter and case narrative. Attachment G presents a frequency of detection summary for field samples.

The hardcopy data packages were reviewed by the project chemists applying the review process which generally follows that outlined in the Environmental Protection Agency (EPA) guidance document Contract Laboratory Program National Functional Guidelines for Organic (1999) and Inorganic Data Review (1994) [NFG]) Areas of review included (when applicable to the method) holding time compliance, calibration verification, blank results, method accuracy as demonstrated by LCSs, field duplicate results, surrogate recoveries, internal standard performance, and interference checks. A data review worksheet was completed for each of these data packages and any non-conformance documented. This data review and validation process is independent of the laboratory's checks and focuses on the usability of the data to support the project data interpretation and decision-making processes.

1

Data that were not within the acceptance limits were appended with a qualifying flag, which consists of a single or double-letter abbreviation that reflects a problem with the data. Although the qualifying flags originate during the database query process, they are included in the final data summary tables deliverable so that the data will not be used indiscriminately. These also include secondary, or the two-digit "sub-qualifier" flags which are entered into the comments field of the database. The secondary qualifiers provide the reasoning behind the assignment of a specific qualifier to the data. The sub-qualifiers are presented and defined in Table 3. The following primary flags were used in the validation process.

- U Undetected. Analyte was analyzed for but not detected above the method detection limit.
- UJ Detection limit estimated. Analyte was analyzed for, and qualified as not detected. The result is estimated
- J Estimated The analyte was present, but the reported value may not be accurate or precise
- R Rejected The data are unusable (NOTE Analyte/compound may or may not be present)

Numerical sample results that are greater than the method detection limit (MDL) but less than the laboratory reporting limit (RL) are qualified with a "J" for estimated as required by the EPA Functional Guidelines for Evaluating Data Quality

The entire database was queried for frequency of detection in blanks and samples, detailed listing of blank detects, field duplicate precision, method accuracy, surrogate recoveries, preparation and analysis dates pertaining to holding times. The queries were then manipulated to calculate necessary statistics for evaluation of the data.

Once the data review and validation process was completed, the entire data set were reviewed for chemical compound frequencies of detection, dilution factors that might affect data usability, and patterns of target compound distribution. The data set was also evaluated to identify potential data limitations, uncertainties, or both in the analytical results. Attachment A lists the changes in data qualifiers due to the validation processes. Attachment D presents all data which were rejected

Holding Times

The holding times for each parameter were evaluated according to SW-846 requirements. There were no samples flagged for missing established holding times.

Calibration

Initial and continuing calibration data were reviewed for method compliance with relative response factors (RRI), percent relative standard deviation (RSD) and percent difference (%D) criteria. As reflected in Attachment A, 97 records (87 VOC and 10 SVOC) were qualified as estimated (J or UJ) due to established criteria not being met. No data were rejected.

Laboratory Method Accuracy

Laboratory control samples (LCSs) or blank spikes (BSs) are quality control samples utilized to monitor laboratory method performance. This sample does not possess a difficult matrix as it consists of deionized (DI) laboratory water spiked with the target compounds of interest LCS recoveries are presented in Attachment F.

Of the 261 LCS records for individual compounds, a single toluene LCS was outside criteria at 122% with an upper control limit of 119%. As all of the toluene results associated with this LCS were reported as non-detects, no samples were qualified. These data indicate that the laboratory method was in control.

Potential Field Sampling and Laboratory Contamination

Three types of blank samples were used to monitor potential contamination introduced during field sampling, sample handling, shipping activities, as well as sample preparation and analysis in the laboratory

- Trip Blank (TB). A sample of ASIM Type II water that is prepared in the laboratory prior to the sampling event. The water is stored in VOC sample containers and is not opened in the field, and travels back to the laboratory with the other samples for VOC analysis. This blank is used to monitor the potential for sample contamination during the sample container trip. One trip blank should be included in each sample cooler that contained samples for VOC analysis. Fifteen trip blanks were submitted to the laboratory with these samples.
- Equipment Rinsate Blank (ERB). A sample of the target-free water used for the final rinse during the equipment decontamination process. This blank sample is collected by rinsing the sampling equipment after decontamination and is analyzed for the same analytical parameters as the corresponding samples. This blank is used to monitor potential contamination caused by incomplete equipment decontamination. One equipment rinsate blank should be collected per day of sampling, per type of sampling equipment. Nine (VOCs only) equipment rinsate blanks were submitted to the laboratory for this field effort.
- Laboratory Method Blank or Method Blank (MB): A laboratory method blank is ASTM Type II water that is treated as a sample in that it undergoes the same analytical process as the corresponding field samples. Method blanks are used to monitor laboratory performance and contamination introduced during the analytical procedure. One method blank was prepared and analyzed for every twenty samples or per analytical batch, whichever was more frequent.

According to the EPA Functional Guidelines, concentrations of common organic contaminants detected in samples at less than ten times the concentration of the associated blanks can be attributed to field sampling and laboratory contamination rather than environmental contamination from site activities. Common volatile organic contaminants include acetone, methylene chloride, and 2-butanone. For other organic contaminants, five times the concentration detected in the associated blanks (rather than ten times) is used to qualify results as potential field and/or laboratory contamination rather than environmental contamination. This guidance was applied on an SDG by SDG basis and not globally. Global application, however, would account for anomalous data. Detects in the samples at levels less than the action levels (5 or 10 times rule) were qualified as not detected. Attachment A (Change in Qualifiers) lists all changes in qualifier due to data validation and blank contamination (101 total results). A comprehensive list of all detects in each blank is provided in Attachment B. Table 2 compiles the blank detections into a "frequency of detection" by target parameter. Additionally, Attachment F compiles frequency of detection by target analyte for all field samples after validation.

Five volatile compounds were reported in laboratory method or field blanks. These included methylene chloride, chlorobenzene, toluene, bromomethane, and chloromethane. Methylene chloride is used as an extraction solvent and is a common lab contaminant. This compound was found in trip and laboratory blanks. Nine results were qualified for methylene chloride. Toluene is was detected in seven equipment blanks and a single trip blank at sub-part-per-billion levels. Sixteen records at concentrations less than 1 ug/l. were qualified as non-detects due to blank contamination.

Bromomethane and chloromethane are not common contaminants but did appear in laboratory and field blanks at levels similar to those found in field samples. Fifty-one chloromethane and twenty-four bromomethane results were qualified as non-detects due to contamination. I here are 2 bromomethane records remaining as detects in the database, however it is probable that these are also due to contamination. No other volatile samples were qualified due to contamination.

Phthalate compounds are used as plasticizers. The most common phthalates are bis(2-ethylhexyl) phthalate (BEHP) and di-n-butylphthalate. Phthalates are often introduced into samples during handling. Additionally, laboratory chemists use latex or vinyl gloves when handling samples and extracts. Gloves are coated with plasticizers such as BEHP to facilitate release of the gloves from the skin. Diethylphthalate was reported in a single laboratory blank and in a single field sample at roughly the same concentration level. This sample was qualified as a non-detect. While BEHP was not detected in the blanks, 5 soil samples and a single water sample were reported to contain BEHP at levels normally associated with contamination. Thus, BEHP should be considered as a probable contaminant and not indicative of site related activities.

Matrix Effects

Surrogate Spike Recovery

Surrogate spike compounds were added to every sample analyzed for the organic parameters including field and laboratory blanks as well as field environmental samples. Surrogate spikes consist of organic compounds which are similar to the method targets in chemical composition and behavior in the analytical process, but which are not normally found in environmental samples.

Surrogate spike recoveries were used to monitor both laboratory performance and matrix interferences. Surrogate spike recoveries from field and laboratory blanks were used to evaluate laboratory performance because the blanks should represent an "ideal" sample matrix. Surrogate spike recoveries for field samples were used to evaluate the potential for matrix interferences. According to Functional Guidelines, semivolatile data are not qualified with respect to surrogate recoveries unless two or more surrogates are out of specifications. Volatile data are flagged if a single surrogate is out.

All reported surrogate spike recoveries for field and QC samples are presented in Attachment C. As the attachment indicates, surrogate recoveries were well within method acceptance ranges. No samples were qualified as estimated due to surrogates recovering outside criteria

Field Duplicate Sample Results

Field duplicate analyses measure both field and laboratory precision and can also be affected by the homogeneity of the samples. Therefore the results may have more variability than lab duplicates, which measure only lab performance. According to the EPA Functional Guidelines, there are no qualification criteria for field duplicate precision.

There were three sets of water and seven sets of soil field duplicates collected during this field effort. Both the native and duplicate samples were analyzed for the same parameters.

An aqueous control limit of \pm 20% for the RPD was used for original and duplicate sample values greater than or equal to five times the reporting limit (RL). Solid samples utilized a control limit of 35 RPD. A control limit of \pm the RL was used if either the sample for the duplicate value was less than five times the RL for waters and twice the RL for soils. In the cases where only one result is above the five times the RL level and the other is below, the \pm RL criteria were applied. Attachment E includes a summary of the field duplicate measurements and their associated precision statistic.

As the attachment reflects, almost all of the precision data were within the defined control limits. Only 4 records of 234 results were calculated to be outside criteria. These are highlighted in the Attachment. Thus, the precision data indicate that matrix heterogeneity and sampling technique did not greatly influence the final numerical result.

PARCCs

Precision--is defined as the agreement between duplicate results, and was estimated by comparing duplicate matrix spike recoveries and field duplicate sample results. The precision between native and field duplicate sample results were within acceptable criteria indicating that the sample matrix did not significantly interfere with the overall analytical process.

Accuracy--is a measure of the agreement between an experimental determination and the true value of the parameter being measured. For the organic analyses, each of the samples was spiked with a surrogate compound, and for organic and inorganic analyses a MS/ MSD, and LCS were spiked with a known reference material before preparation. Each of these approaches provides a measure of the matrix effects on the analytical accuracy. The LCS results demonstrate accuracy of the method MS/MSD results establish precision and accuracy of the matrix. Spike recoveries were within the method acceptance limits for all of the measurements; therefore, there was no evidence matrix interferences that would affect the usability of the data

Representativeness—this criteria is a qualitative measure of the degree to which sample data accurately and precisely represent a characteristic environmental condition. Representativeness is a subjective parameter and is used to evaluate the efficacy of the sampling plan design Representativeness was demonstrated by providing full descriptions in the project scoping documents of the sampling techniques and the rationale used for selecting sampling locations

Completeness--is defined as the percentage of measurements that are judged to be valid compared to the to total number of measurements made. Other than the results rejected due to dilution or linear range exceedences (there can only be a single valid result per compound, per sample), no other data were rejected. A goal of 90 percent usable data was established in the project scoping document and 100 percent of the data (3215/3215) was determined to be valid.

Comparability--is another qualitative measure designed to express the confidence with which one data set may be compared to another. Factors that affect comparability are sample collection and handling techniques, sample matrix type, and analytical method. Comparability is limited by the other PARCC parameters because data sets can be compared with confidence only when precision and accuracy are known. Data from this investigation are comparable with other data collected at the site because only EPA methods were used to analyze the sample and EPA Level III QC data are available to support the quality of the data.

Summary and Conclusions

Conclusions of the data quality evaluation process include

- The laboratory analyzed the samples according to the EPA methods stated in the work plan as demonstrated by the deliverable summaries and analytical run sequences
- Methylene chloride, chloromethane, bromomethane, and phthalate concentrations should be attributed to laboratory contamination
- Sample results for target organic compounds above the MDL but less than the RL should be considered as uncertain but indicative of the presence of that compound at an estimated concentration

• Surrogates and field duplicate sample results indicate that the specific sample matrix did not significantly interfere with the analytical process or the final numerical result.

The project objectives or PARCCs were met, and the data can be used in the project decision-making process as qualified by the data quality evaluation process

Table 1 - Number of Samples Collected by Matnx, Method, and Type

Matrix	Analytical Method	Analytical Method Description	Prep Method	Leach Method	S N	FD	EB	TB.
! SO	SW8260B	Volatile Organic Compounds by GCMS	SW5035	NONE	27	3	i ;	
WG	SW8260B	Volatile Organic Compounds by GCMS	SW5030	NONE	68	7	9	15
i WG	SW8270	GC/MS for Semivolatile Organics	SW3520	NONE	1			i
SO	SW8270C	GC/MS for Semivolatile Organics	SW3510C	SW1312	6			
SO	SW8270C	GC/MS for Semivolatile Organics	SW3550B	NONE	6		i i]
SO	SW9060	Total Organic Carbon	NONE	NONE	20			

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Frep.	SW5030	SW5030	SW5030	SW5030	SW5030	SW5035	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW3520
Analytical Method	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8270
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Table 2 - Frequency of Detection in Blanks

Table 3 - Data Validation Sub-Qualifiers

Code	Definition
TN	Tune
BS	Blank Spike/LCS
IS	Internal Standard
MS	Matrix Spike and/or Matrix Spike Duplicate Recovery
MD	Matrix Spike/Matrix Spike Duplicate Precision
2S	Second Source
SD	Serial Dilution
SS	Spiked Surrogate
LR	Lab Re-extraction or Re-Analysis
IC	Initial Calibration
CC	Continuing Calibration Verification
PD	Pesticide Degradation
LD	Lab Duplicate
2C	Second Column (Confirmation)
HT	Holding Time
PS	Post Spike
BL	Blank
RE	Re-extraction
DL	Dilution
IB	In Between MDL and RL
FD	Field Duplicate
OT	Other (Defined in DV Worksheet)
Order of Q	ualifiers is in Order of Importance, Impact on the Data

Table 4 - Percent Completeness by Analytical Fraction

Matrix:	Ana/Ext Method	Total Unique	Rejected Results	Difference	Percent Complete
SO	SW8270C	6	0	6	100
SO	SW8270C/SW1312	6	0	6	100
SO	SW8270C	330	0	330	100
SO	SW8270C/SW1312	42	0	42	100
so	SW9060	20	0	20	100
SO	SW8260B	780	0	780	100
WG	SW8270	55	0	55	100
WG	SW8260B	1976		1976	100
		3215		3215	!
	% Completeness				100.0

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Attachment A - Change in Quainfier Due to the Data Validation Process

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Attachment A - Change in Qualifier Due to the Data Validation Process

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Attachment A - Change in Qualifier Due to the Data Validation Process

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Attachment A - Change in Qualifier Due to the Data Validation Process



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SO M	MW-108-97	7.		SW8260B	SW5035	NONE	Bromomethane	ر ې	. >	>.⊃	i ⊐i	• =	- 0	 	DYKO DYKO	ي د
	MW-102-10	z		SW8260B	SW5030	NONE	Chlorobenzene	-	 >	_	•-	· ⊃	0	. -	UG/L	ပ္တ
	MW-102-8	z ;		SW8260B	SW5030	NONE	cis-1 3-Dichloropropene		 >	>	⊃í ►) 	0 0 0	1 10	UG/L	ပ္င
	WW-102-80	년 :	٠	SW8260B	SW5030	NONE	ന	-¦	ر 'د	; ص,	⊃i -) 	. 0 0 V	. 1.	UGA	ō
<u>-</u> -	MW-102-9	- z!:	ì	SW8Z60B	SW5030	NONE	ന	- <u> </u>	_	- -	±;	ار ا	0	1 10	UG/L	ပ ်
212	MW-101-103	-; - 2 2	1	SW8Z6UB	5W5030	NON:	ه, نب	- ·	> :	- - - :	اد - - -	기 L	0	1 1 1	UG/L	ပ
	MW-101-89	. 2	1	SW8260B	SWS030		cis-1, 3-Uichioropropene	- •	 > :	_ = c	ສ໌: - -	o : 	0 0		UGA	و ^ا ن م
-	WW-107-125B	z	- 4	SW8260B	SW5030	, INCA	ca. 13-Dichoropopera	- •	ביכ	 > =	ο = - -	 	6 6		5 5 5	ຼຸດ
WG MV	MW-107-147	z	• -	SW8260B	SW5030	NONE	cis-1 3-Dichloropropene) =	-	- -) = -	-		֖֖֖֖֖֖֖֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	<u>.</u> د
wg w	MW-108	z	;	SW8260B	SW5030	MON	cis-13 Dichloropropene	· -	, ,	_ ,,=	i,⊐	, <u>-</u>	0.0	- -	, , , ,	<u>.</u>
;	SW-2	. . .		SW8260B	SW5030	NONE	بن	; -	- ·	 	· -	` _			ng/L	<u>.</u>
-	WW :00-92 5	z	• -	SW8260B	SW5035	NONE	oluene	54	ر د	¦⊃	5.4 ·	;⊃ 	-	7 - 54	OG/KG	. <u>ن</u>
	MW-101-23	z,	•	SW8260B	SW5035	NONE	Toluene	, 151	: _ . →.	'⊃'	5: .	, ! 		66 51	UG/KG	ı İ
-	MW-:01-94	z ,¦	•	SW8260B	SW5035	NONE	Toluene	63	· .	, <u>.</u> '⊃:		;⊃;	- 1	82 63	UGIKG	<u>က</u>
-	MW-161-994	은 :		SW8260B	SW5035	NONE	Toluene	6	_	 : :>	6.9	`	0	69	OG/KG	ပ္ခ
	WW-104-10	2 2		SW8260B ·	SW5030	NON I	trans-1 3-Dichloropropene	- -	 >		- -			07 1 1	, UGAL	ū
	MW-104-2	2 2		SW8250B	SW5030	NONE		-		_	j	- -	000	- 1	UG/L	ပ -
2 2	MW-104-3	 Z Z	•	SW826UB	SW5030	NO CO		- ' · -	 : 'د	 - :	⊃ : 	⊃': ¬	0	1	ה הפאר	ပ္တ, (
	MW-104-5	2,Z	<u>-</u>	SWAZEOB	34V3030		trans-1 3-Dichloropropene): 	3¦: -:•) : 	0	- ' - - -	ਰ ਹੈ: ਹੈ:	<u>ი</u> .ლ
¦ _	MW-104-50	2	+	SW8260B	SW5030	HNCN	-1	- -	- - - c	- -	3 =	>;= - - -!-	000	· ·	100	<u>ي</u> د
	MW-104-6	2	† -	SWAZEOR	SW5030	INCN		- -		- -	3 : - -] - - -	0	- •	֓֞֝֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	ي د



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Unite State	N. B.	UGA	מלוי	ug'r	, Jo	ng/L	UG/L	1/5/n	ŮĠ.	: : 55 : 55				J/Sn	8	UGA	NG/L	Jon J	UG/L	NG/	ชา	ટું	- 2 2 3	ر ا ا	j.	, <u>7</u>		เอ็ก	l Ng/	NO/L	750	าย กั	ଅନ୍ତ୍ର	5 3	_1 	֡֝֞֝֟֝֟֝֟֝֟֝֟֟֝֟֝֟֝֟֟ ֓֓֓֓֞֓֓֓֓֞֓֓֞֓֓֓֓֞֓֓	100	า กับ	ng Ng	UGA	UG/L	ÚGL	UĞU	UG/L	֓֞֝֞֝֞֝֟֝֝֟֝֝֟֝ ֖֓֞֞֞֞֞֞֞֞֞֞֞֞֞֞֞֞֩֞֞֞֞֞֞֓֓֓֞֞֞֩֞֓֡֓֓֡֓	OG/KG	ر الحالة الحالة	֧֧֓֞֝֝֝֝֝֝֝֝֝֝֝֝֝֝֝֝֝֝֝֝֝֝֝֝֝֝֡ ֓֓֓֓֓֓֓֓֓֓		North
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F. C. S. S. S. S. S. S. S. S. S. S. S. S. S.	国内に対するというで	trans-1,3-D chloropropene	trans-1 3-Dichloropropene		trans-1 3-Dichloropropene		c,	trans-1 3-Dichloropropere	trans-1,3-Dichloropropere	trans-1,3-Dich oropropene	trans-1,3-Dichloropropene	trans-*,3 Dichloropropene	trans-1,3-Dichloropropene	trans-1 3-D chloropropene	trans-1,3-0 chloropropene				ų,	trans-1,3-2 chloropropene	trans-1,3-Dichloropropene			trans-1,3-Dichloropropene	ო	trans-1 3-Dichloropropene	ტ,	trans-1,3-Dichloropropene	trans-1,3-Dichloropropene		- •	rans-1 3-Dichloropropere	Tetrachloroethene	Tetrachloroethene	Tetrachloroethene	Tetrach oroethene	Tetrachicroethene	Tetrachloroethene	Tetrachloroethene	Tetrachloroethene	Tetrachloroethene	Tetrachloroe here	letrachioroethene	Terrach occeptions	Tochlocothere	Trichloroethene	Trichloroethene	Trichloroethene	Trichloroethene	Trichloroethene
Leach	1.00 ES.	NONE	NONE	NONE	NONE	NONE	NON I	NON-	NON!	NONE	NONE	NONE	NONE	NONE	NONE.	NONE	NONE	NONE	2 S		I II	L NO	NON	NONE	NONE :	NONE	NONE	NONE	UNON I	JONE NO.	- NON NO.		NON	NON	NON	NONE	NONE	NONE	NOVE S	NON	UNON !	W.L.	NON IN	N. CN	I INCK	NON	NONE	NONE	NONE	NONE
Prep Method		SW5030	SW5030	SW5030	SW5030	SW5033	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	24,5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SWEDS	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW5030	SW2000	SW5030	SW5035	SW5030	SW5030	SW5030	SW5030	SW5030
LR Analytical		SW8260B	SW8260B	SW8260B	SW8ZBUB	SW8ZBUB	SW8ZEUB	SW8260B	SW8260B	SW8260B -	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	S. M. 0.2600	SWRZEDB	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8Z6UB	SW8260B	SW8260B 1	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8Z608	SW8Z60B	SW8ZBUB	SIA/8250B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B
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Samp	Ser Seminary Action	MW-104-7	MAY-104-6	8-401-VVV	- 56-AAIA-	1414-00-100	201-165-161	7-56-00.0	MW-99-0	WW-99-4	WW-99-5	MW-99-50	9-66-MM	7-66-MW	8-6-MW	S AN AN AN AN AN AN AN AN AN AN AN AN AN	2 CO 1414	MAN-07-5	MW.97.6	7-76-WM	WW-97-8	MW-97-80	MW 102-8	WW.102-80	MW-102-9	MW-101-09	MW 101-124	MW-101-89	BCZL-/UL-WW	MW-109	SW-1	SW.2	MW-100-10	MW-100-2	MW-100-3	MW-100 4	WW-100-5	WW. 100-6	7-001-MW	0-00-00-00-00-00-00-00-00-00-00-00-00-0	100-001 - MANA 100-000	MW-101-109	MW-101-124	MW-101-89	MW-100-92 5	MW-104-10	MW-100-1	MW-100-10	MW-100-2	MW-100-3
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Table 1	oethe	roether	roethen	roether	oether	oether
arameter.	hlaroethe	chloroether	:h:oroethen	chloroether	chloroether	chloroether
Parameter Parameter Frichloroether	Trichlamethene	Trchloroether	Trichtoroathane	Trichloroether	Trichloroether	Trichloroether
Parameter Parame	Trichlomethe	Trchloroether	Trichloroethen	Trichloroether	Trichloroether	Trichloroether
Parameter Parame	Trichlaroethe	Trchloroether	Trichtoroathen	Trichloroether	Trichloroether	Trichloroether
	` I					
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	` I					NONE
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STYTHOLICE:	Transplantable return	Difference of	Language, Sam.	1 275 7 7 4. 3	In the Comment of the comment	I come (in)			1	r	
Matrix		Sample	Analytical	Prep	STATE OF	Lib	(Lab)	Lab		3.77=2.72 A	(4)
1	Sample ID	Type	& Method 3	Method	Parameter	Result	Qual	Conc	DL.	RL	Units
WQ	011010IB	I TB	SW8260B	SW5030	Bromomethane	15-3-25-15-6 0 59	100 495c	<u>'ପିଘରି। ି</u>	0 18	2 (SEE SE	X. 75454.
wo	011015TB	TB -	SW8260B	SW5030	. Bromomethane	0.53		J	0 18	¦	UG/L UG/L
WQ	011018TB	TB-	SW8260B	SW5030	Bromomethane	0 72		,	0 18		UG/L
WQ -	J1017W01	LB -	SW8260B	SW5030	Bromomethane	0 32	j		0 18		UG/L
WQ	J1018W01	LB	SW8260B	SW5030	Bromomethane	0 41		j	0 18		UG/L
WQ	J1025W01	LB	SW8260B	SW5030	Bromomethane	0.54	- <u>-</u>	- j	0 18	· i	UG/L
WQ	RB-1-JP	EB	SW8260B	SW5030	Bromomethane	1	<u> </u>		0 18	ii	ÜĞÆ
WQ	RB-2-AK	EB -	SW8260B	SW5030	Bromomethane	0.51			0.18	1 7	UGAL
WQ	011130TB	TB T	SW8260B	SW5030	Bromomethane	0 27	J		0 14		UG/L
WQ	R1207W01	LB	SW8260B	SW5030	Bromomethane	0 58	J	j	0 14	1	UG/L
WQ	R1210W01	ĹB	SW8260B	SW5030	Bromomethane	0 44	J	J	0 14	1 1	ÜĞÂ
wa	_R1211W01_	LB.	SW8260B	SW5030	Bromomethane	0 44	Ĵ	J	0 14	1	UG/L
_ <u>w</u> Q	R1212W01	<u> </u>	SW8260B	_SW5030	Bromomethane	0 33	J	J	0 14	- 1 į	UG/L
WQ	EB-6	EB	SW8260B	SW5030	Chlorobenzene	0 12	J_		01	1	ÜĞL
LWQ	EB 7	_EB	SW8260B	SW5030	Chlorobenzene	0 11	_ J _	<u></u>	0.1	1 -	UG/L
wo	K1217W01	LB	SW8260B	SW5030	Chlorobenzene	0 18	_ J		01	1	UG/L
wo	010919TB	TB	SW8260B	SW5030	Chloromethane	0 54	_ J _ j	. J	0 13	1	ÜĞ/L
WQ	011010TB	_ TB	SW8260B	SW5030	Chloromethane	0 63	J	J ,	0 13	1 1	UG/L
WQ	J0924W01	I.B.	SW8260B	SW5030	Chloromethane	0 29	_ <u>J</u> _]	_ J '	0 13	1 i	UG/L
WO	_J1018W01	L. LB	SW82608	SW5030	Chloromethane	0 18	J	;	0 13_	_ 1	UG/L
SQ	K1009S01_	LB	SW8260B	SW5035	Chloromethane	1.7	<u> </u>	J	06	10	UG/KG
WQ	R8-1-JP	EB .	SW8260B	SW5030	Chloromethane	3.7	= i	= :	_0 13	1 _	UG/L
wo	RB-2-AK	_EB	SW8260B	SW5030	Chloromethane	0 23			0 13	1	UG/L
wq_	R1207W01	LB	SW82608	SW5030	Chloromethane	0 29	J_ ¦		0 17	1	UG/L
WQ	R1210W01	LB	SW8260B	SW5030	Chloromethane	02		Ji	0 17	1	UG/L
WQ	R1211W01	LB	SW8260B	SW5030	Chloromethane	021	J	_ j ļ	0 17	1 1	UG/L
. wa wa	EB-1	EB :	SW8260B	SW5030	Chloromethane	0 19	_ i _ ;	J	0 13	1 }	UG/L
wa	EB-4 J1210W01	- EB	SW8260B	SW5030	Chloromethane	0 17	<u>J</u>	J	0 13	1 1	UG/L
- wa	011211TB	LB	SW8260B SW8260B	_SW5030 + SW5030	Chloromethane	0 14		_J_ i	0 13	1	UG/L
wa :	G1226WA1	ĹĎ	SW8270	·	Chloromethane	03	!'	<u>-</u> !	0 13	1	UG/L
-wa	0109191B	TB	SW8260B	SW3520 SW5030	Diethylphthalate	0.75	- ;	J	0.64	10 [UG/L
WQ	010924TB	~ YB -	SW8260B	SW5030	Methylene chloride Methylene chloride	0 66 ·			0 06	2	UG/L
	010926TB	TB .	SW8260B	SW5030	Methylene chloride	0 65			0 06 0 06	2	_ UG/L
WQ	011001TB	ŤB -	SW8260B	SW5030	Methylene chlonde	055	, - ;		_006	<mark>2</mark>	UG/L
wa	011010TB	TB	SW8260B	SW5030	Methylene chloride	0.26		- '	0.06	2	UG/L
wo-	0110151B	TB ,	SW8260B	SW5030	Methylene chloride	0.35	1	ا ز -	0 06	- 2	UG/L
wa	011018TB	- TB	SW8260B	SW5030	Methylene chloride	- 0.33 0.42 i			0 06	2	UG/L
WQ	011019TB	<u>8</u>	SW8260B	-\$W5030	Methylene chlonde	- 0 32 - L	· j~- ¦	;	-0 06	2 - -	UG/L
WQ	011022TB	TB	SW8260B	SW5030	Methylene chlonde	0 52	-	· - J̈— !	006		UG/L
WQ	R1210W01	LB -	SW8260B	SW5030	Methylene chlonde	0 12	- j -	·	- 0 11 +	~ - }	UG/L
WQ	J1213W02	LB	SW8260B	SW5030	Methylene chloride	0 084	·- -	ji	0 06		ÜĞÆ
WO_	011005TB	TB	SW8260B	SW5030	Methylene chloride	02	- -	<u>-</u>	0 06	· 2 - 1	UG/L
WQ	J1008W01	LB	SW8260B	SW5030	Methylene chloride	1			0.06		UG/L
wa	RB-1-JP	EB !	SW8260B	SW5030	Toluene	0 21	<u>5</u> -	<u>-</u> - +	0 12	- <u>-</u>	UGAL
wa	RB-2-AK	E8	SW8260B	SW5030	Toluene	0 22			0 12	- 1	UGAL
WQ	011130TB2	TB	SW8260B	SW5030	Toluene	0 34	- 	- -	0 12	- i - :-	UG/L
wa !	EB-1	EΒ	SW8260B	SW5030	Tolucne	0 15	~ J4.		0 12	- 1	UG/L
WQ	EB-2	EB	SW8260B	SW5030	Toluene	0 12	- <u>-</u> - †	- j	0 12	1	UG/L
WQ	LB-5	_EB	SW8260B	SW5030	Toksene	0 13			0 12	1 - 1	UG/L
WQ	EB-6	EB	SW8260B	SW5030	Toluene	0 18	7		0 12	1	UGAL
WO	EB-7	EB	SW8260B	SW5030	Toluene	0 18		ן נ	0 12	1	ÜĞA

140-55	a company and a	S seater. Fig.	小海绵	Programme	120 St. 400 C. C.	The Total	Bost State	19. 28 "19" 1937ur.	XST104675
		1233	F.S.	8	S S S	经可能数	第二8	S	家多交流
42					Ç Q	S OF S	ONE S	後9.20	
9.5	1.00		400	2.5	\$ 10 PER 18	200	N S E	3.45	20.00 E
74 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		Sample	LI R		₩ S. E.	2 6 8 5°	100 B	20 E	20 8 68 10 8 10 10 10 10 10 10 10 10 10 10 10 10 10
Matrix	Sample ID	Type	type	15.5	N O L	St 28 1	25.5	\$ Q	8 8 8 W
1			100	5.9	8 2	E O	第18 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	5 38 2	9 5 S
				6 E	3.2	22.2	2 8 8	25 E	12,00
4 10 3		300 mg		15 St. 5	A A CO		8.5	-0. S. D.	
43		100	199	20					建筑 。2006
SO	MW-85-84	N	ļ				96~61~118~	107~74~118~	98~58~122~
so	MW-86-78	N		<u> </u>	}	 	102~61~118~	102~74~118~	100~58~122~ 94~58~122~
SO SO	MW-85-97 MW-86-86	N		<u> </u>			87~61~118~ 99~61~118~	104~74~118~ 105~74~118~	99~58~122~
so	MW-88-78	<u>N</u>	 		 	 	94~61~118~	98~74~118~	96~58~122~
so	MW-88-788	FD		<u>i</u>	• • • • • • • • • • • • • • • • • • • •		91-61-118-	98~74~118~	94~58~122~
so	MW-92-77	N					92-61-118-	97~74~118~	95~58~122~ ;
SO SO	MW-92-96 MW-93-100	N N				<u> </u>	86~61~118~ 96~61~118~	94~74~118~ 107~74~118~	90~58~122~ 100~58~122~
j <u>so</u>	MW-94-108	N			' 		99~61~118~	112~74~118~	97~58~122~
· so	MW-93B-101	N -	ļ				102~61~118~	110~74~118~	104~58~122~
· so	MW-96-62	N			L		101-61-118-		94-58-122-
<u>SO</u>	MW-96-82	N				ļ	91-61-118-	106~74~118~	95-58-122-
so so	MW-98-106 MW-97-100	N N		·	!	<u> </u>	108~61~118~	105~74~118~	102~58~122~ ' 105~58~122~
so	MW-97-100	- N					94~61~118~	100~74~118~	97~58~122~
so	MW-99-90 5	N				'	104-61-118-	104-74-118-	101~58~122~
SO	MW-100-92 5	N					94~61-118~	111~74~118~	89~58~122~
. <u>so</u> _	MW-100-92 5DL	LR	DL				102~61~118~	101-74-118-	101~58~122~
SO SO	MW-101-23 MW-101-94	N					97~61~118~ 93~61~118~	111-74-118-	88-58-122- 87-58-122-
} - šo	MW-101-994	FD		}			91-61-118-	110~74~118~	87~58~122~
so	MW-102-108	Ñ					85~61~118~	102-74-118-	81~58~122~
so	MW-103-15	N	-				94~61~118~	98~74~118~	88-58-122-
SO SO	MW-103-72 MW-103-61	N N	r		·	}	87~61~118~ 92~61~118~	91~74~118~	95~58~122~ 91~58~122~
-sō	MW-104-63		——- <u>†</u>	· - ·i			90-61-118-	102-74-118~	97~58~122~
' so	MW-104-663	FD					85~61~118~	102-74-118-	92~58~122~
so .	MW-107-125	<u>N</u>					86-61-118-	104-74-118-	90~58~122~
SO SO	MW-101B-87 MW-108-97	N					90~61~118~ 105~61~118~	103-74-118-	92~58~122~ 102~58~122~
- SQ	C0927S02	LB			·		107~61~118~	102~74~118~	104~58~122~
SQ	C0927S02LCS	BS	j				94~61~118~ ;	96-74-118-	97~58~122~
SQ	C0928S01	LB					113~61~118~	102~74~118~	109~58~122~
SQ -	C0928S01LCS	BS	∔				94-61-118-	90-74-118-	88~58~122~ 109~58~122~
SQ SQ	C0928S01 C0928S01LCS	LB BS	لسسا	<u>i</u>		 		90~74~118~	88~58~122~
SQ	C0928S01	LB	——;	;			113-61-118-	102-74-118-	109~58~122~
SQ	C0928S01LCS	BS					94-61-118-	90~74~118~	88~58~122~ }
SQ	K1009S01	LB	1	‡			108-61-118-		109~58~122~
- <u>SQ</u>	K1009S01LCS C1010S01	BS LB				·	_1 <u>07-</u> 61-118- <u> </u> 	98-74-118-	98~58~122~
SQ	C1010S01LCS	BS					100-61-118-	101~74~118~	101-58-122-
ĪŠQ	C1010S01	LB		'			110~61~118~	- 	104~58~122~ ;
sa	C1010S01LCS	BS					-		101-58-122-
SQ -	C1019S01	LB					99~61~118~ 87~61~118~	109-74-118-	91~58~122~
SQ	C1019S01LCS K1020M01	BS LB					103~61~118~		108~58~122~
1	K1020M01LCS	BS						107-74-118-	105~58~122~
so	C1019501	LB		;	+ · · · · · · · · · · · · · · · · · · ·	i		109-74-118-	91~58~122~
SQ	C1019S01LCS	BS					87-61-118-		83~58~122~
SQ	K1023S01	LB BS	 	:			99~61~118~ ; 102~61~118~ ;		102~58~122~ 96~58~122~
SQ	K1023501LC5	LB	· ·		-		99-61-118-	102-74-118-	102~58~122~
so	K1023S01LCS	BS	: 	- +			102~61~118~	102-74-118-	96~58~122~_ '
SO	K1023S01	LB '					99~61~118~	102-74-118-	102~58~122~ ,

				Attachment	O - Opixed Sunt	ogate recoveries			
100	是是知识的	32(11)	A 18		新发生	The state of the	199		10000000000000000000000000000000000000
10	VALUE NO.	13.3	2.30	- S. J. F.	温等回 6个这	数是Ⅲ 。	S	製造 の対策	经经回次 [3]
	大 工作的			治理 医激	126.5	35 6 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	股份學表	1 6 6 6	一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个一个
5.3 8			5.5	5 2 3 S	THE ZIENE	Z.0	多数 of 注意	38 2 5 3 6	2 2 2 V
No.		3	\$6.50 m		ASS S		Z S	18 S 5 264	是是 3 次代表
	通过主义	Sample	:LR:	SW8260B/SW5030/NONE Bromofiluorobenzene	SW8260B/SW5030/ Ibromofluorometha	18 8 18 18 18 18 18 18 18 18 18 18 18 18	发 20年8月	A EST	SW8280B/SW803s/N
Matrix	Sample ID			5.6	\$ \$\$\$\$\$\$	*** *	100 CO	1.7 <u>9.8</u> AE	新心 美 種 [18]
		A Abe	Type	7 - 4 S 15 ME	12.50 SERVE	然为 275~%。	派系的	新新 公司[20]	後 X X X 医 高四
1		on the said	32.33	10000000000000000000000000000000000000	ANO EV		.825 C 20		(数学员:含字题)
小孩我就				0 0	N E	1.2% E	MAN DEPOSIT	A CERT	
SEE	(1)	1. 大	# C}	2.6%第	20 2 2		\$ 5 S	经验3.5 至	は変数を対し
1388		180	3.46	W. P. S. P.	经验5°至1支	200	Z a ±	180 SX	1.00 Met 3
1.00 3		国海滨		74 2 5 3 3 W	第二十二	A STATE OF THE STA			为是一种的
SQ	K1023S01LCS	BS		THE GOVERNMENTS		ا الدائد عامرة الإسرام ياتي به ميكنكا ا	102-61-118-	102~74~118~	96~58~122~
SQ	C1025S01	LB	<u>!</u>				109-61-118-	103~74~118~	104-58-122-
SQ	C1025S01LCS	BS	i				108~61~118~	103~74~118~	104~58~122~
•		1 55	-	00 74 400	404 70 426	106~74~124~	100 01 110	103 74 110	104 30 122
WG	MW-104-2	N	t	98~74~128~	104-70-136-	;		··	
WG	MW-104-3	N	j	99-74-128-	106-70-136-	108-74-124-			
WG	MW-104-4	N	:	98~74~128~	107~70~136~	107-74-124-	···		
i WG	MW-104-5	N	<u> </u>	97~74~128~	102~70~136~	106~74~124~			
WG	MW-104-50	FD		96~74~128~	106-70-136-	102~74~124~			
WG	MW-104-6	N	-	98~74~128~	102~70~136~	105~74~124~			
WG	MW-104-7	N	*	96-74-128-	107~70~136~	102-74-124-			
	MW-104-8	- N		90~74~128~	78~70~136~	117~74~124~			
WG _									
i WG	MW-104-9	<u> </u>		96-74-128-	103-70~136~	107~74~124~			
WG	MW-104-10	N	L -	96~74~128~	104~70~136~				
WG	MW-104-10DL	LR	DL	94-74-128-	106~70~136~	98~74~124~			
WG	MW-99-1	N	ĩ	99~74~128~	102~70~136~	106~74~124~			1
WG	MW-99-2	N		96~74~128~	106~70~136~	105~74~124~			
WG	MW-99-3	,N	: _	91-74-128-	100~70~136~			·	
WG	MW-99-4			96~74~128~	105~70~136~	105~74~124~			
	+			~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		·			— — ———
WG	MW-99-5	N	;	101-74-128-	108-70-136-	113-74-124-	!		
WG	MW-99-50	FD		105~74~128~	109-70-136-	102~74~124~			
WG	MW-99-6	N		91-74-128-	105~70~136~	106~74~124~		<u> </u>	
WG	MW-99-7	N	,	88~74~128~	106~70~136~	100~74~124~			
' WG	MW-99-8	N		97~74~128~	94~70~136~	100~74~124~			
WG	MW-99-9	,N_	-	94~74~128~	102~70~136~	107~74~124~	· 		
WG	MW-99-10	N		97~74~128~	98~70~136~	106~74~124~			
WG T	MW-99-100	FD :	\$	95~74~128~	104~70~136~	109-74-124-			
	MW-97-3			103-74-128-	130~70~136~	103-74-124-	·		
WG	<u> </u>	N	·						
WG	MW-97-4	. N	! r -	105-74-128-	126~70~136~				
'_WG_	MW-97-5	. <u>N</u> .	[_	101-74-128-	130~70~136~	99-74-124-			
WG	MW-97-6	N		99~74~128~	128~70~136~	103~74~124~			L
j WG	MW-97-7	N		100~74~128~	120~70~136~	103~74~124~			
WG	MW-97-8	N	 -	105~74~128~	114~70~136~	106~74~124~			
WG	MW-97-8DL	LR	DL	90~74~128~		103~74~124~	· · - · · ·	·	
WG	MW-97-80	FD	, =	98~74~128~		103-74-124-			; - i
)	MW-97-80DL	•- •	<u>-</u>	94~74~128~					
WG_	 	LR	DL .		98-70-136-	102-74-124-			
WG	MW-98-1	<u>N</u> _		100~74~128~	99-70-136-	103-74-124-			<u> </u>
WG	MW-98-1DL	LR	DL	93-74-128-	95-70-136-	100~74-124~			i
WG	MW-98-2	<u>N</u>	.	95~74~128~	98-70-136-	101~74~124~			· · · · · · · · · · · · · · · · · · ·
WG	MW-98-2DL	LR	DL	93~74~128~	96~70~136~	104~74~124~			
WG	MW-98-3	N		97~74~128~	100~70~136~	102-74-124-	-		
' WG	MW-98-4	<u> </u>		95~74~128~	97~70~136~	100~74~124~		-	
" WG	MW-98-5			95~74~128~	101-70-136-	105-74-124-	·		
- W G	MW-98-5DL		DL	95-74-128-	96~70~136~	104-74-124-			
WG	MW-103-1	N		92~74~128~		103-74-124-			
	<u> </u>		; ·						
\ WG	MW-103-2	N	· 	95~74~128~		103-74-124- ,			<u> </u>
WG	MW-103-3	N	<u> </u> _	94~74~128~	96-70-136-	102~74~124~ }			
WG	MW-103-4	N N		96~74~128~	96~70~136~	106~74~124~	. <u> </u>		
WG	MW-103-5	, N	L	89~74~128~	90~70~136~	102~74~124~			
WG	MW-103-50	FD		93~74~128~	96~70~136~	106~74~124~			
WG	MW-103-6	N		94~74~128~		104~74~124~			
' WG	MW-103-7	N ,		92-74-128-	98-70-136-	110~74~124~			
wG W	MW-103-8		•	94-74-128-	98~70~136~	109~74~124~			
	MW-103-9	+ -N		93-74-128-	99~70~136~	109~74~124~ ,			<u> </u>
WG						/			
WG	MW-103-10	'N		88~74~128~	92~70~136~	 .			-
WG	MW-104-1	<u> </u>		92~74~128~	96~70~136~	104~74~124~			
, WG	MW-94-1DL	LR	ĎΓ	104~74~128~	97~70~136~	102~74~124~			

Delia		137.53	TESTY	148×4 14 4×2	THE STATE OF	1 Ping the wall	- 	Part of the same	学习 .游心心态
		Ser siene	门京新	1 A 2 3 1	E S	河流 罗港	80	SEL	i garage
MAR.			148	N 30.2	2.2	N Single	N. S. S.	V Ž E	Q of
				2.0012	20.5		Z	7.5	200
Matrix	Sample ID	Sample		00 g	25 25 5 5 5 5 5 5 5 5 5 		8 9 7	4 % E	· Section
		Type	Type	S .0	8 5	S B C	A STORE	N O	2 2 5 7
e 3, 62		***		0.00	8280B/SWS	1 8 E	3296	作-85.5	* Sec. 18
				25.5	N.O.	8 × ×	20.0	\ \	
1	357.335			5			S.W.S.	- T	1
WG	MW-94-2	N		103-74-128-	95-70-136-	102-74-124-			
WG	MW-94-2DL MW-100-1	LR N	DL	103~74~128~ 114~74~128~				· 	
WG	MW-100-1DL	LR	DL		109~70~136~				
WG WG	MW-100-2	N		104~74~128~		100-74-124-	,		
WG-	MW-100-2DL MW-100-3	LR N	DL	104-74-128- 109-74-128-					
WG	MW-100-3DL	LR	DL	102-74-128-				<u></u>	
WG WG	MW-100-4	N	<u> </u>	108~74~128~		102-74-124-			
WG	MW-100-4DL MW-100-5	LR N	DL	101~74~128~	_96~70~136~ 102~70~136~	102-74-124-		·——	
WG	MW-100-5DL	LR	DL	106-74-128-	117~70~136~	106-74-124-			
WG WG	MW-100-6 MW-100-6DL	LR	; ⊢+	109-74-128-	100-70-136-	·			
WG-	MW-100-6DL	N	DL	102~74~128~	97~70~136~ 101~70~136~	100-74-124-			
WG	MW-100-7DL	LR	ĎL	88-74-128-	98~70~136~	86~74~124~	·		
WG WG	MW-100-8 MW-100-8DL	LR		106~74~128~ 116~74~128~ ;	105~70~136~ 118~70~136~	101~74~124~			
WG	MW-100-80	FD	UL	98-74-128-	101-70-136-	99-74-124-	;		
WG	MW-100-80DL	LR	DL	102-74-128-	102~70~136~	97~74~124~			
WG	MW-100-9 MW-100-9DL	N 	- 	107~74~128~ 117~74~128~	100~70~136~ 123~70~136~	101-74-124-			
-wG	MW-100-10	- K - 1	· · · · ·	103-74-128-	105~70~136~	98~74~124~			i
WG	MW-100-10DL	LR	DL	100-74-128-	101-70-136-	92~74~124~			
WG WG	MW-102-1 MW-102-2	_ N	:	102~74~128~	99~70~136~ 102~70~136~	100~74~124~	!		
WG	MW-102-3	~~~N		104-74-128-1	100~70~136~	103~74~124~	- -	· - ·	
WG	MW-102-4	N	·	103-74-128-	99~70~136~	100-74-124-			
WG WG	MW-102-5 MW-102-6	N -		103~74~128~	101~70~136~ 103~70~136~	99~74~124~			· ~i
WG	MW-102-7	N ;	l	102~74~128~]	100-70-136-	100-74-124-			
WG WG	MW-102-8 MW-102-80	N FD		110~74~128~	104~70~136~	110-74-124-			
WG	MW-102-9	- <u>k</u> - †		107~74~128~ 109~74~128~		109~74~124~	— ļ		
WG	MW-102-10	N	 	107~74~128~	115~70~136~	103-74-124-			
WG	MW-108 MW-107-125B	N		104-74-128- 106-74-128-		i			
WG	MW-107-1238 ,	- 'N - +		106-74-128-		106~74~124~			
WG	MW-101-124	N		107-74-128-	101~70~136~	101~74-124~			
WG WG	MW-101-124DL MW-101-109	<u> </u>		102~74~128~ 99~74~128~	112~70~136~ 97~70~136~	100~74~124~ 97~74~124~	-		
WG	MW-101-109DL	- <u>:\</u>			110-70-136-	104-74-124-		-	
WG	MW-101-89	N				103-74-124-			
WG WQ	MW-101-89DL : 010919TB	LR			110~70~136~ 100~70~136~	102-74-124-			
wa	J0921W01	LB		102~74~128~	100~70~136~	104~74~124~			
WQ	J0921W01LCS	BS			95~70-136~	104~74~124~			
WQ WQ	010920TB :	TB LB			96~70~136~ 98~70~136~	109-74-124-	··	·· ·	
wo	J0924W01LCS /	BS			99-70-136-	107-74-124-			
WO	010924TB	TB			98-70-136-	98-74-124-			
- <u>w</u> a -	J0928W01 J0928W01LCS	LB : BS			101-70-136- 101-70-136-	100~74~124~	·		-
WQ	010926TB	ŤB `		99-74-128-	100~70~136~	99-74-124-			
WQ WQ	J0930W01 J0930W01LCS	LB ·			103~70~136~	103-74-124-			
	masowolf(2)	.BSi_	<u>-</u>	95-74-128-	99-70-136-	92-74-124-		<u> </u>	

Martin Samps D	4.64	12 m (C) 2	TES	《	Physical	建造之程 致		医 多种性	4-500-007-1-07
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WQ J1215W01 LB 109-74-128~ 114-70~136~ 105-74-124~ }	wa	J1214W02LCS [BS	100~74~128~	100~70~136~		· -		
The second secon	wo	J1215W01	LB [109-74-128-	114~70~136~	105-74-124-1			

Main	Sample ID	Sample Type	SW8260B/SW903B/NONE) (SW8260B/SW903B/NONE)
WQ	J1215W01LCS	BS	101-74-128- 101-70-136- 104-74-124-
WQ	J1219W01	LB	114-74-128- 108-70-136- 116-74-124-
WQ	J1219W01LCS	BS	106-74-128- 100-70-136- : 109-74-124-
WQ	K1217W01	LB	103-74-128- 104-70-136- 101-74-124-:
WQ	K1217W01LCS	BS	97~74~128~ 99~70~136~ 96~74~124~
wq	011221TB	тв	102-74-128- 94-70-136- 102-74-124-
WQ	J1224W01	LB	114-74-128- 101-70-136- 98-74-124-
WQ	J1224W01LCS	, BS	106-74-128- 105-70-136- 109-74-124-
' WQ	1	. 75	106-74-128- 110-70-136- 105-74-124-
AACS	J1227W01	LB	100-74-120-110-70-130-103-74-124-

1	\$ 10°55	Mary Mary Straight	Sample	亚建筑 。	Git D - Data Rejected Tillougi	1.00	E JOHN ST. C.	<u>£a6</u> *	1	E 1997	loge/le	، عالجه	100 N TO 100 N
ļ	Matrix	Sample ID		LRType	Parameter	Result	Qua	COST COST	Final	ĎŮ	RL	Units	DV Notes
ļ	WG	MW-100-2	Type	THE REAL PROPERTY.	Total Control of the	hear's			Qual	123.75		***	70
	WG	MW-100-2	<u> </u>		Tetrachloroethene Tetrachloroethene	48,	E	<u>E</u>	R	0 12	<u> </u>	UG/L UG/L	LR LR
	WG	MW-100-4	N		Tetrachloroethene	64	E	E		0 12	٠'	UG/L	LR
	WG	MW-100-5	N		Tetrachloroethene	63	Ε	E	R	0 12	! 1	UG/L	LR
	WG	MW-100-6	N		Tetrachloroethene	57	Ε	E	R	0 12	1 -	UG/L	LŔ
-	WG	MW-100-7	N		Tetrachloroethene	54	E	E	R	0 12	1	UG/L	LR
	WG :	MW-100-8	N		Tetrachloroethene	56	E	E	R	0 12	1	UG/L	LR
1	WG	MW-100-80 MW-100-9	FD N		Tetrachloroethene Tetrachloroethene	55 58	E	E	<u>R</u> R	0 12 0 12	1	UG/L UG/L	LR
- 1	WG	MW-100-10	N		Tetrachloroethene	43		E	' <u>R</u>	0 12	1	UG/L	LR LR
Ì	WG	MW-101-124	N		Tetrachloroethene	140	E		⊢R	0 12	1	UG/L	
	WG	MW-101-109	N		Tetrachlorocthene	140	Е	E	R	0 12	ĩ	UG/L	LR
	WG	MW-101-89	' <u>N</u>		Tetrachloroethene	140	E	E	R	0 12	1	UG/L	LR
!	- <u>SO</u>	MW-100-92 5	N		<u>Inchloroethene</u>	140	E	E	R	0 73	54	UG/KG	LR
j	WG WG	MW-104-10 MW-100-1	N		Trichloroethene Trichloroethene	20 48	E	E	_R _R	0 13		UG/L	LR
ì	wg-	MW-100-1	- N		Trichloroethene	67	E		<mark>r</mark>	0 13	-	UG/L ÜĞ/L	LR LR
ĺ	WG]	MW-100-3	N		Trichloroethene	71	E	E	R	0.13		UG/L	LR
ľ	WĠ	MW-100-4	N		Trichloroethene	80	Ē	Ε	<u>:</u> R	0 13	·· i	UG/L	LR
į	WG	MW-100-5	N		Trichloroethene	82	E	E	R	0 13	1_	UG/L	LR
١	WG ,	MW-100-6	N		Trichloroethene	78	E	E	R.	0 13	1	UG/L	LR
-	WG_ ; _ WG_ ;	MW-100-7	Ŋ		Trichloroethene	83	<u>E</u>	Ē	R	0 13	1 -	_UG/L_	LR
į	- WG	MW-100-8 MW-100-80	N FD		Tnchloroethene Tnchloroethene	80 76	E	E	R R	0 13	1	UG/L	LR
i	WG	MW-100-9	, N		Trichloroethene	81	E	- <u>E</u>	<u>R</u>	0 <u>13</u> 0 13		UG/L UG/L	LR
ł	WG	MW-100-10	N	لا۔ ۔۔۔۔ ا	Trichloroethene	-86	È	 }	<u>'</u> R	0 13	1 1	UG/L	<u>LR</u>
Ł	so	MW-100-92 5DL	LR	DL	1,1,1-Trichloroethane	570	Ū	Ū	R	59	570	UG/KG	DL
ĺ	_ <u>w</u> g	MW-104-10DL	ĹR	DL	1,1,1-Trichloroethane	2	<u> </u>	U	R_	0 24	2	UG/L	DL
ļ	WG	MW-97-8DL	LR	DL	1,1,1-Trichloroethane	2	_ U	U	R	0 28	2	UG/L	DL
	WG WG	MW-97-80DL	LR	DL	1,1,1-Trichloroethane	2	U	U	R	0 28	2	UG/L	DLi
Ī	-₩Ğ -	MW-98-1DL MW-98-2DL	LR L	DL DL	1,1,1-Trichloroethane 1,1,1-Trichloroethane	2 2	U	_ <u>U</u>	R . R	0 28 1	2	UG/L	DL
	`wg -	MW-98-5DL	LR	륪	1,1,1-Trichloroethane	2	- U		- <u>^-</u> -	0 28	2	UG/L UG/L	DL :
ı	WG .	MW-94-1DL	LR	DL	1,1,1-Trichloroethane	40	u	υ	'R' -	48	40	UG/L	<u>DL</u>
ľ	WG	MW-94-2DL	LR	DL	1,1,1-Trichloroethane	40	U	Ū	Ŕ	48	40	UG/L	DL
-	WG.	MW-100-1DL	LR	DL	1,1,1-Trichloroethane	5	Ü	U	R	06	5	ŪG/L ☐	DL
Į.	_WG	MW-100-2DL	LR	DL	1,1,1-Trichloroethane	10	U	U	<u>R</u> .	12	10	UG/L	DL
- }-	WG ;	MW-100-3DL MW-100-4DL	LR LR	DL DL	1,1,1-Trichloroethane	10	U	_ <u>_</u>	- <u>R</u>	12	-10	UG/L	DL
ŀ	MG 1	MW-100-5DL	LR -	DL	1,1,1-Trichloroethane	10 10	- U	U	R R	12	10	UG/L UG/L	DL DL ;
ŀ	WG T	MW-100-6DL	LR	DL	1,1,1-Trichloroethane	10	- ö -	Ü	R /	12	10	UG/L	
Ī	WG_	MW-100-7DL	LR	DL	1,1,1-Trichloroethane	10	U	Ŭ	<u>-</u>	12	10	UG/L	DL
Ĺ	WG :	MW-100-8DL	LR	DL	1,1,1-Trichloroethane	10	Ü	U	R	12	10	UG/L	DL DL
-	WG	MW-100-80DL	_ LR	DL	1,1,1-Trichloroethane	10	U	Ū	Ŕ	12	_10 [UG/L	DL
-	WG	MW-100-9DL	LR	DL	1,1,1-Trichloroethane	10	U	Ų	R	12	10	UG/L	DL ,
}-	WG ₩G	MW-100-10DL 7	LR I	DL DL	1,1,1-Trichloroethane 1,1,1-Trichloroethane	10	Ü	Ü	- R	12	10	UG/L	<u>DL</u>
ŀ	WG	MW-101-109DL	LR	DL.	1,1,1-Inchloroethane	40 40		$-\frac{\upsilon}{\upsilon}$		48	40	UG/L UG/L	DL ;
t	wG 1	MW-101-89DL .	- ii -+	DL	1,1,1-Trichloroethane	40	U	U	<u>'`</u> ` -	48	40	UG/L	DL
-	so	MW-100-92 5DL	LR	DL	1,1,2,2-Tetrachloroethane	570	Ü	U	<u>:</u> }	34		UG/KG	<u>ה</u>
Ĺ	WG ,	MW-104-10DL	LR	DL	1,1,2,2-Tetrachloroethane	2	Ū	Ū		0 181	2	UG/L	ĎL
}-	WG :	MW-97-8DL	LR _	DL	1,1,2,2-Tetrachloroethane	2 2	U	Ü		0 16	_2	UG/L_	DL
h	WG WG	MW-97-80DL MW-98-1DL	LR	-DL	1,1,2,2-Tetrachloroethane	. 2 -	Ü	<u>U</u>		0 16	2	UGÏL	DL
}-	WG i	MW-98-1DL .	LR	DL DL	1,1,2,2-Tetrachloroethane 1,1,2,2-Tetrachloroethane	2 2	U	U	R	0.16	$-\frac{2}{2}$	UG/L	DL
İ	wg	MW-98-5DL	LR -	DL	1,1,2,2-Tetrachloroethane		- U +	U ├	— <u>R</u> -	0 16	-2 -	UG/L UG/L	DL DL
1	WG	MW-94-1DL	LR T	DL	1,1,2,2-Tetrachloroethane	40	╗┼	U	- <u>'}</u>	36	40	UG/L	DL
	WG	MW-94-2DL	LR	DL	1,1,2,2-Tetrachloroethane	40	Ū	U	R	36	40	UG/L	DL
	WG	MW-100-1DL	<u>LR</u>	DL	1,1,2,2-Tetrachloroethane	0 81	DJ	J	R	0 45	5	UG/L	DL
ļ.	WG	_MW-100-2DL	LR	DL	1,1,2,2-Tetrachloroethane	10	U	U			10	UG/L	DL
ì	WG WG	MW-100-3DL 1 MW-100-4DL	LR LR	DL DL	1,1,2,2-Tetrachloroethane	- 10	<u>-u</u>	U	- <u>R</u> -R	09	-10 -	UG/L	DL
Ţ	WG	MW-100-4DL MW-100-5DL	- LR	DL	1,1,2,2-Tetrachloroethane	10	- 0	_0	Ŕ		10 10	UG/L UG/L	DL DL
-	WG I	MW-100-6DL	- LR	DL	1,1,2,2-Tetrachloroethane	10			<u>'</u> R	09	10	UG/L	DL
	WG	MW-100-7DL (LR	DL	1,1,2,2-Tetrachloroethane	10	υ υ	<u>u</u> [R	0.9	<u></u> :	UG/L	DL

海 Matrix	Sample ID	Sample	LR Type		Parameter.	Lab Result	Lab (Lab (Qual	Conc.	Final Qual	DL	RL	Units	DV Notes
USEE WG	MW-100-8DL	LR	DL	1.1.2.2	Tetrachloroethane	10	U	V. U	Literaturi R	0.9	10	UG/L	LABBET I
WG	MW-100-80DL	LR	DL		Tetrachloroethane	10	Ū	†ū	R	09	10	UG/L	DL
WG	MW-100-9DL	LR	DL		Tetrachloroethane	10	U	Ü	R	09	10	UG/L	DL
i WG ∫ WG	MW-100-10DL	LR	DL		Tetrachloroethane	10	U _	U	R	0.9	10	UG/L	DL;
WG	MW-101-124DL MW-101-109DL	LR LR	DL DL		Tetrachloroethane Tetrachloroethane	40	U	Ü	R	36 36	40 40	UG/L	DL DL
WG	MW-101-89DL	LR	DL		Tetrachloroethane	40	ΰ	Ü	R	3.6	40	UG/L	DL :
so	MW-100-92 5DL	LR	DL	1,1,2	-Trichloroethane	570	Ū	Ū-1	R	49	570	UG/KG	DL ,
WG	MW-104-10DL	LR	DL		Trichloroethane	2	U	U	R	0 24	2	UG/L	DL
WG_ WG	MW-97-8DL MW-97-80DL	LR LR	DL DL		-Trichloroethane -Trichloroethane	$-\frac{2}{2}$	Ü	U	- R -	0 22	2	UG/L	<u>- D</u> L
, wg	MW-98-1DL	LR	DL		Trichloroethane	2	U	Ü	R	0 22 0 22	2	UG/L UG/L	DL
WG	MW-98-2DL	LR	DL		Trichloroethane	2	Ü	Ŭ;	R	0 22	2	UG/L	- <u>D</u> L
WG	MW-98-5DL	LR	DL	1,1,2	Trichloroethane	2	U	ົບ້	Ŕ	0 22	2	UG/L	DL
WG	MW-94-1DL	LR	DL		Trichloroethane	40	U	Ü	R	48	40	UG/L	<u>DL</u>
WG WG	MW-94-2DL MW-100-1DL	LR LR	DL DL		Trichloroethane Trichloroethane	40 5	_ U	U	- <u>R</u>	48	40	UG/L	DL
WG -	MW-100-1DL	LR	DL		Trichloroethane	10	Ü	U	$-\frac{R}{R}$	12	5 10	UG/L UG/L	DL DL
WG	MW-100-3DL	LR	DL		Trichloroethane	10	<u>ٽ</u>	- -		12	10	UG/L	- DL
WG	MW-100-4DL	LR	DL :		Trichloroethane	10	U	U	R	1.2	10	ŰĞ/L	DL
WG	MW-100-5DL	LR	DL		Trichloroethane	_ 10	Ü	Ü	R	12	10	UG/L	DL
wg	MW-100-6DL MW-100-7DL	LR LR	- DL		Trichloroethane	10	U	<u>U</u> _ ;	- R	12	10	UG/L	DL
WG	MW-100-7DL	LR	DL		Trichloroethane Trichloroethane	10 10	U	<u>U</u>	<u>R</u>	12	10 10	UG/L UG/L	DL DL
WG .	MW-100-80DL	LR I	DL		Trichloroethane	16+	U	U -¦	R i	12	10	UG/L	<u>Dr</u>
WG	MW-100-9DL	LR	DL	1,1,2-	Trichloroethane	10	Ū-	Ū,	R	12	10	ÜĞ/L	DL
WG	MW-100-10DL	LR	DL		Trichloroethane	10	U	U	R	12	10	UG/L	DL ,
WG	MW-101-124DL	LR_	_ DL _ ;		Trichloroethane	_40 .	U	<u> </u>	_ R∔	48	40	UG/L	DL_
wg wg.	MW-101-109DL MW-101-89DL	LR I	DL DL		Trichloroethane Trichloroethane	40	U	Ü	R	48	40 40	UG/L UG/L	DL
so	MW-100-92 5DL	- 設 -	· DL '		chloroethane	570	U	- Ü '	R +	- 5 9	570	UG/KG	DL DL
WG -	MW-104-10DL	ĹR	DL		Dichloroethane	0 69	<u> </u>	j	-~¦?: +	0 24	2	UG/L	DL
WG	MW-97-8DL	LR	DL	~	Dichloroethane	2	U	υ,	R	0 28	2	UG/L	DL
WG	MW-97-80DL	LR	DL		Dichloroethane	2	U	U	<u>R</u>	0 28	2	UG/L	DL
− WG WG	MW-98-1DL [MW-98-2DL	LR LR	DL		Ochloroethane	2/2	_ <u>U</u>	U ,	- R	0 28	2 -	UG/L	DL - :
WG	MW-98-5DL	LR	DL :-		ichloroethane j ichloroethane i	$-\frac{2}{2}$	_U	- U 🚦	R R	0 28	$-\frac{2}{2}$	UG/L UG/L	<u>.</u> Dr
WG	MW-94-1DL	LR	DL ;		ichloroethane	40		· - Ŭ - +	R	48	40	UG/L	DL
wg.	MW-94-2DL	LR	DL	1,1-0	ochloroethane [40	Ü	ũ	ŔŢ	4.8	40	UG/L	DL ,
WG	MW-100-1DL	LR .	DL		ochloroethane	5	U	U	R	06	5]	UG/L	DL
WG	MW-100-2DL MW-100-3DL	LR LR	DL		hichloroethane	10	<u>U</u>	<u> </u>	R	12	10	UG/L	DL
WG	MW-100-3DL	LR	DL :		hichloroethane	10 10	υ	U	R	1.2	10	UG/L UG/L	DL DL
WG	MW-100-5DL	LR	DL		chloroethane	10	-ŭ-†	~~~~	~~ R	12	10	UG/L	DL ,
WG	MW-100-6DL	LR	DL [ichloroethane	10	Ü	. U .	_ R	12	10	UG/L	DL
WG	MW-100-7DL	LR	_DL		ichloroethane	10	U		R	12	10	UG/L	DL
WG -	MW-100-8DL MW-100-80DL	LR LR	DL i		ichloroethane	10	. <u>U</u>	<u>.</u> U	R	12	10	UG/L	DL
WG	MW-100-80DL	LR	DL	~- '-	ichloroethane	10	Ü	<u>u</u> ;	R	12	10	UG/L UG/L ;	DL \
- wG	MW-100-10DL	LR	<u>D</u> L †		chloroethane	10	Ü	Ü	R	12	10	UG/L	DĽ '
WG	MW-101-124DL	LR	DL ;		chloroethane	40	Ü	Ŭ T	R	48	40	UG/L	DL -
WG	MW-101-109DL	LR	DL		ichloroethane i	40		Ū į	R	48	40	UG/L	DL
WG	MW-101-89DL !	LR	DL		rchloroethane	40	Ų_,	U	R	48	40	UG/L	DL
SO :	MW-100-92 5DL MW-104-10DL	LR LR	DL ;		ichloroethene	570	U		R +	59		UG/KG	DL
WG	MW-97-8DL	LR	DL i		ichloroethene	13	D)	<u>n</u>		0 22 0 46	2	UG/L UG/L	DL DL
WG	MW-97-80DL	LR	DL -		chloroethene	2	-u -†	-ŭ-¦-		0 46	2	UG/L	DL - ;
WG :	MW-98-1DL	LR	DL	1,1-D	chtoroethene	2	Ū !	ับ	R	0 46	2	UG/L	DL ,
WG	MW-98-2DL	LR	DL		chloroethene	2	. U	Ū		0.46	2	UG/L	DL
wg_ wg	_ MW-98-5DL . :	LR	<u>DL</u>		ichloroethene	2	U	. U :		0 46	2	UG/L	<u>D</u> r
WG	_ MW-94-1DL	LR LR	DL DL		chloroethene	40	Ü	<u>u</u> U	$\frac{R}{R} \rightarrow$	44	40	UG/L ,	DF DF
wg	MW-100-1DL	LR	DL		chloroethene	5	- U	_U		0 55	5	UG/L ,	DL ,
wg _	MW-100-2DL	LR	DL		chloroethene	10	U	Ü	R	11	10	UG/L	DL
∏WG_,	_ MW-100-3DL	LR [DL	1,1-D	chloroethene	10	<u>ี้บู</u>	ַ עַ	_R	11	10	UG/L] DL]

	Mátrix	Sample ID	Sample	LR Type	Parameter Parameter	Lab	(Lab	~Lab?	Final			3326	至为不定
ģ			Typen	2.0	rarameter	Result	Qual	Conc	Qual	DL.	N.	Units	DV Notes
\Box	WG	MW-100-4DL	LR	DL	1.1-Dichloroethene	10	U	U	R	111	10	UG/L	DL
y -	WG WG	MW-100-5DL MW-100-6DL	LR LR	DL DL	1,1-Dichloroethene 1,1-Dichloroethene	10	U	ับ	R	11	10	UG/L	DL
	WG	MW-100-7DL	LR -	Di	1,1-Dichloroethene	. 10 10	U	U	R	11	10	UG/L UG/L	DL DL
	WG	MW-100-8DL	LR	DL	1,1-Dichloroethene	10	ับ	U	R	11	10	UG/L	DL
ļ.	WG WG	MW-100-80DL MW-100-9DL	LR	DL	1,1-Dichloroethene	10	U	U	R	11	10	UG/L	DL
	WG	MW-100-10DL	: - <u>LR</u> _	DL DL	1,1-Dichloroethene 1,1-Dichloroethene	10	U	Ü	R	11	10 10	UG/L UG/L	DL
	WG	MW-101-124DL	LR	DL	1,1-Dichloroethene	40	Ü	U	R	44	40	UG/L	DL
Ļ	WG.	MW-101-109DL	LR	DL	1,1-Dichloroethene	40	U	U	R	44	40	UG/L	DL
-	WG_ SO	MW-101-89DL MW-100-92 5DL	LR LR	DL	1,1-Dichloroethene 1,2-Dichloroethane	40 570	Ü	U	R	44	40	UG/L	DL _
-	WG	MW-104-10DL	LR	DL	1,2-Dichloroethane	2 7	U	Ü	R	67 0 22	570 2	UG/KG UG/L	DL
	WG	MW-97-8DL	LR	DL	1,2-Dichloroethane	7 2 '	U	֓֞֞֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֟֓֓֓֟֓֓֟	R	02	2	UG/L	DL -
-	WG WG	MW-97-80DL MW-98-1DL	LR .	DL	1.2-Dichloroethane	2	U	Ü	R	02	2	UG/L	DL
	WG	MW-98-2DL	, LR ! LR	DL DL	1,2-Dichloroethane 1,2-Dichloroethane	. 2	U	U	R	02	2	UG/L UG/L	DL DL
_	WG	MW-98-5DL	ĹŔ	DL -	1,2-Dichloroethane	2	Ŭ	Ü	R	02	2	UG/L	DL .
	WG]	MW-94-1DL	LR	DL	1,2-Dichloroethane	40	U	U	- R	44	40	UG/L	DL
— ~	WG WG	MW-94-2DL MW-100-1DL	LR LR	DL DL	1,2-Dichloroethane	40	U	U	R	44	40	UG/L	DL
	w G ;	MW-100-10L	LR		1,2-Dichloroethane	10	U	Ü	R R	0 55	5 10	UG/L UG/L	DL DL
_	WĞ	MW-100-3DL	LR	DL	1,2-Dichloroethane	10	ŭ	ŭ -	¦Ř-+	11	10	UG/L	<u>D</u> L
h	WG	MW-100-4DL	LR	DL	1,2-Dichloroethane	10	U	Ų	R	1.1	10	UG/L	DL
	WG	MW-100-5DL MW-100-6DL	LR LR	DL	1,2-Dichloroethane 1,2-Dichloroethane	10 1	U	Ü	R	11	10	UG/L	DL
-	WG i	MW-100-7DL	LR	DL :	1,2-Dichloroethane	10	Ü	U	R	11	10	UG/L	DL DL
· · ·	₩Ġ Ţ	MW-100-8DL	LR	DL	1,2-Dichloroethane	10	_ບີ ້	-ŭ-	R	11	10	UG/L	- DL
	WG WG	MW-100-80DL MW-100-9DL	LR LR	Dr;	1,2-Dichloroethane	10	U	U	R	11	10	UG/L	DL
_	wg T	MW-100-10DL	LR LR	DL	1,2-Dichloroethane	· _10 ·	_ U	U	R ;	11	10 10	UG/L UG/L	DL i
_	WG]	MW-101-124DL	LR	DL ,	1,2-Dichloroethane	+- 40 -;	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	Ű		44	40	UG/L	DL
	WG	MW-101-109DL	LR	DL	1,2-Dichloroethane	40		U	R	44	40	UG/L	ַ וֹסֹנ
	wg i	MW-101-89DL MW-100-92 5DL	<u>LR</u> .	DL DL	1,2-Dichloroethane 1,2-Dichloropropane	40 570	. <u>U</u>	U	R	44	40	UG/L	DL
1	wG 1	MW-104-10DL	LR	DL	1,2-Dichloropropane	2	- <u>ö</u> -†		R	69 0 22	570	UG/KG	DL DL
-	WG	MW-97-8DL	LR	DL	1,2-Dichloropropane	2	Ü	Ū		0 16	2	UG/L	<u>Dr</u>
	WG T	MW-97-80DL MW-98-1DL	LR	DL DL	1,2-Dichloropropane	2	Ų	U		0 16	2	UG/L	DL
	WG :	MW-98-2DL		- <u>DL</u>	1,2-Dichloropropane 1,2-Dichloropropane	2	U	U		0 16 0 16	2 2	UG/L UG/L	DL DL
	wg j	MW-98-5DL	_ LR	DL	1,2-Dichloropropane	2	ŭ -+	Ü		0 16	2	UG/L 1	DL
	WG]	MW-94-1DL	LR,	DL	1,2-Dichloropropane	40	Ų Į	U	R	4.4	40	UG/L	DL
	WG	MW-94-2DL MW-100-1DL	LR I	DL DL	1,2-Dichloropropane 1,2-Dichloropropane	40	Ū	U	R	44	40	UG/L	DL
	NG	MW-100-2DL	LR L	DL	1,2-Dichloropropane	5 10		Ü	R	0 55	5 10	UG/L	DL DL
	NG	MW-100-3DL	LR	DL	1,2-Dichloropropane	10	- U -	U	R	111	10	UG/L I	DL
	NG NG	MW-100-4DL MW-100-5DL	LR I	DL	1,2-Dichloropropane	10	U	U	R :	11	10	UG/L	DL
	WG +	MW-100-5DL	LR LR	DL 1	1,2-Dichloropropane 1,2-Dichloropropane	10	U U	Ü	R	11	10	UG/L UG/L	DL
[_V	NG	MW-100-7DL	LR	- D L~+	1,2-Dichloropropane	10		- ::	- R -+	11	10	UG/L +	<u>DL</u>
	NG	MW-100-8DL	LR	DL	1,2-Dichloropropane	10	U	Ü	R	11	10	UG/L	DL
	NG NG	MW-100-80DL MW-100-9DL	LR LR	DL DL	1,2-Dichloropropane	_10	Ū	<u>U</u>	R	11	10	UG/L	DL
	vg +	MW-100-10DL	···-LR	뜐+	1,2-Dichloropropane 1,2-Dichloropropane	10 10	U		R	11	10	UG/L UG/L	DL DL
v	٧Ġ	MW-101-124DL	LR	ĎL	1,2-Dichloropropane	40		<u> </u>	R	44		UG/L	DL
	VG	MW-101-109DL	LR	DL	1.2-Dichloropropane	40	ר יט־	U	R	44	40	UG/L	ÖL
	VG SO	MW-101-89DL 1	LR	DL	1,2-Dichloropropane Benzene	40	U	-U		44		UG/L	DL
V	VG :	MW-104-10DL	· LR ·	DL +	Benzene :	570 2 +	- 🖟	-U -	R	54 0 24		JG/KG UG/L	DL DL
	VG]	MW-97-8DL	LR '	DL i	Benzene	2	ΰ	U	R	0 28		UG/L	DL
	VG VG	MW-97-80DL MW-98-1DL	LR	DL - 1-	Benzene	2	U	U		28	2	UG/L	DL
	vg ¬-	MW-98-2DL	LR	DL :	Benzene Benzene		<u>u</u> -	- U -		0 28 0 28		UG/L UG/L	DL DL
N	VG	MW-98-5DL	LR !	DL.	Benzenc	2	U	U		0 28		UG/L	. מנ
<u>w</u>	/G	MW-94-1DL	LR	DL .	Benzene	40	U	<u>u</u> ''		4.8		ŪG/L	DL

Attachment D - Data Rejected Through the Data Validation Process

司制	BOY THE	Sample.	1		Lab	Lab	· Lab	Final		96	李 16年	
Matrix	Sample ID	Type	LR Type		Result	Qual	Conc	Quai	·DLY ···································	RL	Units	DV Notes
WG	MW-94-2DL	LR	LETTER LET	Benzene	40	U U	U	·追索亞 R	4.8	40	UG/L	DL
WG	MW-100-1DL	LR	DL .	Benzene	5-5-	T U	·	R	06	5	UG/L	DL
WG	MW-100-2DL	+LR	DL	Benzene	10	U	ن	R	12	10	UG/L	DL
WG	MW-100-3DL	LR	DL	Benzene	10	- U	ָר ער י	R	12	10	UG/L	DL
WG	MW-100-4DL	LR	DL	Benzene	10	U	υ	Ŕ	12	10	UG/L	DL
WG	MW-100-5DL	LR	DŁ	Benzene	10	U	Ü	R	12	10	UG/L	DL
WG	MW-100-6DL	LR	DL	Benzene	10	_ <u>V</u>	į ų)	<u>R</u>	12	10	UG/L	DL -
WG	MW-100-7DL	LR	DL	Benzene	10	Ū	<u>U</u>	R	12	10	UG/L	DL
WG ~	MW-100-8DL MW-100-80DL	LR LR	DL	Benzene	10	Ü	<u> </u>	R R	12	10 10	UG/L UG/L	DL
WG	MW-100-9DL	LR	DL DL	Benzene Benzene	10	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓		- <u>R</u> -	12	10	UG/L	DL
WG	MW-100-10DL	LR	DL	Benzene	10	Ü	}- อั- ₁	' <u>``</u>	12	10	UG/L	DL
WG -	MW-101-124DL	LR	DL	Benzene	40	· <u>~</u>	-Ū- 1	R	48	40	UG/L	DL
WG	MW-101-109DL	LR	DL	Benzene	40	U	Ū	-R	48	40	UG/L	DL
WG	MW-101-89DL	LR	DL	Benzene	40	ָ ט	Ū,	R	48	40	UG/L	DL
SO	MW-100-92 5DL	LR	DL	Bromodichloromethane	570	U_	Ū_;	Ŕ	63	570	UG/KG	DL
WG	MW-104-10DL	LIR	DL	Bromodichloromethane	2	U	U	R	0.16	2	UG/L	DL
WG	MW-97-8DL	LR	DL DL	Bromodichloromethane	2	U	<u> </u>	R	0 26	2	UG/L	DL
WG	MW-97-80DL	LR	DL	Bromodichloromethane	2	U	U	<u>Ř</u> ;	0 26	2	UG/L	DL
WG	MW-98-1DL	LR	DL	<u>Bromodichloromethane</u>	2	U	<u> </u>	R	0 26	2	UG/L	DL
WG	MW-98-2DL	LR	DL	Bromodichloromethane	2	Ü	ָּרְ בְּיִנֶּים בְּיִרְ	R R	0.26	2	UG/L	DL
WG -	MW-98-5DL MW-94-1DL	LR LR	DL [Bromodichloromethane Bromodichloromethane	- <u>2</u> - 40	Ü	. U,	- R	0 26	40	ÚĠ/L UG/L	DL DL
WG	MW-94-2DL	LR	DL	Bromodichloromethane	40	-	<u>u</u>	<u>R</u>	32	40	UG/L	DL
WG -	MW-100-1DL	LR	DL i	Bromodichloromethane	5	Ů-	<u>ŭ</u>	- <u>R</u>	04	5	UG/L	DL
wg	MW-100-2DL	LR	DL	Bromodichloromethane	10	υ	:	- ::: :	08	10	UG/L	DL 1
WG	MW-100-3DL	LR	DL !	Bromodichloromethane	10	T Ü	-	R	08	10	UG/L	DL
WG	MW-100-4DL	LR	DL	Bromodichloromethane	10	ַ ט	U	R	0.8	10	UG/L	DL
WG	MW-100-5DL	ĹŔ	DL !	Bromodichloromethane	10	υ,	υ,	R	08	10	UG/L	DĹ 1
WG	MW-100-6DL	LR	DL	Bromodichloromethane	10	Ų i		R	08	10	UG/L	DL i
WĞ	MW-100-7DL	LR	DL	Bromodichloromethane	10		U .	R	08	10	UG/L	DL
WG	MW-100-8DL	LR	DLi	Bromodichloromethane	10_	Ū	Ų	_R	0.8	10	UG/L	DL_
WG	MW-100-80DL	LR	DL	Bromodichloromethane	10	U	Ŭ	. <u>. R</u> <u>.</u>	08	10	UG/L	<u>D</u> L :
WG	MW-100-9DL	LR	DL	Bromodichloromethane	10	<u>U</u>	U	R	8.0	10	UG/L	DL DL
_ WG _+	MW-100-10DL MW-101-124DL	LR LR	DL	Bromodichloromethane	10 40	- U	ان	<u>R</u>	0.8 3 2	- <u>10</u> - 40	UG/L UG/L	DL
WG .	MW-101-124DL	LR	<u>DL</u>	Bromodichloromethane Bromodichloromethane	40	. U!		R	$\frac{32}{32}$	40	UG/L	DL
WG -	MW-101-89DL	LR	_ 	Bromodichloromethane	- 40-	Ŭ ·	ບັ- :		$-\frac{3}{3}\frac{2}{2}$	40	UG/L	
so	MW-100-92 5DL	LR	DĹ	Bromoform	570	<u>ٽ</u>			68		UG/KG	<u>D</u>
WG .	MW-104-10DL	LR	DL	Bromoform	2	U	ΰ	R	0 12	2	UG/L	DL
WG	MW-97-8DL	LR	DL	Bromoform		Ū	Ū	R ,	0 24	2	UG/L	DL
WG	MW-97-80DL	LR	DL	Bromoform	2 1		Ū,	R	0 24	2	UG/L	DL
WG	MW-98-1DL	LR	DL	Bromoform	2	U	Ū.	R	0 24	2 2	UG/L	DL
WG	MW-98-2DL	LR	DL	Bromoform	2	U	ָּרָע <u>ַ</u> '		0 24		ÜG/L	DL
WG	MW-98-5DL	LR	DL	Bromoform	2	U	<u> </u>		0 24	2	UG/L	DL
WG	MW-94-1DL	LR	DL	Bromoform	40	_ <u>U</u> _	Ū	_ R	24	40	UG/L	DL
WG	MW-94-2DL	LR	DL	Bromoform	40	U	<u>U</u>	-R	24	40	UG/L	DL
WG	MW-100-1DL	LR	_ DL:	Bromoform	5 1	Ü	U	R	03	5 10	UG/L UG/L	DL
WG	MW-100-2DL ! MW-100-3DL !	LR LR	DL DL	Bromoform	- <u>10</u> -	U	Ü	R	06	10	UG/L UG/L	DL;
wG :	MW-100-3DL	LR	DL	Bromoform	10 ;	- Ū		- <u>R</u>	06	10	UG/L	DL DL
wg	MW-100-5DL	- LR	DL :	Bromoform	10		- -	R	06	10	UG/L	DL
wG	MW-100-6DL	LR I	DL :	Bromoform	10	ٽ	Ŭ.	'` }	06	10	UG/L	יי ס <u>ר</u>
WG	MW-100-7DL	TIR T	DL ;	Bromoform	10	Ŭ	Ŭ	R	06	10	UG/L	DL
WG ,	MW-100-8DL	LR	DL	Bromoform	10	Ū	U	R	06	10	UG/L	DL [
WG	MW-100-80DL	LR	DL	Bromoform	10 ;	Ų	U	R	06	10	UG/L	DL
WG	MW-100-9DL	LR	DL	Bromoform	10	U	Ū	R	06	10	UG/L	_ DL
WG	MW-100-10DL	LR	DL	Bromoform	10	Ų	Ü	R	0.6	10	UG/L	DL ;
WG	MW-101-124DL	LR	DL	Bromoform	40	Ü	U	R	24	40	UG/L	DL
WG !	MW-101-109DL_	LR	Ďľ	Bromotorm	40		<u> </u>	_R	24	40	UG/L	Dr -
WG :	MW-101-89DL	LR	DL	Bromoform	_40 į	<u>V</u>	Ü	_R	24	40	UG/L	DL DL
SO .	MW-100-92 5DL MW-104-10DL	LR	DL -	Bromomethane Bromomethane	_570 { 2 {	U		R	81 0 36	— →	UG/KG	DL
_WG WG	MW-97-8DL	LR LR	DL ; DL	Bromomethane	0 68	U ;	_U_	R R [™]	0 28	$-\frac{2}{2}$	UG/L	DL DL
WG	MW-97-80DL	LR L		Bromomethane	0.88	P2	- j- :		0 28	· · · · · · · · · · · · · · · · · · ·	UGAL	DL T
								~	= .			

Matrix	Sample ID	Sample		Paramoter 24	, Lab	Lab	Lab? Conc	Final		紅華	21.03	DV Notes
		Llype	LR Type		Result	Qual s	Qual	Qual:		RL	Units	
WG	MW-98-1DL	LR	DL	Bromomethane	0.51	DJ	J	R	0 28	2	UG/L	DL
WG	MW-98-2DL	LR	DL	Bromomethane	0.7	_on	- <u>- j</u> _	_ <u>R</u>	0 28	2	UG/L	DL
WG	MW-98-5DL MW-94-1DL	LR LR	DL DL	Bromomethane	0.53	i U DJ '	<mark>.;</mark>	R	0 28	2	UG/L	DL
WG	MW-94-10L	LR	DL	Bromomethane Bromomethane	40 40	. <u>U</u>	_ U _ ;	R	72	40 40	UG/L UG/L	DL DL
WG	MW-100-1DL	LR	DL	Bromomethane	5	<u>ű</u> :	-	R	09	5	UG/L	DL
WG	MW-100-2DL	LR	DL ,	Bromomethane	10	U -	Ū	R	18	10	UG/L	DL
WG	MW-100-3DL	LR	DL	Bromomethane	10	<u>"</u> "	Ü	R	18	10	UG/L	DL
WG _	MW-100-4DL	LR	DL	Bromomethane	10	U		R	18	10	UG/L	DL .
L WG	MW-100-5DL MW-100-6DL	LR LR	DL DL	Bromomethane Bromomethane	10 10	' U	U.	R	18	10 10	UG/L UG/L	DL DL
wG	MW-100-7DL	LR	DL .	Bromomethane	10	U	U T	 	18	10	UG/L	DL
WG	MW-100-8DL	LR	DL	Bromomethane	10	ָּ ' ע	· Ď	R	18	10	ŲG/L	DL
WG	MW-100-80DL	LR	DL :	Bromomelhane	10	U	Ū	Ř	18	-10 T	UG/L	
WG	MW-100-9DL	LR	DL	Bromomelhane	10 ;	Ū	Ų	R	18	10	UG/L	DL
WG.	MW-100-10DL	LR	DL ,	Bromomethane	_10 _	, _U	Ü	R	18	10	UG/L	DL
WG WG	MW-101-124DL MW-101-109DL	LR LR	DL DL	Bromomethane	40	Ų	_ ਮੂ	R	72	40	UG/L	DL
WG	MW-101-89DL	LR	DL	Bromomethane Bromomethane	40	_ <u>U</u> .:	_ U	R	72	40	UG/L UG/L	DL
so	MW-100-92 5DL	LR	-ÔL	Carbon tetrachlonde	570	υ - ΄	_Ŭ!	R	65	570	UG/KG'	DL
WG	MW-104-10DL	LR	DL	Carbon tetrachlonde	- 2 -	-~ŭ'	υŢ	R	02	2	UG/L	<u>DL</u>
WG	MW-97-8DL	LR	DL	Carbon tetrachlonde		ַן טַ	ŭ <u>;</u>	R	0 28	2	UG/L	ĎĹ 1
WG	MW-97-80DL	LR	DL	Carbon tetrachlonde	_ 2 ;	ΰ	ű	R	0 28	2	UG/L	DL
WG_	MW-98-1DL	_ <u>LR</u>	DL	Carbon tetrachlonde	2	Ū	, U	R	0 28	2	UG/L	DL
wG WG	MW-98-2DL MW-98-5DL	LR LR	DL DL	Carbon tetrachlonde :	_2 ,	U .	U	R R	0 28	_2	UG/L	DL J
WG	MW-94-1DL	LR	DL	Carbon tetrachlonde	2 }	٠ - ال	- <u>U</u> .:	R	4	40	UG/L UG/L	DL
WĠ	MW-94-2DL	LR	DL	Carbon tetrachionde	40	Ü:	- Ŭ	 	4 1	40	- UĞ/L	DL -,
WG	MW-100-1DL	ĹŔ	DL	Carbon letrachlonde	5	Û	ֹ ט י	R	0.5	5	UG/L	DL (
WG	MW-100-2DL	LR	DL	Carbon tetrachlonde	10	_ [Ū_`	บั	R	1	10	UG/L	. <u></u>
, MG	MW-100-3DL	LR .	DL_	Carbon tetrachlonde	_10 -	U	Ų,	R	_1	10	UG/L	ĎĽ '
. WG . WG	MW-100-4DL MW-100-5DL	LR LR	DL ,	Carbon tetrachlonde Carbon tetrachlonde	10	n '	- U	$-\frac{R}{R}$	-1-	_10_	UG/L	<u>D</u> L — ;
⊢ wg	MW-100-6DL	LR	DL	Carbon tetrachlonde	- 10 <u>'</u>	- <u>n</u> ,	Ü	<u>'`</u> ;	~ ;	10 10	UG/L UG/L	Dr;
WG	MW-100-7DL	LR	DL	Carbon tetrachlonde	10	· Ū ·	ΰ	R		10	UG/L	DL
WG	MW-100-8DL	LR	DL,	Carbon tetrachlonde	10	Ü,	υ	R	1	10	UG/L "	DĹ
WG	MW-100-80DL	LR	<u>D</u> L'	Carbon tetrachlonde	10,	U	_Ų,	R	1 [10	ŪG/L	DL
WG_	MW-100-9DL MW-100-10DL	LR	_ DL _ ;	Carbon tetrachlonde	10	. <u>.</u> u ¦	⊍	- R		10	UG/L	Dr 4
WG	MW-101-124DL	LR L	<u>DL</u>	Carbon tetrachlonde Carbon tetrachlonde	$-{}^{10}_{40}$	U !	U Ū	R	<u> 1</u> -	10 40	UG/L , UG/L	DL ;
WG '	MW-101-109DL	LR	DL -	Carbon tetrachlonde	40	ដូ		R	$-\frac{4}{4}$	40	UG/L	·
WG .	MW-101-89DL	LR	DL	Carbon tetrachlonde	40	_ Ŭ 🗄	Ü	R	-4	40	UG/L	DL ,
SO	MW-100-92 5DL	LR	DL	Chlorobenzene	570	: ע־־	U "	R	54		ŪĠ/ĸĠŢ	DL
WG .	MW-104-10DL	LR	DL	Chlorobenzene	2	<u>`</u> Ŭ_	ΰ_,	- R	02	2	UG/L	DL
WG WG	MW-97-8DL	LR	<u>D</u> L	Chlorobenzene	2	Ü	∺-∔	R	02	_2_	UG/L_!	DL
WG :	MW-97-80DL MW-98-1DL	LR LR	DL :	Chlorobenzene	- 2. L			R	02	2	UG/L	DL
WG ~	MW-98-2DL	LR LR	- DL +	Chlorobenzene Chlorobenzene	2 1	<u>.u</u>	U U	R	02	2	UG/L UG/L	DL DL
WG	MW-98-5DL	LR	DL :	Chlorobenzene	2	Ü		R	02	2	UG/L	DL
WG	MW-94-1DL	LR	DL	Chlorobenzene	40		Ŭ-	R	4	40	UG/L	DL T
WG	MW-94-2DL	LR	DL	Chlorobenzene	40	. Ū [].	U	R	4	40	UĞ/L	DL
WG	MW-100-1DL	LR	DL'	Chlorobenzene	5	U	U	R	05	5	UG/L	DL
WG	MW-100-2DL	LR	- <u>DL</u>	Chlorobenzene	10	U	Ů.	_ R	1	10	UG/L T	DL
WG /	MW-100-3DL MW-100-4DL	LR LR	DL :	Chlorobenzene Chlorobenzene	10 1	_ <u>U</u>	U	R	1	10	UG/L UG/L	<u>DF</u>
wG	MW-100-5DL	LR	DL	Chlorobenzene	- 10 ÷	Ü	u †	R	+	10	UG/L UG/L	<u>DL</u> - ;
wG	MW-100-6DL	LR	DL	Chlorobenzene	10	. n_ 1	Ü	R	1	10	UG/L	DL
WG	MW-100-7DL	LR		Chlorobenzene	10	_ Ū	Ū	R	1	10	UG/L	DL
WG	MW-100-8DL	LR	DL	Chlorobenzene	10	u;	Ű	R	1	10	UG/L	DL
WG .	MW-100-80DL	LR_	DL	Chlorobenzene	_10	U	U	R	1	10	UG/L	DL
WG WG	MW-100-9DL MW-100-10DL	LR LR	_DL _DL	Chlorobenzene Chlorobenzene	10 10	U.	U	- R	-1-+	10	UG/L	DL .
, WG	MW-101-124DL	LR	DŁ	Chlorobenzene	40	U -	.U -‡	R	1 4	40	UĠ/L UG/L	DL ;
WG	MW-101-109DL	LR	DL (Chlorobenzene	40	-Ŭ .	υį	R	4	40	UG/L	DL -
WG	MW-101-89DL	LR	DL .	Chlorobenzene	40	Ū	Ū,	R	4	40	UG/L	DL
			-	~		-						

Attachment D - Data Rejected Through the Data Validation Process

di Pere	1 15 1 15 15 15 15 15 15 15 15 15 15 15	1200	1302363	A A A A A A A A A A	79. 12	N. Sar		~Lab	500 July 1	1 500	FL, S.A.	Sucre in	ASSESSED AND A SECOND
Matrix	Sample ID	Sample	LR Type	Parameter 2	12.,4	Lab Result	Lab Qual	Conc Qual	Final Qual	ĎĽ	RL	Units	DV Notes
SO	100 00 50	Type	137537		إلى	المستشالية	متند المتند		نعمتك		YY		
WG	MW-100-92 5DL MW-104-10DL	LR LR	DL DL	Chloroethane Chloroethane	_ ::	570 j	· - U	U	R	0 22	<u>. 570</u> .	UG/KG	DL DL
WG	MW-97-8DL	LR -	DL	Chloroethane		· - ·	. Ū	- 0	R	0 28	2	UG/L	DL
WG	MW-97-80DL	LR	† <u>D</u> L	Chloroethane	:		Ŭ	Ŭ-	R	0 28		UG/L	DL
WG	MW-98-1DL	ĹR	DL	Chloroethane		2	υ_	Ü	R	0 28	2 2	UG/L	DL
WG	MW-98-2DL	LR	, DL	Chloroethane		2	U	U	R	0 28	2	UG/L	DL
WG	MW-98-5DL	LR	DL	Chloroethane	- 4	2	~ - <u>U</u> _	U	R	0 28	_ 2_	UG/L	DL
WG	MW-94-1DL MW-94-2DL	LR LR	DL	Chloroethane Chloroethane	- -	- 40	<u>U</u>	U	R	44	40	UG/L	DL
WG	MW-100-1DL	LR	DŁ	Chloroethane	i	40 5	U	U	R	0 55	40 5	UG/L	DL DL
WG	MW-100-2DL	LR	DL	Chloroethane	· i	jo i	Ŭ	U	- <u> </u>	11		UG/L	DL
WG	MW-100-3DL	LR	DL	Chloroethane	~	10	_Ū	Ū	R	11	10	UG/L	DL
WG	MW-100-4DL	LR	DL	Chloroethane		10	U	U	R	11	10	ÚGAL	DL
WG	MW-100-5DL	LR	DL	Chloroethane	1.	_10	<u> </u>	U	<u>R</u>	11	10	UG/L	DL
WG WG	MW-100-6DL MW-100-7DL	LR LR	DL DL	Chloroethane	!_	10	_ <u>U</u> _	<u>U</u>	R	11	10	UG/L	DL
WG	MW-100-8DL	LR	- DL	Chloroethane Chloroethane		10 10	- U	<u>u</u>	R R	11	10 10	UG/L UG/L	DL DL
WG	MW-100-80DL	LR	DL	Chloroethane		10	Ü	-	R	11	10	UG/L	DL
WG	MW-100-9DL	LR	DL	Chloroethane		10	Ŭ-†	·ប៉	R	<u> </u>	10	UG/L	DL
WG	MW-100-10DL	LR	DL	Chloroethane	:	10	_ U	Ū-	R	11	10	UG/L	DL
WG	MW-101-124DL	LR	DL	Chloroethane	- ;	40	U		R	44	40	ÛG/Ĺ	DL
WG	MW-101-109DL	LR_	DL	Chloroethane	;	40	U	U	R	44	40	UG/L	DL
WG SO	MW-101-89DL MW-100-92 5DL	LR /	DL DL	Chloroethane		40	U		R	44	40	UG/L	DL
-WG	MW-104-10DL	LR	- DL	Chloroform Chloroform		570 ·	n I	_ <u>_</u>	R R	65 0 24	570 2	UG/KG UG/L	DL DL
WG	MW-97-8DL	ĹR	DL	Chloroform		23 :	-U	Ū ¦	- R	0 28	. 2	UG/L	DL
WG	MW-97-80DL	LR	DL	Chloroform		2 -	Ŭ	-ŭ-l	R	0 28	2.	UG/L	- DL
wg '	MW-98-1DL	LR	DL	Chloroform	:	0 29	ַ בֿעם	J;	R	0 28 ,	- <u>ź</u>	UG/Ĺ	DL
WG	MW-98-2DL	LR	DL	Chloroform	- 	2 ,	U		R	0 28	2	UG/L	DL
WG -	MW-98-5DL	- <u>rB</u> -1	. DL	Chloroform		2 .	- !!	<u>U</u>	<u>R</u> .	0 28	2	UG/L	DL
WG	MW-94-1DL MW-94-2DL	LR LR	DL	Chloroform Chloroform		40	Ü	U i	R	48	40 .	UG/L	<u>DL</u>
WG-	MW-100-1DL	- LR	DL -	Chloroform	- 1-	40 5	- U -+	- U -	~ -R · ·	48 06	40 5	UG/L UG/L	DL DL
WG	MW-100-2DL	LR	DL	Chloroform	-	10	-ŭ- †	-	<u>``</u>	$\frac{30}{12}$.	10	UG/L	- DL
WG	MW-100-3DL	ĹR	DL	Chloroform	,	10	Ū	- U	R	12	10	UG/L	DL
WG ·	MW-100-4DL	_LR	DL	Chloroform		10	U	U	R	12	10 ,	UG/L	DL
WG	MW-100-5DL	_LR	DL	Chloroform	4	10	U	Ū	R	12	10	UG/L	DL
WG WG	MW-100-6DL MW-100-7DL	LR LR	DL DL		!	_ 10	U	U		12	10	UG/L	DL
WG :	MW-100-8DL	- LR	DL	Chloroform	'	- <u>10</u> - <u> </u> 10	- + -	. <u>u</u> -	R	12	10 !	UG/L { UG/L }	DL DL
WG	MW-100-80DL	LR	DL	Chloroform	. ل	10 +	ŭ	Ü	R	12	10	UG/L	DL
WG	MW-100-9DL	LR	DL	Chloroform	- 1	10	Ū	Ü	R	12.	10	UG/L	DL
WG_	MW-100-10DL :	LR	DL	Chloroform		10	U	U	R	12	10	UG/L	DL
WG	MW-101-124DL	LR	DL	Chloroform		40	U	Ü	R	48	40	UG/L	DL
WG WG	MW-101-109DL 3 MW-101-89DL	LR	DL	Chloroform		40	Ū_	Ü	R	48	40_	UG/L	DL
SO	MW-100-92 5DL	LR LR	DL +	Chloroform Chloromethane	1.	40 570 ;		U	R	4.8 71	40	UG/L UG/KG	DL
WG	MW-104-10DL	LR -	DL	Chloromethane		2	Ū	- U		0 26		UG/L	DL
WG	MW-97-8DL	LR	DL	Chloromethane		0 38 1	. Ľ	- j +		0 34	2 2	UG/L	DL
WG	MW-97-80DL	LR	DL	Chloromethane		04	DJ	J		0 34	2	UG/L	- <u>DL</u> -
WG	MW-98-1DL	ĹŔ	DL	Chloromethane]	2	Ū	U	Ri	0 34 1	2	UG/L	DL
WG	MW-98-2DL	LR	DL	Chloromethane		0 37	DJ	j		0 34	2	UG/L	DL
WG	MW-98-5DL	LR	_DL_	Chloromethane		0.36	Dì	J		0 34	2	UG/L	DL
WG	MW-94-1DL MW-94-2DL	LR I	DL	Chloromethane Chloromethane	1	40	U	U	R	52	40	UG/L	DL
WG	MW-100-1DL	LR -	- <u>DL</u> -	Chloromethane		. 10 . [5 .	- U 	U		5 2 0 65	40 5	UG/L	DL DL
WG	MW-100-2DL	LR	DL	Chloromethane	- 5	10	-	u		13	10	UG/L	DL
WG ,	MW-100-3DŁ	LR 1	DL	Chloromethane	- ;	10	u	U		1.3	10	UG/L	DL
WG	MW-100-4DL	LR	DL	Chloromethane	;	19 📜	וַס	J	Rİ	13	10	UG/L	DL
WG I	MW-100-5DL	_LR	DL	Chloromethane		10	U	U		13		UG/L	DL
WG L	MW-100-6DL	LR	DL	Chloromethane		17.	DJ	J		13		UG/L	_ DL
WG ,	MW-100-7DL MW-100-8DL	LR]	DF	Chloromethane Chloromethane		23 16	합	J	R	13		UG/L	DL
WG	MW-100-80DL	LR L	- DL - T	Chloromethane		10	ָ <u>֖</u>	J		13 13	10 10	UG/L !_ UG/L	DL DL
wĠ '	MW-100-9DL	LR -	_pr -{-	Chloromethane		18 +	<u> </u>	- 5		13		UG/L	<u>pr</u>
		~ 'J .				·- · · · · · ·		<u> </u>	:`	. ' . ' . !			

Matrix	Sample ID	Sample	LR Type	Parameter .	Lab	Lab	Conc	Final	DL	ŘĽ.	Units	DV Notes
2 011111		*Type *	1		Result	oual	Qual	EQual :	DL	建設		
WG	MW-100-10DL	LR	DL	Chloromethane	10	<u></u>	U ~	ĻĘ.	13	10	UG/L	DL
WG	MW-101-124DL	LR	DL	Chloromethane	40	U	U	, <u>R</u>	5 <u>2</u>	40	UG/L	DL
WG WG	MW-101-109DL MW-101-89DL	LR LR	DL DL	Chloromethane Chloromethane	40	U	U	<u>R</u> R	5 2 ·	40 40	UG/L UG/L	DL DL
šo	MW-100-92 5DL	LR -	DL	cis-1,3-Dichloropropene	570	-ŭ	Ü	. R	55	570	UG/KG	DL
WG	MW-104-10DL	LR	DL	cis-1,3-Dichloropropene	2	Ū	Ū	R	0 14	2	ŬĠ/L	DL
WG	MW-97-8DL	LR	DL	cis-1,3-Dichloropropene	2	Ū	<u> </u>	R	0 22	2	UG/L	DL
WG	MW-97-80DL	LR	DL	cis-1,3-Dichtoropropene	2	U	Ü	. R	0 22	2	UG/L	DL
WG	MW-98-1DL MW-98-2DL	LR LR	DL	cis-1,3-Dichloropropene	2	Ü	Ü	R	0 22	2	UG/L UG/L	DL DL
WG	MW-98-5DL	LR	DL	cis-1,3-Dichloropropene cis-1,3-Dichloropropene	2 - ~	U	Ū	R.	0 22	2 -	UG/L	DL
WG	MW-94-1DL	LR	DL	cis-1,3-Dichloropropene	40	ٽا	_ U	R	28	40 1	UG/L	DL
WG	MW-94-2DL	LR	DL	cis-1,3-Dichloropropene	40	Ü	Ü	Ŕ	28	40	ŪG/L	DL
WG	MW-100-1DL	LR	DL	cis-1,3-Dichloropropene	5	U	U	R	0.35	5_,	UG/L	DL
WG	MW-100-2DL	LR	DL	cis-1,3-Dichloropropene	10	U	<u>u</u> _	<u> </u>	0.7	10	UG/L	DL (
WG WG	MW-100-3DL MW-100-4DL	LR LR	DL -	cis-1,3-Dichloropropene	10	U		R	07 07	10	UG/L \	DL DL
WG	MW-100-4DL	LR	DL	cis-1,3-Dichloropropene cis-1,3-Dichloropropene	10	U	- 0 -	<u>R</u>	07	10	UG/L	DL -
WG	MW-100-6DL	LR	DL	cis-1,3-Dichloropropene	10	-5-	U	R	07	10	UG/L	DL
WG	MW-100-7DL	LR	DL	cis-1,3-Dichloropropene	10	Γ- Ū-	- Ŭ	R	07	10	UG/L	DL
WG	MW-100-8DL	LR	DL	cis-1,3-Dichloropropene	10	Ū	Ü	Ŕ	07	10	UG/L	DL ,
WG	MW-100-80DL	LR	DL	gis-1,3-Dichloropropene	10	Ų		R	07	10	UG/L ;	DL
WG	MW-100-9DL	LR	DL	cis-1,3-Dichloropropene	10	Ū	_ <u>U</u>	R	07 [10	UG/L	<u>DL</u> 1
WG WG	MW-100-10DL MW-101-124DL	LR LR	DL DL	cis-1,3-Dichloropropene cis-1,3-Dichloropropene	10 40	Ü	U	R R	07 28	10 40	UG/L (DL)
WG	MW-101-109DL	LR LR	DL -	cis-1,3-Dichloropropene	40	-ŭ-	ö	R	28	40	UG/L	DL
WG	MW-101-89DL	LR	DL	cis-1,3-Dichloropropene	40	U	Ū	R	28,	40	UG/L	- Di 1
so	MW-100-92 5DL	LR	DL	Dibromochloromethane	570	ີບໍ່	Û	R T	59		ŪĠ/ĸĠ	DL
WG	MW-104-10DL	LR	DL	Dibromochloromethane	2	U		R	0 14 :	2	UG/L	DL
WG WG	MW-97-8DL	LR -	DL	Dibromochloromethane	2	U	. U .	R	0 22		UG/L	.DL .
WG_	MW-97-80DL MW-98-1DL	LR LR	DL DL	Dibromochloromethane Dibromochloromethane	-2 -2	<u>U</u>	- U	R	0 22	~ 2 2	UG/L UG/L	DL DL
wG	MW-98-2DL	LR	DL	Dibromochloromethane	2	Ü	<u>-</u>	R	0 22	2 .	UG/L	DL
WG	MW-98-5DL	LR	DL	Dibromochloromethane	2	Ū	i	R	0 22	2	ŪG/L	DL
WG	MW-94-1DL	LR	DL	Dibromochloromethane	40	U	Ū_	R	28	40	ŪĠ/L	DL T
WG	MW-94-2DL	LR	DL .	Dibromochloromethane	40	<u> </u>	U	R	28	40	UG/L ;	DL
WG WG	MW-100-1DL MW-100-2DL	LR LR	DL DL	Dibromochloromethane Dibromochloromethane	5 10	֓֞֞֞֞֓֞֓֞֞֓֓֓֞֞֞֓֓֓֓֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֞֝֓֓֓֞֝֓֡֝֡֓֡֝֡	U :	R	0 35	5_ \ 10 \	UG/L UG/L	DL
WG	MW-100-3DL	LR	DL	Dibromochloromethane	10	-	ប៊	- -	-07	10	UG/L	DL
WG	MW-100-4DL	LR	DĹ	Dibromochloromethane	10	Ū	Ū	Ŕ	07	10	UG/L 1	DL
WG	MW-100-5DL	LR	DL	Dibromochloromethane	10	U	Ū	R	07	10	UG/L	DL
WG	MW-100-6DL	LR	DL	Dibromochloromethane	10	U	U	R	07		UG/L	DL
wg	MW-100-7DL	LR	DL	Dibromochloromethane	10	U	Ų.	R	0.7	10	UG/L	DL
WG WG	MW-100-8DL MW-100-80DL	LR LR	DL DL	Dibromochloromethane	10	Ü	<u> </u>	R	07 07	10	UG/L UG/L	DL
WG-	MW-100-9DL	LR	DL	Dibromochloromethane Dibromochloromethane	! <u>0</u> ↓ 10	U	U	Ŕ	07	10 ;	UG/L :	DL ~
WG	MW-100-10DL	LR	- <u>DL</u>	Dibromochloromethane	10	-	֓֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	- <u>R</u> -	0.7	10	ŪĠ/L	DĹ '
WG	MW-101-124DL	LR	DL	Dibromochloromethane	40	U	U	R	28	40	UG/L	DL
WG	MW-101-109DL	LR	DL	Dibromochloromethane	40	U	<u>U</u>	R	28	40	UG/L	ĎĽ,
WG	MW-101-89DL	LR	DL	Dibromochloromethane	40	U	Ü	<u>R</u>	28	40	UG/L	DL
SO WG	MW-100-92 5DL MW-104-10DL	LR LR	DL DL	Ethylbenzene Ethylbenzene	570	U	U		57 0 22		UG/KG; UG/L	DL DL
-wG	: MW-97-8DL	LR	DL -	Ethylbenzene	2		-0 -1	R	0 24	$-\frac{2}{2}$	UG/L	DL
- wg	MW-97-80DL	LR	DL	Ethylbenzene	2-	-	-ŭ ,	'R'1	0 24	2 - 2 - 2	UG/L	DL
WG	MW-98-1DL	LR	DL	Ethylbenzene	041	DJ	J	R	0 24		UG/L	DL
WG	MW-98-2DL	LR	DL	Ethylbenzene	0 31	DJ	J	R	0 24	2	UG/L	DL
WG_	MW-98-5DL	LR	DL	Ethylbenzene	0 42	DJ	J	R	0 24	2	UG/L	DL
WG -	MW-94-1DL ,MW-94-2DL	LR LR	DL DL	Ethylbenzene Ethylbenzene	40	U	U U	R	44	40 40	UG/L UG/L	<u>DL</u> -
WG	MW-100-1DL	LR		Ethylbenzene Ethylbenzene	5				0 55	5	UG/L	DL
WG	MW-100-2DL	LR	DL !	Ethylbenzene	10	ΰ	υŢ	Ř	11	10	UG/L	DL
WG	MW-100-3DL	LR	DL	Ethylbenzene	10	_ <u>U</u>]	Ū	Ř	1 1	10	UG/L	DL
L WG	MW-100-4DL	LR	DL ,	Ethylbenzene	10	_ U [Ü	<u>R</u> _	11	10	UG/L	, OL
WG	MW-100-5DL MW-100-6DL	LR .	DL	Ethylbenzene	10	<mark>U</mark> -:	- Ü	R Ř	-11-	_ 10 _	UG/L,	. Dr .
' WG	INIAA- IOO-ODF	LR	DL	Ethylbenzene	_ 10 <u>_ j</u>		ָ ט יַ	- K	11	10	UG/L	DL

Attachment D - Data Rejected Through the Data Validation Process

Matri	Sample ID	Sample	LR Jype	Parameter	Lab	Lab Qual	Conc	Final	ĎĽ	《 (RL)	Units	DV Notes
95	11、15年度16、6				Kesult	Crual	Quai	-Cual	200	÷*'9'4	7,00	
WG	MW-100-7DL	LR -	<u>DL</u>	Ethylbenzene	10	<u>U</u> .	<u>U</u>	R	11	10	UG/L	DL
WG	MW-100-8DL MW-100-80DL	LR LR	DL	Ethylbenzene	10	U	Ü	R	11.	10	UG/L	DL
WG	MW-100-9DL	LR LR	DL	Ethylbenzene Ethylbenzene	10	U	U	R	11	10	UG/L UG/L	DL DL
WG	MW-100-10DL	LR	DL	Ethylbenzene	+- 10	Ü	-	R	11	10	UG/L	DL :
WG	MW-101-124DL	LR	DL	Ethylbenzenc	40	Ü	Ū	R	44	40	UG/L	DL
[_WG_	MW-101-109DL	LR_	DL	Ethylbenzene	40	U	U	R	44	40	UG/L	DL
WG SO	MW-101-89DL	LR	DL. DL	<u>Ethyfbenzene</u>	40	υ	U	R	44	_40	UG/L	DL
WG	MW-100-92 5DL MW-104-10DL	LR LR	DL	Methylene chloride Methylene chloride	1100	U	Ü	R	78	1100	UG/KG	DL
WG	MW-97-8DL	LR	DL	Methylene chloride	2	. U	U	R	0 12	2 2	UG/L	DL DL
WG	MW-97-80DL	LR	DL	Methylene chloride	2	<u> </u>	Ŭ	R	0 22	2	- UG/L	<u>D</u> L
WG	MW-98-1DL	LR	DL	Methylene chlonde	2	U	U	R	0 22	2	UG/L	DL
WG	MW-98-2DL	LR	DL	Methylene chlonde		U	Ū	R	0 22	2 ;	UG/L	DL]
WG_ WG	MW-98-5DL	LR	DL	Methylene chloride	2	U	<u>U</u>	R	0 22		<u>UG/L</u>	DL
WG	MW-94-1DL _ {	LR LR	DL DL	Methylene chlonde Methylene chlonde	40	<u>U</u>	Ü	R R	24	40	ŪĞ/L	DL
WG	MW-100-1DL	LR	DL	Methylene chloride	5	- - 0	Ü	R	03	40 5	UG/L UG/L	DL DL
WG	MW-100-2DL	LR	DL	Methylene chlonde	10	-ŭ	Ü	R	06	10	UG/L	DL
WG	MW-100-3DL	LR ,	DL	Methylene chloride	10	U	- - -	R	06	10	UG/L	<u>D</u> ī - 1
WG	MW-100-4DL	LR	DL	Methylene chlonde	10	U	U	R	06	10	UG/L	DL
WG	MW-100-5DL	LR	_ DL _ ‡	Methylene chlonde	10	<u> </u>	_ U	R	06	10	UG/L	DL
₩Ğ WĞ	MW-100-6DL /	LR LR	DL DL	Methylene chloride	10	<u>U</u>	Ũ	R	06	10	UG/L	DL
- wG	MW-100-7DL	LR ,	DL -	Methylene chlonde Methylene chlonde	10	U	Ü	- R	06 i	10	UG/L	DL
-wG	MW-100-80DL	LR-	ĎL	Methylene chloride	10 .	U	-5-	<u>R</u>	0.6	_10_ 10_	UG/L UG/L	DL DL
WG	MW-100-9DL	LR	DL	Methylene chlonde	10	- Ŭ †	ŭ	R	06 ;	10	UG/L	DL -
wg	MW-100-10DL	LR	ĎL 🕌	Methylene chlonde	10	Ü	Ū	R	06	10	ÜĞ/L	DL ;
WG	MW-101-124DL	LR	DL !	Methylene chloride	40 ,		U	R	24.	40 .	UG/L	DĹ
WG	MW-101-109DL	LR	_ DL	Methylene chlonde	40	Ü	U	R	24	40	UG/L	DL
WG SO	MW-101-89DL MW-100-92 5DL	LR L	DL DL	Methylene chloride	40	Ų	U	R	<u>24</u> ;	40 ,	UG/L	DL
wG	MW-104-10DL	LR.	- DL	Tetrachloroethene Tetrachloroethene	570	U	- U	R R	41 0 24 ±	570	UG/KG_ UG/L_	DL ;
WG	MW-97-8DL	LR	DL	Tetrachloroethene	$-\frac{2}{2}$	·Ŭi	ü		0 24	2	UG/L	DL
WG	MW-97-80DL	ĪR 📑	DL +	Tetrachloroethene	2	Ü	-ŭ l		0 24	2	UG/L	DL
WG	MW-98-1DL	LR	DL	Tetrachloroethene	51	_ D	= 1	R	0 24	2	ÚG/L ~	DL
WG	MW-98-2DL	LR	. DL	Tetrachloroethene	5.5	D	= 1		0 24	2	UG/L	DL
WG	MW-98-5DL MW-94-1DL	LR	DL OL	Tetrachloroethene	15	D1	- J		0 24	2 1	UG/L	DL
wg	MW-94-2DL	- LR -	-DL	Tetrachloroethene Tetrachloroethene	40 -	U	U	R	48	40	UG/L UG/L	DL
WG	MW-100-1DL	LR -	-DL	Tetrachloroethene	13	D	= +	R	06	1 _	UG/L	DL
so	MW-100-92 5DL	LR	ĎĽ ;	Toluene	570	<u>Ū</u>	U	R	52		JG/KG	DL
WG	MW-104-10DL	LR	DL	Toluene	2 [_Ū	U	R	0 24		UG/L	DL
WG	MW-97-8DL	LR.	ĎL	Toluene	2	Ü	U		0 22		UG/L	DL
i⊢ WG	MW-97-80DL	<u>LR</u>	DL	Toluene	2	. <u>U</u> . ‡	U		0 22	2	UG/L	DL j
WG W	MW-98-1DL MW-98-2DL	LR LR	DL :	Toluene	0 27	_DJ	<u></u>		0 22	. <i>–</i>	UG/L	Dr
-WG	MW-98-5DL	LR :	DL -	Toluene Toluene	$\frac{2}{063} +$	- <u>m</u> -	Ŋ		0 22	- <u>2</u>	ŪĠ/L UG/L	DL DL
WG	MW-94-1DL	LR ;	DL	Toluene	40 ;	- Ŭ	U		48		ŪĞ/L	DL
WG	MW-94-2DL	LR	DL ,	Toluene	40	- U -	Ü		48	4 -	UG/L	- DL
WG	MW-100-1DL	LR	DL	Toluene	5	_U	U		06		ŪĞ/L	DL
WG	MW-100-2DL	LR_	DL ;	Toluene	10	U	U	R	12		UG/L ;	DL
WG :	MW-100-3DL	LR ;	DL	Toluene	10	U	<u>. U</u>		12		UG/L	DL
WG WG	MW-100-4DL MW-100-5DL	LR .	DL	Toluene Toluene	10	- Tir- t-	U		12		UG/L	DL
wg	MW-100-6DL	LR ;	- <u>Pr</u> - 1 -	Toluene	10	- <u>U</u> +	U		12		UG/L UG/L	DL
WG	MW-100-7DL	LR -	DL -	Toluene	10	- U -	U		12		UG/L	DL DL
WG	MW-100-8DL	LR	DL +	Toluene	10	u	U -		12		UG/L	DL
WG	MW-100-80DL	LR	DL T	Toluene	_10	U	U	R	12		UG/L	DL
WG_	MW-100-9DL	- LR +-	DL	Toluene	_10	U	Ü		12		UĞ/L	DL T
WG WG	MW-100-10DL	LR	. DL	Toluene	~ 10 - 1		U.		12		UG/L	DL
WG H	MW-101-124DL 3 MW-101-109DL 3	LR :	Dr , .	Toluene Toluene	40	U	U		48		UG/L	<u>DL</u> ;
wG	MW-101-89DL	LR	DL ::-	Toluene	40	U	U		48 48	_ ;	UG/L UG/L	DL '
so	MW-100-92 5DL	LR	DË	trans-1,2-Dichloroethene	570	<u>u</u>	<u>ŭ</u> †		_4_		ig/kg	DL J

		Sample ID	Sample Type	LR Type	Parameter	Lab Result	(Lab Qual	Lab Conc Qual	Final Qual	DL	RL	Units	DV Notes
	WG	MW-104-10DL	LR	DL.	trans-1,2-Dichloroethene	2	Sinday in	U.	R	0 22	2	k\$t∂⊅≪ UG/L	DL
	WG	MW-97-8DL	ĹŔ	DL	trans-1,2-Dichloroethene		Ü	Ū	R	03	2 -	UG/L	DL
	WG	MW-97-80DL	ĹR	DL	trans-1,2-Dichloroethene	2	U	U	R	03		UG/L	DL
	WG	MW-98-1DL	LR	DL	trans-1,2-Dichloroethene	2	U	U	R	0.3	$-\frac{2}{2}$	UG/L	DL
	WG	MW-98-2DL	LR	DL	trans-1,2-Dichloroethene	2	Ü	U	R	03	2	UG/L	DL "
١	WG	MW-98-5DL	LR	DL	trans-1,2-Dichloroethene	2	U	Ü	R	03	2	UG/L	DL
ļ	WG	MW-94-1DL	LLR	DL	trans-1,2-Dichloroethene	40	U	U	R	44	40	UG/L	DL
ŀ	WG WG	MW-94-2DL MW-100-1DL	LR	DL	trans-1,2-Dichloroethene	40	Ú	U	R	44	40	UG/L	DL
-	WG	MW-100-1DL	LR LR	DL DL	trans-1,2-Dichloroethene trans-1,2-Dichloroethene	5 10	U	U	R	0 55	5	UG/L	DL
-	wg.	MW-100-2DL	LR	DL	trans-1,2-Dichloroethene	10	U	U ~	R ;	11	10 10	UG/L UG/L	DL DL
	WG	MW-100-4DL	LR	DL	trans-1,2-Dichloroethene	10	U	- U	R -	111	10	UĞ/L	DL
ľ	WG	MW-100-5DL	' LR	DL	trans-1,2-Dichloroethene	10	- <u><u></u><u></u></u>	Ü	R	1.1	10	UG/L	DL
- [WG	MW-100-6DL	LR	DL	trans-1,2-Dichloroethene	10	<u>v</u>	<u>ŭ</u>	∵ Ř :	11	10	UG/L	DL
	WG	MW-100-7DL	LR	DL	trans-1,2-Dichloroethene	10	U	Ū-			10	UG/L	DL
	WG	MW-100-8DL	LR _	DL	trans-1,2-Dichloroethene	10	U	U	R	11	10	UG/L	DL
	WG	MW-100-80DL	LR	DL	trans-1,2-Dichloroethene	10	Ú	υ	R	<u> </u>	10	ÜG/L	DL
ļ	WG	MW-100-9DL	LR	DL	trans-1,2-Dichloroethene	10	U	U	R	11	10	UG/L	DL
-	WG	MW-100-10DL	LR	DL	trans-1,2-Dichloroethene	10	U	U_	R	11	10	UG/L	DL
- }-	WG	MW-101-124DL	LR	DL	trans-1,2-Dichloroethene	40	Ų	U	R	4.4	40	UG/L	DL
ŀ	WG WG	MW-101-109DL MW-101-89DL	LR	DL _	trans-1,2-Dichloroethene	40	. U	<u>U</u>	R	44	40	UG/L	DL
ŀ	SO	MW-100-92.5DL	LR LR	DL	trans-1,2-Dichloroethene trans-1,3-Dichloropropene	40 570	<u>U</u>	U	R 	44	_40 570	UG/L	DL
ŀ	WG	MW-104-10DL	LR	DL	trans-1,3-Dichloropropene	2	Ü	U	- R †	0 14	2	UG/KG UG/L	DL
-	WG	MW-97-8DL	LR I	DL	trans-1,3-Dichloropropene	2-1	U	Ü		0 26		UG/L	ביים ביים
	WG	MW-97-80DL	LR	DL	trans-1,3-Dichloropropene	2	-ŭ-	<u>ŏ</u>	<u>R</u>	0 26	2	UG/L	DL -
Ì	WG	MW-98-1DL	LR	DL	trans-1,3-Dichloropropene	2	Ü	Ü	R	0 26	2	UG/L	DL
ſ	_WG_	MW-98-2DL	LR :	DL	trans-1,3-Dichloropropene	$\bar{\mathbf{z}}$ i	- U	U	∵R ¹	0 26	2	UG/L	DL
[_wg	MW-98-5DL	LR	DL	trans-1,3-Dichloropropene	2	บ	u-;	ĪŔ.	0 26	2	UG/L	DL1
ļ	WG	MW-94-1DL	֓֞֞֞֞֞֞֞֞֞֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓	DL	trans-1,3-Dichloropropene	40	U	U	R	28	40	UG/L	DL ,
	WG	_MW-94-2DL	LR	DL	trans-1,3-Dichloropropene	40	U	U	R	28	40	UG/L	DL
	WG .	MW-100-1DL	LR I	DL	trans-1,3-Dichloropropene	5	U	Ú		0 35	5	UG/L	DL
-	WG WG	MW-100-2DL MW-100-3DL	LR LR	DL DL	trans-1,3-Dichloropropene trans-1,3-Dichloropropene	10	U	U	_R Ř į́	07	10	UGAL	DL
╁	WG	MW-100-4DL	LR	DL	trans-1,3-Dichloropropene	10	U	U	R	07	10	UG/L	DL DL
ŀ	wg	MW-100-5DL	LR	DL -	trans-1,3-Dichloropropene	10	-	👸	R †	07	-10-	UG/L	DL }
ı	WG !	MW-100-6DL)	LR	DL	trans-1,3-Dichloropropene	10	- Ŭ	· - Ŭ 🕂	R	- 0 7	10	ÚĞ/L	DL
ľ	WG :	MW-100-7DL ;	LR 1	DL	trans-1,3-Dichloropropene	10	Ū	Ū ¦	Ř	07	10	UG/L	DL
	WG	MW-100-8DL	LR	DL	trans-1,3-Dichloropropene	10	U	-Ū	R	0.7	10	UG/L	DL ;
	WG !	MW-100-80DL	LR	DL	trans-1,3-Dichloropropene	10	U	U	R	07	10	UG/L	DL
╁	WG	MW-100-9DL	LR [DL	trans-1,3-Dichloropropene	10	U	U	R	07	10	UG/L	DL
-	WG	MW-100-10DL	LR	DL	trans-1,3-Dichloropropene	10	U	Ū	R	07	10	UG/L	DL
┝	WG WG	MW-101-124DL	LR	DL	trans-1,3-Dichloropropene	40	<u>U</u>	U	R	28	40	UG/L	DL
-	WG	MW-101-109DL MW-101-89DL	LR LR	DL	trans-1,3-Dichloropropene	40	Ü	U	R	28	40	UG/L	DL
-	WG	MW-97-8DL ,	LR LR	DL DL	trans-1,3-Dichloropropene Trichloroethene	40	U	U		28	40	UG/L UG/L	DL
-	wg	MW-97-80DL	- ia	- DL	Inchloroethene !	2 2	- 🖰 🕂	$\frac{0}{0}$	<u>R</u> <u>+</u>	0 24	2	UG/L UG/L	DL DL
ŀ	WG	MW-98-1DL	LR	 †	Trichloroethene	0.86	La	- j -		0 24	2	UG/L	DL
T	WG	MW-98-2DL	LR	DL	Trichloroethene	0.81	DJ	J	- <u>R</u>	0 24	2	UG/L	DL
	WG	MW-98-5DL	LR	DL	Trichloroethene	043	<u> </u>		R	0 24	2	UG/L	DL
	WG	MW-94-1DL	TLR T	DL	Trichloroethene	40	U	Ū	R	5 2	40	UG/L	DL
	WG	MW-94-2DL !	LR [DL	Trichloroethene	40	U	U	Ŕ	52	40	UG/L	DL
L	WG	MW-101-124DL	LR .	_DL	Trichloroethene	40	U	Ü	R	52	40	UG/L	DL
-	WG	MW-101-109DL	LR]	_DL	Tnchloroethene	40	U	U	R	52	40	UG/L	DL
-	WG SO	MW-101-89DL	LR	DL	Trichloroethene	40	U	U	_ <u>R</u> _i.	52	40	UG/L	DL
F	WG	MW-100-92.5DL MW-104-10DL	LR LR	DL DL	Vinyl chlonde Vinyl chlonde	570	U		R			UG/KG	DL
\vdash	WG	MW-97-8DL	LR LR	DL -	Vinyl chlonde'	2 2 2 2 2 2 2	Ü	U		0 26 0 26 i	2	UG/L UG/L	<u>DL</u> -
-	WG	MW-97-80DL		DL	Vinyl chlonde	- 5	0	- U		0 26	2	UG/L	DL -
-	WG	MW-98-1DL	LR T	DL +	Vinyl chloride		Ü	<u>u</u> -†		0 26	2 1	UG/L	DL
1	WG	MW-98-2DL	LR I	DL ,	Vinyl chlonde	2	-ŭ -	ÿ ∤.		0 26 ;		UG/L	DL
	WG	MW-98-5DL	LR T	DL ,	Vinyl chlonde	2	-Ū			0 26		UG/L	DL
<u> </u>	WG	MW-94-1DL	LR ;	DL	Vinyl chlonde	40	U	Ū	R	52		UG/L	DL
ļ.,	WG	MW-94-2DL	LR I	DL T	Vinyl chlonde	40	_ <u>U</u>		R	5 2 t	40	UG/L	ĎL]
L.	WG	MW-100-1DL	LR	DL	Vinyl chlonde	. 5	U	_u_T	R	0 65	_5_}	UG/L	DL)

Attachment D - Data Rejected Through the Data Validation Process

Matrix	Sample ID	Sample	LR Type	Parameter Parameter	Lab Result	Lab Qual	Lab Conc	Final	P. C.			DV Notes
S. P. Car	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	A.A.A.	1			2.23	Qual:	التعقيدا	تغلظنوا	200	100	
WG	MW-100-2DL	LR	DL	Vinyl chlonde	10	U	U	<u>R</u> _	13	10	UG/L	<u>DL</u>
WG	MW-100-3DL	LR	DL	Vinyl chlonde	10	U	<u> </u>	R	13	10	UG/L	DL ;
WG	MW-100-4DL	LR	DL	Vinyl chlonde	10	U	U	R	13	10	UG/L	DL }
WG	MW-100-5DL	LR	DŁ	Vinyl chlonde	10	U	U	R	13	10	UG/L	DL
WG	MW-100-6DL	LR	DL	Vinyl chloride	10	U	υ	R	13	10	UG/L	DL ,
WG	MW-100-7DL	LR	DL	Vinyl chlonde	10	U	U	R	13	10	UG/L	DL
WG	MW-100-8DL	LR	DL	Vinyl chloride	10	U	U	R	13	10	UG/L	DL ¦
WG	MW-100-80DL	ĹR	DL	Vinyl chlonde	10	U	U	R	13	10	UG/L	DL
WG	MW-100-9DL	ĹR	DL ,	Vinyl chlonde	10	U	U	R	13	10	UG/L	DL
WG	MW-100-10DL	LR	DL	Vinyl chlonde	10	U	U	R	13	10	UG/L	DL :
WG	MW-101-124DL	LR	DL '	Vinyl chlonde	40	U	U	R	5 2	40	UG/L	DL i
WG	MW-101-109DL	LR	DL	Vinyl chloride	40	υ	U	R	5 2	40	UG/L	DL)
WG	MW-101-89DL	LR	DL	Vinyl chloride	40	U	U	R	5 2	40	UG/L	DL ,

80	र 'ेद्र	THE STATE OF		187.24 Barrio		45.00 p	4.3.4	المراجع المراجع	18 cm	Sec.	1,620	1.5(.)7	
6	全众					Lab	Lab	Field	Field	23	(na ez)	1	
	ļatrix	Analytical Method	Prep	Sample ID.	Parameter.	Result	Qual	*Laba	×i ab γ	DL.	ŀΩ.	Units	AS RPD
		学证的证明	W. 78	4,345.25	10.00000000000000000000000000000000000	1,344	4,000	Result	Qual		. 3	10.00	
7	277	31 G. A. A.	(1)38 27-578	of March March	心理如此者 有一切。	125/90/201	27.450	/中线5/35	B 4447.2	X.2.	-41	UG/L	-100 0
\vdash	WG WG	SW8260B	SW5030	MW-100-8	1,1,1-Trichloroethane 1,1,2,2-Tetrachloroethane	0 23	J	0 19	J	0 12	1	UG/L	190
\vdash	WG	SW8260B SW8260B	SW5030 SW5030	MW-100-8 MW-100-8	1,1,2,2-Tetracriloroethane	1	U	1	Ü	0 12	1	UG/L	-100 0
\vdash	WG	SW8260B	SW5030	MW-100-8	1,1-Dichloroethane	 -	Ŭ	1	Ü	0 12	1	UG/L	-100 0
\vdash	WG	\$W8260B	SW5030	MW-100-8	1,1-Dichloroethene	0 21	Ĵ	1	U	0.11	1	UG/L	200 0
	WG	SW8260B	SW5030	MW-100-8	1,2-Dichloroethane	0 17	J	0 15	7	0 11	1	UG/L	12 5
	WG	SW8260B	SW5030	MW-100-8	1,2-Dichloropropane	1	U	1	U	0 11	1	UG/L	-100 0
	WG	SW8260B	SW5030	MW-100-8	Benzene	1	U	1	U	0 12	1	UG/L	-100 0
<u> </u>	WG	SW8260B	SW5030	MW-100-8	Bromodichloromethane	1	U	1	U	0 08	1	UG/L	-100 0
-	WG WG	SW8260B SW8260B	SW5030 SW5030	MW-100-8 MW-100-8	Bromoform	1	U U	1	U	0 06 0 18	1	UG/L UG/L	-100 0 -100 0
\vdash	WG	SW8260B	SW5030	MW-100-8	Bromomethane Carbon tetrachlonde	1	U		U	01	+	UG/L	-100 0
\vdash	WG	SW8260B	SW5030	MW-100-8	Chlorobenzene	1	Ü	1	U	01	1	UG/L	-100 0
\vdash	WG	SW8260B	SW5030	MW-100-8	Chloroethane	1	Ü	1	Ü	0 11	1	UG/L	-100 0
	WG	SW8260B	SW5030	MW-100-8	Chloroform	1	U	1	Ü	0 12	1	UG/L	-100 0
	WG	SW8260B	SW5030	MW-100-8	Chloromethane	1	U	1	U	0 13	1	UG/L	-100 0
	WG	SW8260B	SW5030	MW-100-8	cis-1,3-Dichloropropene	1	U	1	U	0 07	1	ÜG/L	-100 0
	WG	SW8260B	SW5030	MW-100-8	Dibromochloromethane	1	U	1	U	0 07	_1	UG/L	-100 0
<u> </u>	WG	SW8260B	SW5030	MW-100-8	Ethylbenzene	1	U	1	Ü	0 11	1	UG/L	-100 0
<u> </u>	WG WG	SW8260B SW8260B	SW5030 SW5030	MW-100-8 MW-100-8	Methylene chloride	1	U	1	Ü	0.06	1	UG/L UG/L	-100 0 -100 0
}_	WG	SW8260B SW8260B	SW5030	MW-100-8	Toluene trans-1,2-Dichloroethene	0 13	J	0 17	J	0.12		UG/L	26 7
\vdash	WG	SW8260B	SW5030	MW-100-8	trans-1,3-Dichloropropene	1	Ü	1	Ü	0 07	- 	UG/L	-100 0
\vdash	WG	SW8260B	SW5030	MW-100-8	Vinyl chloride	i	Ŭ	1	Ŭ	0 13	1	UG/L	-100 0
\vdash	WG	SW8260B	SW5030	MW-100-8	Tetrachloroethene	56	E	44	-	0 12	1	UG/L	## 10200.0 J.
\vdash	WG	SW8260B	SW5030	MW-100-8	Trichloroethene	80	E	68	=	0 13	1	UG/L	7 200.0 V
	SO	SW8260B	SW5035	MW-101-94	1,1,1-Trichloroethane	63	J	69	U	0 78	63	UG/KG	-100 0
	SO	SW8260B	SW5035	MW-101-94	1,1,2,2-Tetrachloroethane	6.3	U	69	U	0 69	63	UG/KG	-100 0
	SO	SW8260B	SW5035	MW-101-94	1,1,2-Tnchloroethane	63	U	69	U	0 68	63	UG/KG	-100.0
Ψ	so	SW8260B	SW5035	MW-101-94	1,1-Dichloroethane	6.3	U	69 69	U	0 73 0 63	63	UG/KG UG/KG	-100 0 -100 0
\vdash	so so	SW8260B SW8260B	SW5035 SW5035	MW-101-94 MW-101-94	1,1-Dichloroethene 1,2-Dichloroethane	63	U	3	J	0 63	63	UG/KG	200 0
\vdash	so	SW8260B	SW5035	MW-101-94	1,2-Dichloropropane	63	Ü	69	Ü	0 77	63	UG/KG	-100.0
\vdash	so	SW8260B	SW5035	MW-101-94	Benzene	63	Ŭ	69	Ü	0 64	63	UG/KG	-100 0
\vdash	SO	SW8260B	SW5035	MW-101-94	Bromodichloromethane	63	U	69	U	0 69	63	UG/KG	-100 0
	SO	SW8260B	SW5035	MW-101-94	Bromoform	0 91	J	69	U	0.62	63	UG/KG	200 0
	so	SW8260B	SW5035	MW-101-94	Bromomethane	63	U	69	U	0 87	63	UG/KG	-100 0
\perp	SO	SW8260B	SW5035	MW-101-94	Carbon tetrachlonde	63	U	69	U	0 84	63	UG/KG	-100 0
\vdash	so	SW8260B	SW5035	MW-101-94	Chlorobenzene	63	U	69				UG/KG	-100 0
\vdash	SO SO	SW8260B SW8260B	SW5035 SW5035	MW-101-94 MW-101-94	Chloroethane Chloroform	63 63	- -	69 69	U			UG/KG UG/KG	-100 0 -100 0
\vdash	SO	SW8260B	SW5035	MW-101-94	Chloromethane	63	Ü	69	υ			UG/KG	-100 0
\vdash	so	SW8260B	SW5035	MW-101-94	cis-1,3-Dichloropropene	63	Ü	69	Ü			UG/KG	-100 0
	SO	SW8260B	SW5035	MW-101-94	Dibromochloromethane	63	Ü	69	Ū			UG/KG	-100 0
	SO	SW8260B	SW5035	MW-101-94	Ethylbenzene	63	U	69	U	09	63	UG/KG	-100 0
	so	SW8260B	SW5035	MW-101-94	Methylene chloride	63	U	69	U			UG/KG	-100 0
Ĺ	SO	SW8260B	SW5035	MW-101-94	Tetrachloroethene	63	U	69	U	0 92	-	UG/KG	-100 0
<u> </u>	so	SW8260B	SW5035	MW-101-94	Toluene	63	υ:	69	υJ	0.82		UG/KG	-100 0
\vdash	SO.	SW8260B	SW5035	MW-101-94	trans-1,2-Dichloroethene	63 63	C C	69 69	U			UG/KG UG/KG	-100 0 -100 0
\vdash	SO SO	SW8260B SW8260B	SW5035 SW5035	MW-101-94 MW-101-94	trans-1,3-Dichloropropene Trichloroethene	63	Ü	69	Ü			UG/KG	-100 0
	SO	SW8260B	SW5035	MW-101-94	Vinyl chlonde	63	Ü	69	Ŭ	0 64		UG/KG	-100 0
	WG	SW8260B	SW5030	MW-102-8	1,1,1-Trichloroethane	1	Ŭ	1	Ŭ	0 12	1	UG/L	-100 0
	WG	SW8260B	SW5030	MW-102-8	1,1,2,2-Tetrachloroethane	1	U	1	Ū	0 09	1	UG/L	-100 0
	WG	SW82608	SW5030	MW-102-8	1,1,2-Tnchloroethane	1	U	1	U	0 12	1	UG/L	-100 0
_	WG	SW8260B	SW5030	MW-102-8	1,1-Dichloroethane	1	U	1	U	0 12	1	UG/L	-100 0
	WG	SW8260B	SW5030	MW-102-8	1,1-Dichloroethene	1	U	1	U	0 11	1	UG/L	-100 0
	WG WG	SW8260B	SW5030	MW-102-8	1,2-Dichloroethane	1	U	1	Ü	0 11	1	UG/L UG/L	-100 0 -100 0
	WG WG	SW8260B SW8260B	SW5030 SW5030	MW-102-8 MW-102-8	1,2-Dichloropropane Benzene	1	U	1	0	0 12	1	ŲG/L	-100 0
_	WG	SW8260B	SW5030	MW-102-8	Bromodichloromethane	1	Ü	1	—ऍ─	0 08	1	UG/L	-100 0
_	WG	SW8260B	SW5030	MW-102-8	Bromoform	1	Ū	1	Ŭ	0 06	1	UG/L	100 0
_	WG	SW8260B	SW5030	MW-102-8	Bromomethane	1	U	1	U	0 18	1	UG/L	-100 0

WG	SW8260B	T sw5030	MW-102-8	Carbon tetrachlonde	1 1	ΤŪ	1	Ιυ	0 1	1 1	UG/L	-100 0
WG	SW8260B		MW-102-8	Chlorobenzene	 	Ιΰ	+ +	1 0	0 1	1 ;	UG/L	-100 0
WG	SW8260B		MW-102-8	Chloroethane	† i	ΤŬ	1	1 - ŏ -	0 1	_	UG/L	-100 0
WG	SW8260B		MW-102-8	Chloroform	1	ΙŬ	1 1	T U	0 12		UGIL	-100 0
WG	SW8260B		MW-102-8	Chloromethane	1	Ü	1	U	0 13		UG/L	-100 0
WG	SW8260B		MW-102-8	cis-1,3-Dichloropropene	1	U	1	IJ	0.07	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-102-8	Dibromochloromethane	1	U	1	U	0.07		UG/L	-100 0
WG	SW8260B		MW-102-8	Ethylbenzene	1 1	U	1	Ü	0 11		UG/L	-100 0
WG	SW8260B	SW5030	MW-102-8	Methylene chloride	1	U	1 1	U	0.06		UG/L	-100 0
WG	SW8260B	SW5030	MW-102-8	Tetrachloroethene	1 1	U	1	U	0 12		UG/L	-100 0
WG	SW8260B SW8260B	SW5030	MW-102-8	Toluene	1 1	U	1 1	U	0 12		UG/L	-100 0
WG	SW8260B	SW5030 SW5030	MW-102-8 MW-102-8	trans-1,2-Dichloroethene trans-1,3-Dichloropropene	1 1	U	1 1	U	0 11		UG/L	-100 0
WG	SW8260B	SW5030	MW-102-8	Trichloroethene	 	1 0	1 1	Ŋ	0 07		UG/L UG/L	-100 0 -100 0
WG	SW8260B	SW5030	MW-102-8	Vinyl chlonde	+ +	U	1 1	1 0	0 13		UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	1,1,1-Trichloroethane	1 1	ΙÜ	 	 	0 14		UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	1,1,2,2-Telrachloroethane	1 1	1 ŭ	1 1	lυ	0 08		UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	1,1,2-Trichloroethane	1	Ι υ	 i	υ	0 11		UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	1,1-Dichloroethane	16	 - <u></u>	17	=	0 14		UG/L	6 1
WG	SW8260B	SW5030	MW-103-5	1,1-Dichloroethene	15	=	17	† <u>-</u>	0 23		UG/L	125
WG	SW8260B	SW5030	MW-103-5	1,2-Dichloroethane	0 16	J	0 16	J	01	1	UG/L	00
WG	SW8260B	SW5030	MW-103-5	1,2-Dichloropropane	1	U	1	U	0 08	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	Benzene	1	U	1	U	0 14	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	Bromodichloromethane	1	U	1	U	0 13	1	UG/L	-100 0
_WG	SW82608	SW5030	MW-103-5	Bromoform	1_1_	U	1	U	0 12		UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	Bromomethane	1	U	1	U	0 14	-	UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	Carbon tetrachlonde	1	U	1	U	0 14	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	Chlorobenzene	1 1	U	1 1	U	01	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	Chloroethane	1	U	1	U	0 14	1	UG/L	-100 0
WG WG	SW8260B	SW5030	MW-103-5	Chloroform	15	=	16	=	0 14	1	UG/L	6.5
WG	SW8260B SW8260B	SW5030 SW5030	MW-103-5 MW-103-5	Chloromethane	1	U	1 1	U	0 17	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	cis-1,3-Dichloropropene Dibromochloromethane	 	U	 - 	U	0 11	1	UG/L UG/L	-100 0 -100 0
WG	SW8260B	SW5030	MW-103-5	Ethylbenzene	0 15	J	0 19	J	0 12	1	UG/L	23 5
WG	SW8260B	SW5030	MW-103-5	Methylene chlonde	1	Ŭ	1	υ	0 11	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	Tetrachloroethene	1	Ü	1	υ	0 12	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	Toluene	1	Ū	1	Ū	0 11	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	trans-1,2-Dichloroethene	1	U	1	υ	0 15	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	trans-1,3-Dichloropropene	1	U	1	U	0 13	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-103-5	Trichtoroethene	44	<u>-</u>	47	=	0 12	1	UG/L	66
WG	SW8260B	SW5030	MW-103-5	Vinyl chlonde	1	U	1	U	0 13	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	1,1,1-Trichloroethane	1	U	1	U	0 12	1	UG/L	-100 0
WG WG	SW8260B	SW5030	MW-104-5	1,1,2,2-Tetrachloroethane	1	U	1	U	0 09	1	UG/L	-100 0
WG	SW8260B SW8260B	SW5030 SW5030	MW-104-5 MW-104-5	1,1,2-Trichloroethane 1,1-Dichloroethane	0 37	J	0.24	J	0 12		UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	1,1-Dichloroethene	0 48	J	0 21	1	0 12	1	UG/L UG/L	55 2 95 4
WG	SW8260B	SW5030	MW-104-5	1,2-Dichloroethane	1	U	1	n 1	0 11	+	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	1,2-Dichloropropane	1	Ü	1	Ŭ	0 11	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	Benzene	1	Ü	1	Ü	0.12	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	Bromodichloromethane	1	U	1	Ū	0 08	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	Bromoform	1	U	1	Ü	0 06	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	Bromomethane	1	U	1	U	0 18	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	Carbon tetrachlonde	1	U	1	U	01	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	Chlorobenzene	1	U	1	U	01	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	Chloroethane	1	U	1	Ü	0 11	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	Chloromethane	1	: С	1	υ	0 13	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	cis-1,3-Dichloropropene	1	U	1	U	0 07	1	UG/L	-100 0
WG WG	SW8260B SW8260B	SW5030 SW5030	MW-104-5 MW-104-5	Dibromochloromethane Ethydhonagas	1 0.55	Ü	1 0.62	U	0 07	-1-	UG/L	-100 0
WG	SW8260B SW8260B	SW5030 SW5030	MW-104-5 MW-104-5	Ethylbenzene Methylene chlonde	0 55 0 21	J	0 62 0 26	<u>J</u>	0 11	1	UG/L UG/L	12 0 21 3
WG	SW8260B	SW5030	MW-104-5	Tetrachloroethene	1	Ü	1	U	0 12	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	Toluene		U	1	U	0 12	+	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	trans-1,2-Dichloroethene	- i -	Ü	1	Ü	0 12	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	trans-1,3-Dichloropropene	i 1	Ü	1	ű	0 07	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	Vinyl chloride	1	Ŭ	1	Ű	0 13	i	UG/L	-100 0
WG	SW8260B	SW5030	MW-104-5	Chloroform	10	=	63	=	0 12	1	UG/L	F 945.4 3.5%
WG	SW8260B	SW5030	MW-104-5	Trichloroethene	64	=	26	<u>-</u>	0 13	7	UG/L	K4584.4 251
so	SW8260B	SW5035	MW-104-63	1,1,1-Trichloroethane	56	U	63	Ū	0 56	56	UG/KG	-100 0

80	Lewissens	SW5035	1 ADM 404 62	1 1 2 2 Totachlassahassa	1 60	1	1 6 2		1 4	166	Lucaso	1 4000
SO	SW8260B		MW-104-63	1,1,2,2-Tetrachloroethane	56	U	63	<u> </u>	1 0 07	56		
so	SW8260B	SW5035	MW-104-63	1,1,2-Trichloroethane	56	l U	63	U	0 67	56	UG/KG	
so	SW8260B	SW5035	MW-104-63	1,1-Dichloroethane	56	U	6.3	U	0 67	56		
so	SW8260B	SW5035	MW-104-63	1,1-Dichloroethene	56	U	63	Ü	0 78			-100 0
SO	SW8260B	SW5035	MW-104-63	1,2-Dichloroethane	56	U	63	U	0 67	56	UG/KG	-100 0
SO SO	SW8260B	SW5035	MW-104-63	1,2-Dichloropropane	56	U	63	U	0 67		UG/KG	-100 0
so	SW8260B	SW5035	MW-104-63	Benzene	56	U	63	U	0 67	56	UG/KG	-100 0
SO	SW8260B	SW5035	MW-104-63	Bromodichloromethane	56	U	63	Įυ	0 56	56	UG/KG	-100 0
SO	SW8260B	SW5035	MW-104-63	Bromoform	0 88	J	1	J	0 56	56	UG/KG	128
SO	SW8260B	SW5035	MW-104-63	Bromomethane	11	U	13	ÜÜ	12	11	UG/KG	-100 0
SO	SW8260B	SW5035	MW-104-63	Carbon tetrachlonde	56	U	63	U	0 56	56	UG/KG	-100 0
so	SW8260B	SW5035	MW-104-63	Chlorobenzene	56	U	63	U	0 67	56	UG/KG	-100 0
so	SW8260B	SW5035	MW-104-63	Chloroethane	11	U	13	U	111	11	UG/KG	-100 0
so	SW8260B	SW5035	MW-104-63	Chloroform	56	Ū	63	Ū	0.78		UG/KG	-100 0
so	SW8260B	SW5035	MW-104-63	Chloromethane	11	Ū	13	Ŭ	0 67	11	UG/KG	-100 0
so	SW8260B	SW5035	MW-104-63	cis-1,3-Dichloropropene	56	Ū	63	Ū	0 78		UG/KG	-100 0
so	SW8260B	SW5035	MW-104-63	Dibromochloromethane	56	Ü	63	Ŭ	0 56		UG/KG	-100 0
so	SW8260B	SW5035	MW-104-63	Ethylbenzene	56	Ü	63	Ü	0 56	56	UG/KG	-100 0
so	SW8260B	SW5035	MW-104-63	Methylene chlonde	56	ϋ	63	- ŭ -	0 9	56	UG/KG	-100 0
so	SW8260B	SW5035	MW-104-63	Tetrachloroethene	56	Ü	63	U	0 67	56	UG/KG	-100 0
so	SW8260B	SW5035	MW-104-63		56	U	63	Ü				
- <u>30</u>	SW8260B			Toluene	1				0 78	56	UG/KG	-100 0
		SW5035	MW-104-63	trans-1,2-Dichloroethene	56	U	63	U	0 67	56	UG/KG	-100 0
SO	SW8260B	SW5035	MW-104-63	trans-1,3-Dichloropropene	56	U	63	U	0 67	56	UG/KG	-100 0
SO	SW8260B	SW5035	MW-104-63	Trichloroethene	56	U	63	Ų	0 67	56	UG/KG	-100 0
SO	SW8260B	SW5035	MW-104-63	Vinyl chloride	11	U	13	U	0 78	11	UG/KG	-100 0
SO	SW8260B	SW5035	MW-88-78	1,1,1-Trichloroethane	5.5	U	5 5	כ	0 68		UG/KG	-100 0
SO	SW8260B	SW5035	MW-88-78	1,1,2,2-Tetrachloroethane	5 5	U	55	5	06	55	UG/KG	-100 0
SO	SW8260B	SW5035	MW-88-78	1,1,2-Trichloroethane	5.5	Ü	5.5	5	0.59	55	UG/KG	-100 0
SO	SW8260B	SW5035	MW-88-78	1,1-Dichloroethane	5 5	U	5.5	J	0 63	55	UG/KG	-100 0
SO	SW8260B	SW5035	MW-88-78	1,1-Dichloroethene	5.5	U	5 5	5	0 55	55	UG/KG	-100 0
SO	SW8260B	SW5035	MW-88-78	1,2-Dichloroethane	5.5	U	5.5	U	0 67	5.5	UG/KG	-100 0
so	SW8260B	SW5035	MW-88-78	1,2-Dichloropropane	5.5	U	5.5	Ū	0 67	5 5	UG/KG	-100 0
şo	SW8260B	SW5035	MW-88-78	Benzene	5.5	Ü	5.5	Ū	0 56	55	UG/KG	-100 0
so	SW8260B	SW5035	MW-88-78	Bromodichloromethane	5.5	Ü	5.5	Ū	06	55	UG/KG	-100 0
ISO	SW8260B	SW5035	MW-88-78	Bromoform	07	j	0.7	J	0.54	55	UG/KG	00
SO	SW8260B	SW5035	MW-88-78	Bromomethane	5.5	Ů	5.5	Ü	0 75	55	UG/KG	-100 0
so	SW8260B	SW5035	MW-88-78	Carbon tetrachlonde	13	Ĵ	12	- j -	0 73	55	UG/KG	80
so	SW8260B	SW5035	MW-88-78	Chlorobenzene	55	Ü	55	Ü	0 74	55	UG/KG	-100 0
SO	SW8260B	SW5035	MW-88-78	Chloroethane	55	Ŭ	55	U	0 51	55	UG/KG	
so	SW8260B	SW5035	MW-88-78	Chloroform	0 95	<u> </u>	09					-100 0
so	SW8260B	<u> </u>						J	0 72	55	UG/KG	54
so		SW5035	MW-88-78	Chloromethane	5.5	υ	5.5	U	0 71	5 5	UG/KG	-100 0
	SW8260B	SW5035	MW-88-78	cis-1,3-Dichloropropene	5.5	U	5.5	U	0 68	55	UG/KG	-100 0
SO	SW8260B	SW5035	MW-88-78	Dibromochloromethane	5.5	U	5.5	U	0 61	5 5	UG/KG	-100 0
SO	SW8260B		MW-88-78	Ethylbenzene	5 5	U	5 5	U			UG/KG	-100 0
SO	SW8260B	SW5035	MW-88-78	Methylene chloride	5.5	U	5.5	U	•		UG/KG	-100 0
so	SW8260B	SW5035	MW-88-78	Tetrachloroethene	9	=	8.4	=	0.8		UG/KG	69
SO	SW8260B	SW5035	MW-88-78	Toluene	0 89	J	0.75	J	0 71	55	UG/KG	17 1
so	SW8260B	SW5035	MW-88-78	trans-1,2-Dichloroethene	5 5	U	55	U	06	55	UG/KG	-100 0
SO	SW8260B	SW5035	MW-88-78	trans-1,3-Dichloropropene	5.5	U	5 5	U	0.81	55	UG/KG	-100 0
SO	SW8260B	SW5035	MW-88-78	Trichloroethene	5 5	Ü	55	U	0 74		UG/KG	-100 0
SO	SW8260B	SW5035	MW-88-78	Vinyl chlonde	5 5	U	5.5	Ū	0 56		UG/KG	-100 0
WG	SW8260B	SW5030	MW-99-10	1,1,1-Trichloroethane	1	U	1	Ū	0 12	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-99-10	1,1,2,2-Tetrachloroethane	1	Ü	1	Ŭ	0 09	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-99-10	1,1,2-Trichloroethane	1	- ŭ -	1	Ű	0 12	$\overrightarrow{1}$	UG/L	-100 0
WG	SW8260B	SW5030	MW-99-10	1,1-Dichloroethane	1	ŭ	+	- U -	0 12	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-99-10	1,1-Dichloroethene	1	Ü	1	- ŭ -	0 12	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-99-10	1,2-Dichloroethene	1	- U	1	U	0 11		UG/L	
WG	SW8260B	SW5030	MW-99-10		- ;	U U				-1-		-100 0
WG	SW8260B		$\overline{}$	1,2-Dichloropropane			1	U	0 11	1	UG/L	-100 0
		SW5030	MW-99-10	Benzene	1	_ <u>U</u>	1	U	0 12	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-99-10	Bromodichloromethane	- 1	U	1	U	0 08	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-99-10	Bromoform		U	1 1	U	0 06	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-99-10	Bromomethane	1	U	1	U	0 18	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-99-10	Carbon tetrachlonde	1	U	1	U	01	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-99-10	Chlorobenzene	1	U	1	U	01	1	UG/L	-100 0
WG	SW8260B	SW5030	MW 99-10	Chloroethane	1	U	1	U	0 11	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-99-10	Chloroform	0 14	j	0 13	J	0 12	1	UG/L	7.4
WG	SW8260B	SW5030	MW-99-10	Chloromethane	1	U	1	U	0 13	1	UG/L	-100 0
WG	SW8260B	SW5030	MW-99-10	as-1,3-Dichloropropene	1	U	1	U	0 07	1	UG/L	-100 0
_												

WG S	SW8260B 1	CMIEDOO	1									1
		SW5030	MW-99-10	Dibromochloromethane	1 1	U	1 1	U	0 07	1	UG/L	-100 0
WG S	SW8260B	SW5030	MW-99-10	Ethylbenzene	1	U	1 1	U	0 11	1	UG/L	-100 0
	SW8260B	SW5030	MW-99-10	Methylene chloride	1	Ų	1	U	0 06	1	UG/L	-100 0
	SW8260B	SW5030	MW-99-10	Tetrachloroethene	1	Ų	1	U	0 12	1	UG/L	-100 0
WG S	SW8260B	SW5030	MW-99-10	Toluene	1	U	1	U	0 12	1	UG/L	-100 0
	W8260B	SW5030	MW-99-10	trans-1,2-Dichloroethene	1	U	1	IJ	0 11	1	UG/L	-100 0
	W8260B	SW5030	MW-99-10	trans-1,3-Dichloropropene	1	U	1	ŊĴ	0 07	1	UG/L	-100 0
	W8260B	SW5030	MW-99-10	Trichloroethene	1	U	1	U	0 13	1	UG/L	-100.0
	W8260B	SW5030	MW-99-10	Vinyl chlonde	1	U	1	U	0 13	1	UG/L	-100 0
	W8260B	SW5030	MW-99-5	1,1,1-Trichloroethane	1	U	1	U	0 12	1	UG/L	-100 0
	W8260B	SW5030	MW-99-5	1,1,2,2-Tetrachloroethane	1	U	1	U	0 09	1.	UG/L	-100 0
	W8260B	SW5030	MW-99-5	1,1,2-Trichloroethane	1	U	1	_U	0 12	1	UG/L	-100 0
WG S	W8260B	SW5030	MW-99-5	1,1-Dichloroethane	1	U	1	U	0 12	1	UG/L	-100 0
	W8260B	SW5030	MW-99-5	1,1-Dichloroethene	1	U	1	_ U	0 11	1	UG/L	-100 0
WG S	W8260B	SW5030	MW-99-5	1,2-Dichloroethane	1	U	1	U	0 11	1	UG/L	-100 0
WG S	W8260B	SW5030	MW-99-5	1,2-Dichloropropane	1	U	1	υ	0 11	1	UG/L	-100 0
WG S	W8260B	SW5030	MW-99-5	Benzene	1	U	1	U	0 12	1	UG/L	-100 0
WG S	W8260B	SW5030	MW-99-5	Bromodichloromethane	1	U	1	Ü	0 08	1	UG/L	-100 0
WG S	W8260B	SW5030	MW-99-5	Bromoform	1	U	1	U	0 06	1	UG/L	-100 0
WG S	W8260B	SW5030	MW-99-5	Bromomethane	1	U	1	U	0 18	1	UG/L	-100 0
WG S	W8260B	SW5030	MW-99-5	Carbon tetrachlonde	1	U	1	U	01	1	UG/L	-100 0
WG SI	W8260B	SW5030	MW-99-5	Chlorobenzene	1	υ	1	Ü	0 1	1	UG/L	-100 0
WG SI	W8260B	SW5030	MW-99-5	Chloroethane	1	Ü	1	U	0 11	1	UG/L	-100 0
WG SI	W8260B	SW5030	MW-99-5	Chloroform	0 15	J	0 14	J	0 12	1	UG/L	69
WG SI	W8260B	SW5030	MW-99-5	Chloromethane	1	U	1	υ	0 13	1	UG/L	-100 0
WG S	W8260B	SW5030	MW-99-5	cis-1,3-Dichloropropene	1	U	1	U	0 07	1	UG/L	-100 0
WG S	W8260B	SW5030	MW-99-5	Dibromochloromethane	1	U	1	٦	0 07	1	UG/L	-100 0
WG SV	W8260B	SW5030	MW-99-5	Ethylbenzene	1	U	1	U	0 11	1	UG/L	-100.0
	W8260B	SW5030	MW-99-5	Methylene chloride	1	U	1	U	0 06	1	UG/L	-100 0
WG SV	W8260B	SW5030	MW-99-5	Tetrachloroethene	1	U	1	U	0 12	1	UG/L	-100 0
	W8260B	SW5030	MW-99-5	Toluene	_ 1	U	1	U	0 12	1	UG/L	-100 0
	W8260B	SW5030	MW-99-5	trans-1,2-Dichloroethene	1	U	1	υ	0 11	1	UG/L	-100 0
WG SV	W8260B	SW5030	MW-99-5	trans-1,3-Dichloropropene	1	U	1	UJ	0 07	1	UG/L	-100 0
WG SV	W8260B	SW5030	MW-99-5	Trichloroethene	0 14	J	0 13	J	0 13	1	UG/L	74
WG SV	W8260B	SW5030	MW-99-5	Vinyl chloride	1	U	1	U	0 13	1	UG/L	-100 0

Attachment F - Laboratory Control Sample (Blank Spike) Accuracy

Matrix	BS Sample ID	Analytical Method	Prep.	Leach	Parameter	BS Lab Result	BS Lab	BS Units	True	BS:	BSLC		Accuracy Oua
SQ	[7863-7783-2584] C0927S02LCS	SW8260B	SW5035	NONE	1.1-Dichloroethene	44 43	<u>। इ.स. १</u>	UG/KG	Value 50	89	65	\$-= £ 135	\$5. 44. E
<u>sq</u>	C0928S01LCS	SW8260B	SW5035	NONE	1,1-Dichloroethene	45 36		UG/KG	50	91	65	135	
SQ	C0928S01LCS	SW8260B	SW5035	NONE	1,1-Dichloroethene	45 36		UG/KG	50	91	65	135	
SO	C092850 ILCS	SW8260B	SW5035	NONE	1,1-Dichloroethene	45 36		UG/KG	50	91	65	135	
SQ	C1010S01LCS	SW8260B	SW5035	NONE	1,1-Dichloroethene	479	=	UG/KG	50	96	65	135	
SQ_	C1010S01LCS	SW8260B	SW5035	NONE	1.1-Dichloroethene	479	=	UG/KG	50	96	65	135	
sq sq	C1019S01LCS	SW8260B SW8260B	SW5035 SW5035	NONE	1.1-Dichtoroethene	50 12 50 12	<u></u>	UG/KG	50 50	100	65	135	
so	C1079301LCS	SW8260B	SW5035	NONE	1.1 Dichloroethene 1.1-Dichloroethene	1 50 12	<u>-</u>	UG/KG UG/KG	50	100	65 65	135 135	
- wa	J0921W01LCS	SW8260B ,	SW5030	NONE	1 1-Dichloroethene	10 7	=	UG/L	10	107	-74	137	
WQ	J0924W01LCS	SW8260B	SW5030	NONE	1,1-Dichloroethene	11		UGAL	10	110	74	137	
wQ_	J0928W01LCS	SW8260B	SW5030	NONE	1,1-Dichloroethene	97	=	UGAL	10	97	74	137	
WQ_		SW8260B	SW5030	NONE	1,1-Dichloroethene	10 1	=_	UG/L	10	101	74	137	
LWQ	J1005W01LCS J1017W01LCS	SW8260B SW8260B	SW5030 SW5030	NONE	1,1-Dichloroethene	107		UG/L	10	107	74	137	
WQ	J1018W01LCS	SW8260B	SW5030	NONE	1,1-Dichloroethene 1,1-Dichloroethene	96	· - <u>-</u>	UG/L UG/L	10 10	96 102	74 74	137	j
WQ	J1025W01LCS	SW8260B	SW5030	NONE	1,1-Dichloroethene	88	— <u> -</u>	UG/L	10_	88	74	137	
WQ	J1025W01LCS	SW8260B	SW5030	NONE	1,1 Dichloroethene	88		ÜĞ/L	10	88	74	137	
SQ	K1009S01LCS	SW8260B	SW5035	NONE	1,1-Dichloroethene	49 21		UG/KG	50	98	65	135	
so_	K1020M01LCS	SW8260B	SW5035	NONE	1 1-Dichloroethene	6060		UG/KG	5000	121	74	137	
SQ_	K1023S01LCS	SW8260B	SW5035	NONE	1,1-Dichloroethene	48 95		UG/KG	50	98_	65	135	
SQ	K1023S01LCS K1023S01LCS	SW8260B SW8260B	SW5035	NONE .	1,1 Dichloroethene	48 95	- <u>=</u> ;	UG/KG	50	98	65	135	
WQ	K1023501LCS	_ SW8260B _	_SW5035 SW5030	NONE	1,1 Dichloroethene	48 95 9 8	- ;	UG/KG UG/L	50 10	<u>98</u>	65 j	135	
wo	R1207WOILCS	SW8260B	SW5030	NONE	1,1-Dichloroethene	94	<u>-</u> ,	UG/L	10	98_	74	137	
WQ	R1210W01LCS	SW8260B	SW5030	NONE	1,1-Dichloroethene	97	<u></u>	UG/L	10	97	74	137	
wo	R1211W01LCS	SW8260B	SW5030	NONE		93	=,	UG/L	10	93	74	137	— ⊣
WQ	R1212W01LCS	SW8260B	SW5030	NONE	1,1 Dichloroethene	97		UG/L	10	97	74	137	
WQ	J1214W01LCS	SW8260B	SW5030	NONE	1,1 Dichloroethene	10.3	_=	UG/L	10	103_	74	137	
, WQ (WQ	J1207W01LCS	SW8260B	_SW5030	NONE	1,1-Dichloroethene	86	=	UG/L_ '	10	86	74	137	i
WQ -	J1211W01LCS J1213W02LCS	SW8260B SW8260B	SW5030 SW5030	NONE	1,1-Dichloroethene 1,1-Dichloroethene	92	<u> </u>	UGAL	- 10-1	- 92 +	74	137	
wo	J1210W01LCS	SW82608	SW5030	NONE	1,1-Dichloroethene	- 10 3 9	٠-١٠٠٠ ٠	UG/L UG/L	10	- 103 ¦	74	137 137	
<u>wa</u> -	J1214W02LCS	SW8260B	SW5030	NONE	1.1 Dichloroethene	9 9 1	- [-	ÜĞÆ	10	-99 ←	74	-137	
wo	J1215W01LCS	SW8260B	SW5030	NONE	1,1-Dichloroethene	96	= 7	ÚG/L	10	96	74	137	
<u>wo</u> _	J1219W01LCS	SW8260B	SW5030	NONE	1,1-Dichloroethene	93.		ŬG/L	10	93	74	137	
I WQ	K1217W01LCS	SW8260B	SW5030	NONE	1,1-Dichloroethene	89	· - = - +	UG/L	10	89	74	137	!
WQ WQ	J1008W01LCS J1224W01LCS	SW8260B SW8260B	SW5030 SW5030	NONE	1,1-Dichloroethene	_ <u>_12</u>	· - <u>-</u> -	UG/L	10	120	74 74	137	:
- wa	1 J1227W01LCS	SW8260B	SW5030	NONE	1,1-Dichloroethene 1,1-Dichloroethene	10 6 9 8	··- <u>=</u> <u>-</u>	UG/L UG/L	10 10	106 98	74	137	<u></u>
wo	G1226WA1LCS	SW8270	SW3520	NONE	1 2 4-Trichlorobenzene	42 9 -	<u> </u>	UG/L	50	86	56	96	
wa	G1226WA1LCS	SW8270	SW3520	NONE	1 2-Dichlorobenzene	42 3	<u>-</u> •	UG/L	50	85	56	97	
WO	G1226WA1LCS	SW8270	SW3520	NONE	1,2-Diphenylhydrazine	48 9 i		UG/L	50	98	41	125	—— —— i
WQ	G1226WA1LCS	SW8270	SW3520	NONE	1,3 Dichlorobenzene	414		UG/L	50	83	52	92	
- <u>wo</u>	G1226WA1LCS	SW8270	SW3520	NONE	1,4 Dichlorobenzene	<u>41 7</u>	_ =_ ;	UG/L	50_	83	50	99	
, WQ	G1226WA1LCS G1226WA1LCS	SW8270 SW8270	SW3520 SW3520	NONE ,	2,4,6-Tribromophenol - SS	96		PERCENT	100	- 96	51	123	~
wo	G1226WA1LCS	SW8270 1	SW3520	NONE	2,4,6-Trichlorophenol 2.4 Dichlorophenol	47.8 50.1	- -;	UG/L UG/L	50 50	96 100	65 68	118	
-wo	G1226WA1LCS	SW8270 ;	SW3520	NONE	2 4-dimethyphenol	49 6		ÜG/L	_50 - 	99		122	
WQ	G1226WA1LCS	SW8270	SW3520	NONE .	2,4-Dinitrophenol	439	-	UG/L	50	88		114	———— <u>—</u>
WQ	G1226WA1LCS	SW8270	SW3520	NONE	2,4-Dinitrotoluene	50 6	_ <u>*</u>	ÜĞ/L	50	101	61	123	
WQ	G1226WA1LCS	SW8270	SW3520	NONE	2.6-Dinitrotoluene	52 1		ŪG/L	50	104	68	116	
WQ	G1226WA1LCS	SW8270	SW3520	NONE	2-Chloronaphthalene	46 1	7	UG/L	_ 50	92		111	
wq wq	G1226WA1LCS G1226WA1LCS	SW8270 SW8270	SW3520 SW3520	NONE	2-Chlorophenol	52 3	<u> </u>	UG/L	50	105		120	
wo ~	G1226WATECS	SW8270	SW3520 SW3520	NONE '	2 Fluorobiphenyl - SS 2-Fluorophenol - SS	88 i		PERCENT PERCENT	100	88 100		114 115	
i wo	G1226WA1LCS	SW8270	SW3520	NONE .	2-Nitrophenol	52		UG/L	50 :	104	66	177	
WQ	G1226WA1LCS	SW8270	SW3520	NONE	3,3'-Dichlorobenzidine	32	-	UG/L	50 +	64		161	
WQ	G1226WA1LCS	SW8270	SW3520	NONE	4,6-Dinitro-2 methylphenol	48 5	<u> </u>	UG/L		97	63	115	
WQ	G1226WA1LCS	SW8270	SW3520	NONE	4-Bromophenyl-phenylether	48.5		UG/L	50 50	97	6/	119	
WQ	G1226WAILCS	SW8270	SW3520	NONE	4 Chloro-3-methylphenol	513	_=	UG/L	50	103		121	
WQ	G1226WA1LCS G1226WA1LCS	SW8270	SW3520	NONE	4-Chlorophenyl-phenylether	47 9	- - -	ÜG/L	50	96		115	}
wa	G1226WA1LCS	SW8270 SW8270	SW3520 SW3520	NONE NONE	4-Nitrophenol Acenaphthene	45 3 48 1	ا ي	UG/L UG/L	50 50	91 oe		117	i
WQ	G1226WA1LCS	SW8270 +	SW3520 i	NONE	Acenaphthylene	47 2	<u>-</u>	UGAL	- 50 +	- 96 94		118 118	·{
WQ	G1226WA1LCS	SW82/0	SW3520	NONE	Anthracene	47 2	=	UG/L	50 i	94		120	
SQ	C0927S02LCS	SW8260B	SW5035	NONE	Benzene	49 49	` <u> </u>	UG/KG	50_ 1	99	65	135]	
so	C0928S01LCS	SW8260B	SW5035	NONE	Benzene	48 24	_ =	UG/KG 1	50 ⁻ ∫	96	65	135	

Attachment F - Laboratory Control Sample (Blank Spike) Accuracy

Matrix	BS Sample ID	Analytical	Prep	Leach		BS Cab	BS Lab	12.4.3.6.	BŞ.		C BSU	Accuracy
y maurix	S Sample ID	Method	Method	Method	Parameter 13 4		Oual	BS Units	True: Value	KRECT: C		Qual #
SQ	C0928S01LCS	SW8260B	SW5035	NONE	Benzene	48 24		UG/KG	50	96 65	135	
SQ SQ	C0928S01LCS	SW8260B SW8260B	SW5035	NONE	Benzene	48 24		UG/KG	50	96 65	135	
SQ SQ	C1010S01LCS C1010S01LCS	SW82608	SW5035 SW5035	NONE	Benzene Benzene	50 87	=	UG/KG UG/KG	50 50	102 65 102 65	135 135	} —-— - ∤
SQ	C1019S01LCS	SW8260B	SW5035	NONE	Benzene	46 71	<u>-</u> ,	UG/KG	50	93 + 65	135	[
SQ	C1019S01LCS	SW8260B	SW5035	NONE	Benzene	46 71	. <u> </u>	UG/KG	50	93 65	135	
_ sq wo	J0921W01LCS	SW8260B SW8260B	SW5035 SW5030	NONE	. Benzene	45 76 1 10 2	·	UG/KG UG/L	_50 10	92 65 102 78	135	
wo	J0924W01LCS	SW8260B	SW5030	NONE	Bertzene Benzene	103	<u> </u>	UG/L	10	102 78 103 78	121	<u></u>
WQ	J0928W01LCS	SW8260B	SW5030	NONE	Benzene	98		UG/L	10	98 78	121	
WQ.	J0930W01LCS	SW8260B	SW5030	NONE	Benzene	99		UG/L	10	99 78	121	
L_WQ		SW8260B SW8260B	SW5030 SW5030	NONE	Benzene	107	- -	UG/L UG/L	10	107 78 103 78	121	
wo	J1018W01LCS	SW8260B	SW5030	NONE	Benzene	10.5	~== -	UG/L	10	105 78	121	<u></u>
WQ	J1025W01LCS	SW8260B	SW5030	NONE	Benzene	97	= ^.	UG/L	10	97 78	121	i
WQ.	1 J1025W01LCS	SW8260B	SW5030	NONE	Benzene	97	=	UG/L	10	97 78	121	i i
SQ_	K1009S01LCS K1020M01LCS	SW8260B SW8260B	SW5035 SW5035	NONE	Benzene Benzene	52 <u>12</u> 5190		UG/KG UG/KG	5000 5000	104 65 104 78	135	h
SQ	K1023501LCS	SW8260B	SW5035	NONE	Benzene	48 23	- =	UG/KG	50	96 65	135	
SQ	K1023S01LCS	SW8260B	SW5035	NONE	Benzene	48 23	` = .	UG/KG	50	96 65	135	,
SQ	K1023S01LCS	SW8260B	SW5035 SW5030	NONE	Benzene	48 23 9 5	-	UG/KG	_ 50_	96 - 65 95 - 78	135	<u> </u>
l wo	K1029W01LCS R1207W01LCS	SW8260B SW8260B	SW5030	NONE.	Benzene Benzene	95	= ~(UG/L UG/L	10 10	95 78 101 78	121	
wo	R1210W01LCS	SW8260B	SW5030	NONE	Benzene	101	- =	UGAL	10	101 78	121	
_ WO	R1211W01LCST		SW5030	NONE	Benzene	10	= . ;	_ug/_	10	100 78	121	
L_WQ	R1212W01LCS	SW82608	SW5030	NONE	Benzene	10.3	=_ :	ug/L_	10	103 78	121	
WQ WQ	J1214W01LCS J1207W01LCS	SW8260B SW8260B	_SW5030 - SW5030	NONE	Benzene Benzene	104		UG/L UG/L	10 10	104 78 106 78	121	
WO	J1211W01LCS	SW8260B	SW5030	NONE	Benzene	1117	== :	UĞA	10	117 78	121	†
WO	J1213W02LCS	SW8260B	SW5030	NONE	Benzene	106	= _	UG/L	10	106 78	121	
wo	J1210W01LCS	SW8260B	SW5030	NONE	Benzene	10.9	=_	- UG/L	10	109 78	121	· :
- WQ	J1214W02LCS J1215W01LCS	SW8260B SW8260B	SW5030 SW5030	NONE ,	Benzene Benzene	10 4 10	<u> </u>	UG/L UG/L	- 10 10	104 78 100 78	121	- · i
i wo	J1219W01LCS	SW8260B	SW5030	NONE	Benzene	10	·- - ·	UG/L	10	100 - 78	121	[
wo	K1217W01LCS	SW8260B	_SW5030	NONE.	Benzene	95		ŪĢ/Ľ ↓	10]	95 78	121	
WQ	J1008W01LCS	_SW8260B_ ,	SW5030	NONE	Benzene	109	= -	UG/L	10-	109 78	121	¦
wo -	J1224W01LCS J1227W01LCS	SW8260B SW8260B	SW5030 SW5030	NONE :	Benzene Benzene	10.2	- <u> </u>	UG/L UG/L	10		121	
WO	G1226WA1LCS	SW8270	SW3520	NONE	Benzo(a)anthracene	49 4	=	UG/L	50	99 65	119	
WO	G1226WA1LCS	SW8270	SW3520	NONE	Benzo(a)pyrene	46 9	=	UG/L	50	94 61	114	
WQ WQ	G1226WA1LCS G1226WA1LCS	SW8270 SW8270	SW3520 SW3520	NONE .	Benzo(b)fluoroanthene	52 <u>5</u> 40		UG/L UG/L	<u>50</u> ¦	10562_ 57	121	
wo	G1226WA1LCS	SW8270	SW3520	NONE '	Benzo(g,h i)perylene Benzo(k)fluoranthene	536	·- <u>-</u>	UG/L	50	<u></u>	126	
, MO	G1226WATLCS	SW8270	SW3520	NONE	bis(2-Chloroethoxy)methane	518	~ <u>_</u>	TÜG/L	50	104 67	117	
WO	G1226WA1LCS	SW8270	SW3520	NONE	bis(2-Chloroethyl)ether	53.9	=	UG/L	50	108 61	117	
	G1226WA1LCS G1226WA1LCS	SW8270 SW8270	SW3520 SW3520	NONE -	bis(2-Ethylhexyl)phthalate	53.7	- <u>-</u> →	UG/L	50 -	107 50	139	
⊢ <u>sō</u> →	C0927\$02LCS	SW8260B	SW5035	NONE .	Butylbenzylphthalate Chlorobenzene	_52 3_ 48 68		UG/KG	50	105 <u>58</u> 97 65	124	!
sa	C0928S01LCS	SW8260B	SW5035	NONE	Chlorobenzene	46 69	_ = →	UG/KG	50	93 65	135	. – . – j
SO	C0928S01LCS	SW8260B	SW5035	NONE	Chlorobenzene	46 69		UG/KG	_50 .	93 65	135	
SQ -	C0928S01LCS L C1010S01LCS	SW8260B :	SW5035 SW5035	NONE	Chlorobenzene	46 69	<u>=</u> . :	UG/KG	50_	93 65 100 65	135 135	
- SQ	C1010S01LCS	SW8260B	SW5035	NONE	Chlorobenzene Chlorobenzene	49 82 49 82		UG/KG UG/KG	50	0065	135	
so	C1019S01LCS	SW8260B	SW5035	NONE	Chlorobenzene	46 6	=^	UG/KG	50	93 65	135	
į so	C1019S01LCS	SW8260B	SW5035	NONE	Chlorobenzene	46 6	= - 1	UG/KG	50]	93 65	135	
SQ i	C1025S01LCS	SW8260B	SW5035	NONE	Chlorobenzene	49 96	= .	ng/kg	50	100 _ 65	135	
- WQ	J0921W01LCS J0924W01LCS	SW8260B	SW5030 SW5030	NONE :	Chlorobenzene Chlorobenzene	103	=	UGAL	10	103 80 105 80	117	
wo	J0928W01LCS	SW8260B	SW5030	NONE	Chlorobenzene	99	· :	UG/L	10 t	99 80	117	
. wo		SW8260B	SW5030	NONE	Chlorobenzene	97	= [UG/L	10	97 i 80	117	
wo -		SW8260B :	SW5030	NONE I	Chlorobenzene	108	- <u>-</u>	UG/L	10	108 80	117	
		SW82608	SW5030 SW5030	NONE	Chlorobenzene Chlorobenzene	10 2	Ī <u>-</u>	UG/L	10	10280 105 80	117	
wa		SW8260B	SW5030	NONE	Chlorobenzene	97		UG/L	10 j	97 80	117	
		SW8260B	SW5030	NONE	Chlorobenzene	9 7	=	UGAL	10	97 80	117	
		SW8260B	SW5035	NONE	Chlorobenzene	49 28	= .	UG/KG	50_	98 65	135	i
		SW8260B SW8260B	SW5035 SW5035	NONE	Chlorobenzene Chlorobenzene	. 5280 - 47 77	<u>-</u>	UG/KG UG/KG	5000 50	_ <u>10680</u> 65	117 135	
								300				

Attachment F - Laboratory Control Sample (Blank Spike) Accuracy

19/12/19	134070446F 1497	TENER &	do Figurad	DAS SAF	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	स्य: स्ट्राइट	HENRY WAYN	.0.03(MY2107	78S.	P. M. Call And	in just sam	(4) (4) (4) (4) (4) (4) (4) (4) (4) (4)
Maria	BS Sample ID.	Analytical	Prep	Leach?	Parameter		BSLAD	BS Units	True	SBS BSL	C BSV	Accuracy.
447	170 F A. 4 5 7 A.	أورية فالتركبين	1.25.25 VE	المتقعم المتما	المراجع المراج	Result	Qual	مر ومود الا	Value	%Rec *L	, CL	Qual
SQ SQ	K1023S01LCS K1023S01LCS	SW8260B SW8260B	SW5035	NONE	Chlorobenzene	47 77	_=	UG/KG	50	96 65	135	ļ
wo	K1029W01LCS	SW8260B	SW5035 SW5030	NONE	Chlorobenzene Chlorobenzene	$\frac{1}{1} - \frac{47}{10} = \frac{1}{10}$	_=	UG/KG UG/L	5 <u>0</u> 10	96 -65 100 80	135	<u> </u>
WQ	R1207W01LCS	SW8260B	SW5030	NONE	Chlorobenzene	10	-	UG/L	10	100 80 100 80	117	<u>-</u>
WQ	R1210W01LCS	SW8260B	SW5030	NONE	Chlorobenzene	98		UGAL	10	98 80	117	
WQ	R1211W01LCS	SW8260B	:_SW5030	NONE	Chlorobenzene	10	= -	ÜĞÆ	10	100 80	117	i
' WQ_	R1212W01LCS	SW8260B	SW5030	NONE	Chlorobenzene	10.5	- = 1	UG/L	10	105 80	117	
WQ WQ	J1214W01LCS J1207W01LCS	SW8260B SW8260B	SW5030 SW5030	NONE	Chlorobenzene	103.	= '	UG/L	10	103 80	117	
-wa	J1211W01LCS	SW8260B	SW5030	NONE I	Chlorobenzene Chlorobenzene	- <u>10 4</u> - '		UG/L UG/L	10	104 80 109 80	117	- — -∤
wQ	J1213W02LCS	SW8260B	SW5030	NONE	Chlorobenzene	10.5	<u>-</u>	UG/L	10 10	109 80 105 80	117	├ ──
WQ	J1210W01LCS	SW8260B	SW5030	NONE	Chlorobenzene	10.9		UG/L	10	109 80	117	h
WQ	J1214W02LCS	SW8260B	SW5030	NONE	Chlorobenzene	10	- =,	UG/L	10	100 80	117	
<u>wq</u> _	J1215W01LCS	SW8260B	SW5030	NONE	Chlorobenzene	10	_ =_ :	ÜĞÆ	10	100 80	117	
, <u>WQ</u>	J1219W01LCS	SW8260B SW8260B	SW5030	NONE	Chlorobenzene	97	<u>.</u> =	UG/L	10	97 80	117	
i wo	J1008W01LCS	SW8260B	SW5030 SW	NONE	Chlorobenzene Chlorobenzene	94	<u> </u>	UG/L	10 18	94 80	117	
WQ	J1224W01LCS	SW8260B	SW5030	NONE	Chlorobenzene	97	= 1	UG/L	<u>10</u>	107 80 97 80	117	
wa	J1227W01LCS	SW8260B	SW5030	NONE	Chlorobenzene	10 7		- ŪĞĪL	10	107 + 80	117	
WQ	G1226WA1LCS	SW8270	SW3520	NONE '	Chrysene	488	 ;	ŪG/L	50	98 64	120	
WQ _	G1226WA1LCS	SW8270	SW3520	NONE	Dibenzo(a,h)anthracene	418	``	UG/L	50	84 61	114	
WQ WQ	G1226WA1LCS	SW8270	SW3520	NONE	Diethylphthalate	48.9	. = _ `	UG/L_	50 75	98 39	141	
- WQ -	G1226WATECS	SW8270 SW8270	SW3520 SW3520	NONE NONE	Dimethylphthalate	48 7		UG/L	50	97 . 38	140	
WQ	G1226WA1LCS	SW8270	SW3520	NONE	Di n-butylphthalate Di n-octylphthalate	50 3 53 1		UG/L UG/L	<u>50</u> -	101 <u>54</u> 106 <u>63</u>	130	
WQ	G1226WA1LCS	SW8270	SW3520	NONE	Fluoranthene	493	<u>-</u> -•	ÜĞA	50	99 65	122	-
WQ	G1226WA1LCS	SW8270	SW3520	NONE	Fluorene	48 2	- <u>-</u> ´	UG/L	50	96 69	121	
<u>WQ</u>	G1226WA1LCS	SW8270	SW3520	NONE	Hexachlorobenzene	472	- <u>-</u>	UG/L	50	94 60	123	
WQ WQ	G1226WA1LCS	SW8270	SW3520	NONE	Hexachlorobuladiene	40 6	= ;	UG/L	50	81 43	105	
- WQ	G1226WA1LCS G1226WA1LCS	SW8270 SW8270	SW3520 SW3520	NONE	Hexachlorocyclopentadiene	23 3	_ <u>=</u> - `-	UG/L	- <u>50</u> - '	47 24	83	
WQ	G1226WA1LCS	SW8270	SW3520	NONE	Hexachloroethane Indeno(1,2 3-cd)pyrene	<u>39 7</u> 	~- ⁼ '-	UG/L_ ; UG/L ;	50 <u>!</u> 50	<u>79</u> 44 83 61	99	
WQ	G1226WA1LCS	SW8270	SW3520	NONE	Isophorone	53 1		- UG/L	50	106 63	118	
WQ	G1226WA1LCS	_ SW8270	SW3520	NONE	Naphthalene	45.4	=	UG/L	50 .	91 56	114	}
WQ_	G1226WA1LCS	SW8270	SW3520	NONE	Nitrobenzene	519		UG/L	ັ50 <u>ີ</u>	104 63	116	
WQ WQ	G1226WA1LCS G1226WA1LCS	SW8270	SW3520	NONE	Nitrobenzene-d5 - SS	98	_ =	PERCENT	100	98 67	112	
WQ	G1226WAILCS	SW8270 SW8270	SW3520 SW3520	NONE	N Nitrosodimethylamine	50 3		UG/L !	50	101 50	150	
w ā-	G1226WA1LCS	SW8270	SW3520	NONE	N Nitroso-di n-propytamine ¹ N-Nitrosodiphenylamine	- 57 4		UG/L	50 50	115 <u>68</u> 94 54	121	
WQ	G1226WA1LCS	SW8270	SW3520	NONE	Pentachlorophenoi	45.6		UG/L	50	91 55	118	
WQ	G1226WA1LCS	SW8270	SW3520	NONE	Phenanthrene	48 2	= 1	UG/L	50	96 64	120	
WQ	G1226WA1LCS	SW8270	_ SW3520	NONE	Phenol	51 7		UGIL	50	103 57	120	
WQ	G1226WA1LCS G1226WA1LCS	SW8270 SW8270	SW3520	NONE	Phenol-d5 - SS	100		PERCENT	100	100 48	115	
WQ .	G1226WAILCS	SW8270	SW3520 SW3520	NONE	Pyrene	_50.9		UGAL	50	102 64	122	
SQ	C0927\$02I CS	SW82608	SW5035	NONE	Terphenyl d14 - SS Toluene	91 47.96	<u> </u>	UG/KG	100_	91 30	154	
SQ	C0928S01LCS	SW8260B	SW5035	NONE	Toluene	47.8	= ;	UG/KG	50	$-\frac{90}{96}$ - 64	135	——— [
SQ	C0928S011 CS	SW8260B	SW5035	NONE	Toluene	47.8	= 1	UG/KG	50	96 64	135	
SQ	C0928S01LCS	SW8260B	SW5035	NONE	Toluene	47.8		UG/KG	50	96 64	135	
SQ SQ	C1010S01LCS C1010S01LCS	SW8260B SW8260B	SW5035	NONE :	Toluene	50 48	}	UG/KG	50	101 64	135	
SQ	C1019S01LCS	SW8260B ;	SW5035 SW5035	NONE	Toluene	_50 48 43 03	<u>-</u>	UG/KG	50 +	101 64	135	
SQ	C1019S01LCS	SW8260B	SW5035	NONE	Toluene	43 03		UG/KG UG/KG	_50 50	86 <u>64</u> 86 64	135	
SQ	C1025S01LCS	SW8260B		NONE	Toluene ,	49 09		UG/KG	- 50 - 1	60 <u>.64</u> 98 <u>.64</u>	135	
WQ	J0921W01LCS	SW82608	SW5030	NONE I	Toluene	106		ຼົΰG/L ̄Ţ	10 1	106 79 106 79	119	
WQ	J0924W01LCS	SW8260B		NONE	Toluene	106		_UG/L	10 1		119	
WQ WQ	J0928W01LCS J0930W01LCS	SW8260B SW8260B		NONE -	Toluene	99	_ =	nev j	10	. 99 _ 79	119	
wa	J1005W01LCS	SW8260B	SW5030	NONE :	Toluene Toluene	9 6 10 7	_=	UG/L _ L	10	96 79	119	
WQ	J1017W01LCS	SW8260B	SW5030	NONE	Toluene	10 /	<u></u> -	UG/L UG/L	_10 _10	107 7 <u>9</u> 104 79	119 119	
WQ	J1018W01LCS	SW8260B	SW5030	NONE	Toluene	103		ÜĞÆ	10	103 + 79	119	
WQ	J1025W01LCS	SW8260B	SW5030	NONE	Toluene	96		UGAL	10	96 79	119	
- wa	J1025W01LCS	SW8260B	SW5030	NONE	Toluene :	96	_=	UG/L	10 1	96 79 96 79	119	
SO SO	K1009S01LCS K1020M01LCS	SW8260B SW8260B		NONE	Toluene	47 69		UG/KG	50 ;	95 64	135	
SQ SQ	K1023S01LCS	SW8260B	SW5035 SW5035	NONE	Toluene	5120 48 53	· - `	UG/KG	5000	102 79	119	
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so	K1023S01LCS	SW8260B		NONE	Toluene	48 53	'	UG/KG	50 7	97 64	135	
					· · · ·				<u></u>			

Attachment F - Laboratory Control Sample (Blank Spike) Accuracy

Matrix	BS Sample ID	Analytical	Prop	Leach	Paremoter	BŞ Lab	BS Lab	BS Units	S. BS	BSS	BŠĽČ	BSU	Accuracy
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WQ	K1029W01LCS	SW8260B	SW5030	NONE	Toluene	10 1	=	UG/L	10	101	79	119	
WQ	R1207W01LCS	SW8260B	SW5030	NONE	<u>Toluene</u>	10	= :	UG/L	10	100	79	119	
WQ	R1210W0 ILCS	SW8260B	SW5030	NONE	Toluene	99	= _:	UG/L	10	99	79	119	
L WQ	R1211W01LCS	SW8260B SW8260B	SW5030 SW5030	NONE	Toluene Toluene	103	₹	UG/L UG/L	<u>10</u> 10	103	79 79	119 119	├ ─
- WQ	J1214W01LCS	SW8260B	SW5030	NONE _	Toluene	10.5		UG/L -	10	105	79	119	∤
- wo	J1207W01LCS	SW8260B	SW5030	NONE	Toluene	112	· - <u>-</u>	UG/L	10 -	112	79	119	}
-wQ	J1211W01LCS	SW8260B	SW5030	"- NONE	Toluene	12 2	:	UG/L	10	7,722	79	119	
WQ	J1213W02LCS	SW8260B	SW5030	NONE	Toluene	107	= .	UGAL	10	107	79	119	<u> </u>
WO	J1210W01LCS	SW8260B	SW5030	NONE	Toluene	113		UG/L	10	113	79	119	
WQ	J1214W02LCS	SW8260B	SW5030	NONE	Toluene	103	= - ;	UG/L	10	103	79	119	
WQ	J1215W01LCS	SW8260B	SW5030	NONE	Toluene	103	= -	υζ⁄ι	10	103	79	119	
∟ wo	J1219W01LCS	SW8260B	SW5030	NONE	Tofuene	10.2	. = _	UG/I	10	102	79	119	
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so	C1025S01LCS	SW8260B	SW5035 '	NONE	Trichloroethene	46 98	= .	UG/KG	50	94	61_	135	
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L WO	J0924W01LCS	SW8260B	SW5030	NONE	Tnchloroethene	10 4	=	UG/L	10 i	104	81	122	,
wo :	_J0928W01LCS _J0930W01LCS	SW8260B	SW5030 ,	NONE .	Trichloroethene	98		_UG/L	- <u>10</u> - 1	98	81	122	!
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SQ	K1023S01LCS_	SW82608	SW5035	NONE	Trichloroethene	45 17	=	UG/KG	50	90	61	135	-
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rwā ¦	J1214W01LCS	SW8260B	SW5030	NONE 1	Trichloroethene	10.5	= '	UG/L	10	105	81	122	
wo	J1207W01LCS	SW8260B	SW5030	NONE	Trichloroethene	98	=	_UG/L	10]	98	81	122	
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WQ_	J1213W02LCS	SW8260B	SW5030	NONE	Trichloroethene	10 3	=	_UG/L	10	103	81	122]
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	J1214W02LCS	SW82608	SW5030	NONE	Inchloroethene	10 4	=	UG/L 1	10	104		122	
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- wa	J1224W01LCS	SW8260B	SW5030	NONE	Trichloroethene	95	=	UG/L	10	95		122	
	J1227W01LCS	SW8260B	SW5030	NONE	Tnchloroethene	106		UG/L	10	106		122	
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Attachn	Jesen Le Verier Constitution	Total Organic Carbon	Pentachlorophenol	1,2-Dichloroethane	bis(2-Ethylhexyl)phthalate	Bromoform	Carbon tetrachlonde	Chloroform	Methylene chloride	Tetrachloroethene	Toluene	Trichloroethene	1,1,2,2-Tetrachloroethane	1,1-Dichloroethane	1,1-Dichlorgethene	1,2-Dichloroethane	bis(2-Ethylhexyl)phthalate	Bromomethane	Carbon tetrachlonde	Chloroform	Ethylbenzene	Methylene chlonde	Tetrachloroethene	Toluene	trans-1,2-Dichloroethene	Trichloroethene
	Leach, Method	NONE	SW1312	NONE	NONE	NON M	NONE	NON	NON	SON I	NON	NONE	NON:	NONE NO	MON'	NON:	NONE	NON	NONE	NONE		NONE	NON	NONE	NONE	NONE
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	Analytical	SW9060	SW8270C	SW8260B	SW8270C	SW8260B	SW8Z6UB	SW8260B	SW8Z60B	SVV8ZBUB	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	SW8270	SW8260B	SW8260B	SW8250B	SW8260B	SW8260B	SW8260B	SW8260B	SW8260B	2W8Z6UB
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TAB

Appendix B

Appendix B – Rev. 1 EBT Treatability Study Workplan

Defense Distribution Center (Memphis) Main Installation

Enhanced Bioremediation Treatment Treatability Study Workplan

Rev. 1

PREPARED FOR



U.S. Army Engineering and Support Center, Huntsville 4820 University Square Huntsville, AL 35816

PREPARED BY

CH2M HILL

115 Perimeter Center Place NE, Suite 700

Atlanta, GA 30346

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Acronyms

BCT Base Cleanup Team

BRAC Base Realignment and Closure

BTEX benzene, toluene, ethylbenzene, and xylenes

CAH chlorinated aliphatic hydrocarbon

°C degrees Celsius

Cts-1,2-DCE Cis-1,2-dichloroethene

COC Chain-of-Custody

COCs Constituents of concern

cp centipoise

DCE Dichloroethene

DLA Defense Logistics Agency
DQOs data quality objectives

DRC Depot Redevelopment Corporation
EBT Enhanced Bioremediation Treatment

EPA Environmental Protection Agency

FS Feasibility Study

ft feet

H₂ Hydrogen

HRC™ Hydrogen Releasing Compound
LTOA Long Term Operational Area
MCLs Maximum Contaminant Level

MI Main Installation μg/L micrograms per liter

MNA Monitored Natural Attenuation

OVA-FID Organic Vapor Analyzer-Flame Ionization Detector

PCE Tetrachloroethene

POL petroleum/oil/lubricants

QA quality assurance

RAB Restoration Advisory Board

RD Remedial Design

RI Remediation Investigation

ROD Record of Decision

RPO Remedial Process Optimization

TCE Trichloroethylene

TDEC Tennessee Department of Environment and Conservation

TS Treatability Study

UIC underground injection control

VC Vinyl chloride

VOC Volatile organic compound

1.0 Introduction

This Enhanced Bioremediation Treatment (EBT) Treatability Study Workplan for accelerated bioremediation of chlorinated volatile organic compounds or, as referred to in this document, chlorinated aliphatic hydrocarbon (CAH) compounds, in groundwater at the Main Installation (MI) of the former Memphis Depot has been prepared for the U.S. Army Corps of Engineers – Huntsville Center as part of the Remedial Design (RD) for the remediation of groundwater. The Defense Logistics Agency (DLA) is the lead agency for site activities at the Memphis Depot. The supporting regulatory agencies are the U.S. Environmental Protection Agency (EPA) and the Tennessee Department of Environment and Conservation (TDEC). Together, DLA, EPA, and TDFC compose the Base Realignment and Closure (BRAC) Base Cleanup Team (BCT).

Alternative GW3 – Enhanced Bioremediation, as described in the MI Record of Decision (ROD) document (CH2M HILL, 2001), employs the use of injection of electron donor to enhance the natural biodegradation processes and states that pilot tests will be required to determine injection volumes, spacing, and depth. This workplan is a result of the need for a pilot test/treatability study of EBT and has been prepared with reference to Guidance for Conducting Treatability Studies under CERCLA. Final. (EPA, October 1992).

1.1 Scope of Treatability Study

The development of the EBT Treatability Study has occurred in two phases. The first phase involved gathering available information to support selection of appropriate electron donor substrates for accelerated biodegradation of CAHs to evaluate in the field study. Review of this information has allowed CH2M HILL to construct this Treatability Study workplan and recommend two of the more promising electron donor substrates to be evaluated in the field. The following electron donors are considered to be potentially applicable for the treatability study at the MI

- Hydrogen Releasing Compound (HRC™) (e.g., Regenesis's® polylactate ester);
- Commercially available organic carbon electron donor (e.g., lactate, butyrate, propionate, ethanol, vegetable oil, or other material); and
- Direct hydrogen addition (e.g., hydrogen sparging)

This workplan also outlines the need to examine certain subsurface conditions that need to be present for in-situ anaerobic biodegradation to be effective. These conditions generally include presence of appropriate bacteria capable of degrading the target compounds, suitable electron donors (such as organic carbon or hydrogen), an appropriate terminal electron acceptor process (such as methanogenic conditions), and essential nutrients (e.g., nitrogen, phosphorus, sulfur and low levels of iron, manganese, magnesium, etc). Appropriate physical and chemical conditions (such as pH, temperature, DO, ORP), must also be present.

The second phase of the treatability study will include installing two test sites to evaluate the two different electron donor substrates. Each test site, located in the southeast and southwestern areas of the MI, will consist of injection wells screened across the aquifer, and monitoring wells where the electron donors and changes in contaminant levels will be monitored. Monitoring will include baseline and post-injection sampling events. The post-injection events are scheduled for 6 months after the injection phase ends. At the completion of the monitoring events, an EBT Technical Memorandum describing treatability study procedures and results will be produced that will be included in the Intermediate (60 percent.) MI Remedial Design document.

This Treatability Study Workplan is organized into the following sections and appendices:

- **Section 1.0 Introduction** includes a discussion of the work plan structure and organization
- **Section 2.0 Project Description** provides background information on the site and summarizes pertinent waste characterization data. Section 2 also introduces the type of study to be conducted.
- **Section 3.0** Treatment Technology Description describes the principles and characteristics of biodegradation behind EBT as a treatment technology.
- **Section 4.0 Test Objectives** defines the objectives of the treatability study and the intended use of the data.
- **Section 5.0 Electron Donor Selection** defines the selection criteria and conclusion of the electron donor selection process.
- Section 6.0 Experimental Design and Procedures identifies the tier and scale of testing, the volume of waste material to be tested, delivery system, critical parameters, and the type and amount of replication
- **Section 7.0 Equipment and Materials** lists the equipment, materials and reagents that will be used in the performance of the treatability study.
- **Section 8.0 Sampling and Analysis** describes how the Sampling and Analysis Plan will address field sampling, waste characterization, and sampling and analysis activities in support of the treatability study.
- Section 9.0 Data Management, Analysis, and Interpretation describes the procedures for recording observations and raw data in the field or laboratory and procedures that will be used to analyze and interpret data from the treatability study
- **Section 10.0 Health and Safety** describes how the Health and Safety Plan will address the hazards associated with treatability testing
- **Section 11.0** Residuals Management describes the management of treatability study residuals.
- **Section 12.0** Community Relations describes the community relations activities performed in conjunction with the treatability study.

Section 13.0 Reporting describes the preparation of interim and final reports documenting the results of the treatability study.

Section 14.0 Schedule indicates the planned starting and ending dates for the tasks outlined in the work assignment

Section 15.0 References lists all documents cited in this plan.

2.0 Site History and Setting

2.1 Site History

Starting in the 1940s, the Memphis Depot received, warehoused, and distributed supplies common to all U.S. military services and some civil agencies. Activities at the MI included storing and shipping various materials (e.g., food, clothing, medical supplies) and industrial supplies (e.g., hazardous materials). Several commonly used hazardous materials were also used for facility maintenance. Hazardous materials which were used or stored at the Depot during its operational period include. flammables, solvents, petroleum/oil/lubricants (POL), paints, pesticides, herbicides, wood treating products, oxidizers, corrosives, and reactives. The Memphis Depot was deactivated as a military supply center in 1997.

The Memphis Depot, now known as the Memphis Depot Business Park, covers 642 acres of land and is separated into two distinct areas. The MI comprises 574 acres and Dunn Field, to the north of the MI, comprises the balance. A map with the former RI functional unit boundaries within the MI is presented in Figure 2-1.

The MI was extensively developed. The only significant vegetated area is the golf course, located in the MI's southeastern sector. Topography in the MI is nearly level. The two surface water bodies on the Depot are too shallow to intercept the local water table.

2.2 Hydrogeology

The fluvial aquifer beneath the Memphis Depot occurs under unconfined conditions in fluvial-type deposits at an average depth of 87 feet below ground surface (CH2M HILL, January 2000). Aquifer thickness in the fluvial deposits ranges from <1 foot the northwest corner of the MI to as high as 57 feet (ft) in the west central portion of the MI. Hydrogeologic cross-sections typical of the geology beneath the MI are presented in Figures 2-2 and 2-3 The cross-sections were developed as part of the 2002 MI Long Term Operational Area (LTOA) Technical Memorandum. Groundwater flow in this aquifer is variable but is primarily southwest, south, and southeast. Figure 2-4 presents the most recent interpretation of the potentiometric surface underlying the MI.

The fluvial aquifer is typically underlain by a clay-rich unit that occurs beneath most of the MI. This upper clay of the Jackson Formation/Upper Claiborne Group does not appear to be present at the base of the fluvial deposits in the northwestern part of MI and in the southwestern part of Dunn Field (the northern half of the Memphis Depot). The MI RI concluded that clay-rich units (clay or clayey sand) occur in the Jackson Formation/Upper Claiborne Group at variable elevations, and also are highly variable in thickness. The Memphis Sand aquifer is separated from the overlying fluvial aquifer by units of the Jackson Formation/Upper Claiborne Group. The Memphis Sand is the source of water supply for the City of Memphis

A more focused discussion of the hydrogeology of each study area is presented in Section 5.

2.3 Nature and Extent of Contamination

The constituents of concern (COCs) reported in groundwater beneath the MI, as described by the MI Remedial Investigation (RI) Report (CH2M HILL, 2000), are CAHs, primarily tetrachloroethene (PCE) and trichloroethylene (ICE). Impacted groundwater is present within the fluvial aquifer. This Treatability Study workplan focuses on contamination in the fluvial aquifer beneath portions of the MI (Figure 2-5). An apparent source for this groundwater contamination has not been revealed.

Two distinct volatile organic compound (VOC) groundwater plumes were delineated in the southwestern and southeastern portions of the MI within the RI document. These plumes appear to have different origins and, based on recent data, do not commingle. Figure 2-6 illustrates concentrations of PCE and TCE as well as other CAHs in the fluvial aquifer, on the basis of data achieved from the 2001 LTOA investigation. As revealed in groundwater sample data from this investigation, average PCE concentrations range from below laboratory detection limit to 480 micrograms per liter (μ g/L). Average TCE concentrations range from below laboratory detection limit to 79 μ g /L. In addition, an unusual detection of carbon tetrachloride and chloroform at average concentrations of 122 μ g/L and 77 μ g/L, respectively, was revealed in the southeast corner of the MI.

Table 2-1 presents additional details on CAHs detected at least once in groundwater samples collected during the 2001 LTOA investigation. These samples were collected through use of diffusion bag samplers, which allows for sampling at defined intervals Review of Table 2-1 indicates that contamination by CAHs is spread throughout the entire thickness of the aquifer and, in some instances, contaminant levels are highest in the upper portion of the aquifer.

3.0 Treatment Technology Description

Biological natural attenuation processes include biodegradation through either co-metabolic reactions, direct dechlorination, or oxidation. Whether an aquifer is aerobic or anaerobic has a direct effect on which biological process is prevalent. Co-metabolic transformation of CAHs such as ICE in aerobic or anaerobic environments has been reported by McCarty (1994) CAHs such as VC, 1,2-DCE, and chloroethane have been reported by Bradley and Chapelle (1996) as being degraded by oxidation effects in aerobic and anaerobic environments. The process that occurs frequently for the transformation of contaminant compounds such as CAHs is, however, anaerobic reductive dechlorination.

Anaerobic reductive dechlorination is a series of reductions through dechlorination reactions. For example, PCE degrades to TCE, which degrades primarily to cis-1,2-dichloroethene (cis-1,2-DCE), which in turn degrades to vinyl chloride (VC), which is dechlorinated to ethene. Figure 3-1 presents this anaerobic reductive dechlorination pathway. Each step requires a lower reduction/oxidation (redox) potential than the previous one. PCE degradation occurs in a wide range of reducing conditions, whereas VC is reduced to ethene only under sulfate reducing and methanogenic conditions. During each of these transformations, the parent compound releases one chloride ion and gains one hydrogen atoms. Two electrons are transferred during the process, which may provide a source of energy for the microorganism. The ultimate source for the hydrogen and electrons in this reaction is some type of organic substrate. Hydrogen (H₂) is released during fermentation of the substrate. The hydrogen liberated from this substrate acts as the actual electron donor for respiration (ITRC, 1998)

Subsurface microorganisms create energy for life processes by oxidizing organic matter. Only those redox reactions that yield energy are facilitated by microorganisms. During redox reactions, the oxidation of an electron donor (e.g., native organic carbon, fuel hydrocarbons, landfill leachate) combined with the reduction of an electron acceptor (e.g., oxygen, nitrate, manganese, ferric iron, sulfate, carbon dioxide, and anthropogenic compounds such as CAHs) ultimately yields energy for use by organisms. The microbes are using carbon (electron donors) as a food source and are breathing, or respiring, electron acceptors. Dissolved oxygen (DO) yields the most energy and is used first as the prime electron acceptor. After DO is consumed, anaerobic microorganisms typically use native electron acceptors (as available) in the following order of preference. nitrate, ferric iron oxyhydroxide, sulfate, and eventually CAHs (FPA, 1998)

CAH plumes in groundwater can exhibit three types of biodegradation behavior depending on the amount of solvent, the amount of organic (native and anthropogenic) carbon in the aquifer, the distribution and concentration of natural electron acceptors, and the types of electron acceptors being used. Individual plumes may exhibit all three types of behavior in different areas of the plume (EPA, 1998). These three behavior types are as follows:

 Type 1 behavior occurs where the primary substrate is anthropogenic carbon (e.g., benzene, toluene, ethylbenzene, and xylenes [BTEX] or landfill leachate), and this anthropogenic carbon drives reductive dechlorination. Type 1 behavior results in the rapid and extensive degradation of highly chlorinated solvents such as PCE, TCE, and dichloroethene (DCE).

- Type 2 behavior dominates in areas characterized by relatively high concentrations of biologically available native organic carbon; the natural carbon source drives reductive dechlorination. This behavior generally results in slower biodegradation of the highly chlorinated solvents when compared to Type 1 behavior. But, areas with high concentrations of natural organic carbon can result in rapid degradation of CAHs.
- Type 3 behavior dominates in areas characterized by low concentrations of native and/or anthropogenic carbon and concentrations of DO greater than 1.0 milligrams per liter (mg/L). Under these conditions, reductive dechlorination will not occur, therefore, little or no removal of PCE, TCE, and DCE will occur. Biodegradation may proceed via the much slower process of co-metabolism, but will be limited by the low concentrations of native or anthropogenic carbon. Type 3 behavior also occurs in groundwater that does not contain microbes capable of biodegradation of chlorinated solvents.

The list of conditions that a microbial population involved in bioremediation requires for sustainability includes a source of carbon, an electron donor, an electron acceptor, appropriate nutrients, a suitable temperature range, pH, and other environmental conditions. Very often the carbon source serves as the electron donor. A system that stimulates the biodegradation of chlorinated solvents by manipulating these requirements in the subsurface is referred to as enhanced anaerobic biodegradation or as used here, EBT.

There are several different designs of EBT systems for groundwater using various delivery mechanisms, degradation mechanisms, and electron donor or biological amendments. The appropriateness of a particular type of delivery, degradation, or amendment system will vary and will depend on the goal of the proposed project. Table 3-1 presents available mechanisms and amendments available for or used within EBT systems.

TABLE 3-1

Available Mechanisms and Amendments for EBT Systems

Typical Available Delivery Mechanisms

Dual Vertical and Honzontal Wells – injection through well screen of onented wells	Dual Recirculating Wells – injection of material via extracted groundwater and introduction through re-injection system	Direct Injection – gravity or forced injection into one or more vertical wells	Honzontal and Vertical Gas Injection Wells – injection of gases through oriented wells	Passive-Reactive Wells – direct placement of solid or cartndge at well screen or in filter pack of wells
Typical Degradation Mecha	nisms			_,
Reductive Dechlorination – reduction of CAHs through removal of chlorine atoms	Aerobic Cornetabolism – incidental oxidation of CAHs while reducing other VOCs	Oxidation – direct degradation through generation of oxygen		10000L
Common Available Amendr	nents			
Nutrients – inorganics such as ammonium chloride, ammonium sulfate, etc	Electron Acceptors – oxygen, hydrogen peroxide	Bioaugmentation – vanous species of microorganisms		

^{**}Source_ITRC, 1998

One of the objectives of the electron donor injection at the MI is to define if groundwater concentrations of regulated compounds may degrade below concentrations set by EPA Maximum Contaminant Level (MCLs) criteria, as specified in the MI ROD, within a full-scale system Table 3-2 presents the groundwater cleanup target concentrations for PCE and TCE and enhanced reductive dechlorination products. Other objectives for this EBT Treatability Study are presented in Section 4

TABLE 3-2
Groundwater Cleanup Target Levels

Analytes	Units	Federal MCLs	Maximum Reported Concentration
Tetrachlorethene (PCE)	μg/L	5	480
Trichloroethene (TCE)		5	179
Cis-1,2-Dichloroethylene		70	53
Trans-1,2-Dichloroethylene		100	164
1,1-Dichloroethene		7	170
Vinyl chloride	_l	2	0 2

μg/L micrograms per liter

4.0 Test Objectives

The EBT Treatability Study will be conducted in order to compare the effectiveness of selected electron donor materials and define the design parameters for a full-scale injection at the MI. The objectives of the treatability study and additional information required are as follows:

- Obtain additional information on the geology of the aquifer within the study areas. The
 development of detailed information on the geology of the aquifer will be accomplished
 during installation of study injection points and monitoring wells.
- Ascertain the effectiveness of electron donor addition as a remedial treatment by comparing pre-injection to post-injection CAH concentrations. Seven post-injection monitoring events are currently scheduled. Samples will be analyzed for VOC and geochemical parameters.
- Evaluate transport of electron donors within the aquifer, following injection. The
 monitoring points to be installed during this study will be installed downgradient of the
 injection location in a pattern designed to reveal dechlorination aspects along aquifer
 flowpaths
- Estimate the radius of influence of electron donors through analytical monitoring. The study monitoring wells will be installed in a pattern designed to capture as much information on the radius of influence as possible.
- Estimate time for aquifer remediation using electron donors by comparing CAH
 concentrations before and after the 6-month treatment period, against the magnitude
 and extent of the remaining groundwater plume.
- Define the effect of the injection pressure on the aquifer by measuring water and
 pressure levels in adjacent wells during electron donor injection. Equipment to
 accomplish this objective will be installed within each monitoring well prior to injection.
- Define the electron donor depletion period in the aquifer by analytical monitoring after introduction of the donors has been terminated. Seven post-injection monitoring events are currently scheduled and the sample analytical results are expected to reveal the depletion of the enhancement materials.
- Identify preferential pathways for CAH migration or retention, relative to lithology and groundwater flow A "tracer" compound (sodium bromide) will be mixed with each electron donor to provide groundwater velocity and flowpath data. In addition, hydrogeologic information will be compared to groundwater sample analytical results from each monitoring well.

5.0 Enhancement Material Selection

This section will examine several factors that will influence the selection of an electron donor for the EBT Treatability Study. These factors include the geochemistry of the aquifer, concentration of CAHs in the aquifer, dechlorination aspects of electron donors, rate of electron donor depletion, and deliverability of the substrate to the targeted portion of the aquifer.

5.1 Aquifer Geochemistry

The geochemistry of the fluvial aquifer was analyzed by CH2M HILL in 2000 while completing a Monitored Natural Attenuation (MNA) study for the Groundwater Feasibility Study (FS) portion of the MI Remediation Investigation (RI)/FS. The MNA study results were reviewed and commented on by Parsons Engineering Science (Parsons) within their Final Remedial Process Optimization (RPO) Report (Parsons, 2001). CH2M HILL revised the MNA document according to comments made by Parsons and presented the latest version within the Rev 0 Memphis Depot Dunn Field RI. Several important findings from the revised MNA study applicable to fluvial aquifer geochemistry underlying the MI are reviewed in this section.

Table 5-1 presents a summary of geochemical marker values from the fluvial aquifer underlying the MI CH2M HILL (2000), during their review of this data, concluded that limited biodegradation (primarily by reductive dechlorination) of the PCE plume in the MI groundwater appears to be occurring. The limitation on the reductive dechlorination appears to be a result of low anthropogenic or natural carbon in groundwater and elevated DO concentrations in groundwater. If the dechlorination process is to be enhanced, the general aerobic conditions (DO levels above 1 milligram per liter) will have to be altered to anaerobic conditions and the level of carbon increased. Parsons (2001) agreed with this interpretation, stating in the RPO report that degradation of PCE and TCE within the CAH plume "to innocuous daughter products is limited by the low organic carbon content in the substrate and the relatively oxidizing redox conditions."

CH2M HILL (2001) through analysis of data from other sites with active EBT studies has also determined that the presence or absence of potentially competing electron acceptors may affect reductive dechlorination of CAHs activity at a site. Reviewing data presented in Table 5-1 indicates that, other than oxygen, electron accepting nitrate is present at levels where microorganisms may use this instead of anthropogenic electron acceptors (i.e., CAHs). However, the data also show that ferric iron and sulfate are at levels supportive of reductive dechlorination, indicating that microorganisms may use CAHs for electron acceptance once nitrate levels decrease. Ferric iron was actually not reported above laboratory detection limits, however, it is important to note that ferric iron is not soluble. Also, Byl (Personal Communication, 2002) reported that the sands and clay of the fluvial aquifer in West Tennessee does contain significant quantities of ferric iron. According to Bouwer and McCarty (1984), the absence of ferric iron may lead to direct use of CAHs as an electron acceptor.

5.2 Electron Donor Description

Potential electron donors for the EBT Treatability Study can be categorized as highly soluble compounds, slow release compounds, or as direct hydrogen addition.

Highly soluble compounds

- Lactate was reported by Murt (2001) to be a successful donor for stimulating dechlorination of PCE in a "geochemically challenged" site in Nebraska. Other reports have also shown successful reduction of chlorinated contaminants with the use of lactate. Lactate is normally expected to be fermented rather rapidly to acetate and H₂, resulting in high H₂ levels that persist for only short periods as various H₂-using organisms deplete it. However, lactate may be fermented to propionate, which itself can serve as a more slowly fermentable source of persistent, low H₂ levels. Lactic acid can be prepared as very strong stock solutions to prevent microbial growth. Murt (2001) reported using 60 percent food-grade sodium lactate. The viscosity of a 60 percent solution of sodium lactate at 20° C is 38 centipoise (cp) as compared to the viscosity of water at this same temperature of 1.002 cp.
- Butyrate acid amendment in one laboratory study resulted in less methanogenesis than did amendment with ethanol or lactic acid, which generated much higher H₂ levels. Butyrate acid can be prepared as very strong stock solutions to prevent microbial growth (ITRC, 1998).
- Ethanol did not support complete dechlorination, during the short-term tests of one
 microcosm study, but was a viable donor over long-term tests because a portion was
 converted to propionic acid. Ethanol can be stored as a pure solvent to prevent microbial
 growth (ITRC, 1998).
- Molasses was the fastest acting substrate in a CH2M HILL microcosm study, but this
 substrate was also used primarily to generate methane, not to drive reductive
 dechlorination. Multiple studies reported in the literature suggest these results with
 molasses to be typical. The viscosity of molasses at 20°C is 5000 cp.

Slow release compounds

- HRC® is a proprietary food-grade polylactate ester, which breaks down to a polylactate
 ester complex when introduced into water. The HRC® degrades to lactic acid then to
 organic acids including pyruvic acid and acetic acid, releasing hydrogen along each step.
 The release of the HRC® is dissolution and time to breakdown ester dependent. The
 viscosity of HRC® at 20° C is 20,000 cp.
- Vegetable Oil has been shown in some studies to cause immediate declines in aqueous TCE concentrations, due to solubility of the TCE in the oil phase. Results of microcosm and field studies have been mixed. Evaluation of groundwater analytical results 2 months into a vegetable oil interim remedial action in Orlando indicates that groundwater quality data are relatively stable, with no upward or downward trends of CAH degradation evident but with strong indication of increasing natural attenuation. The slow release of the vegetable oil is dissolution dependent. The viscosity of soybean oil at 20°C is 69 cp.

Direct addition of hydrogen

Hydrogen sparging of aquifers contaminated with chlorinated solvents has shown
promise as a method to enhance microbial dechlorination in-situ. However, the low
solubility, explosive nature of this gas, and poor aquifer distribution have limited the
use of hydrogen as an in-situ electron donor.

5.3 Injection Site Description

Effective enhanced in situ bioremediation requires delivery of amendments to the targeted portion of the plume. Site specific characteristics that drive electron donor selection and affect the deliverability of donors include contaminant concentrations and location, hydraulic conductivity, and soil types and heterogeneities.

5.3.1 MI Southwest Corner – Treatability Study Area 1

According to the MI ROD, areas in the southwest corner of the MI were chosen as the site of the EBT Treatability Study (Figure 5-1). These areas were chosen because existing data indicated that higher and more persistent levels of VOCs concentrations are found in the underlying groundwater. Table 5-2 presents the VOC groundwater sample analytical results from the MI RI (CH2M HILL, 2000) for monitoring wells and piezometers that are present in this area (i.e., MW-21, MW-22, MW-47, and PZ-04; see Figure 5-2). Additional monitoring wells MW-100, -101, and -102 have been installed in this area as part of the recent LTOA investigation efforts. Groundwater samples collected from these newly installed wells and the results of that sampling are summarized in Table 5-3.

As presented in Table 5-2, groundwater sample analytical results from the MI RI for monitoring wells MW-21, MW-22, MW-47, and PZ-04 indicate that the magnitude of PCE and TCE concentrations in on-site wells MW-21 and MW-22 have been fairly consistent over the sampling period and that, when analyzed for, the degradation product cis-1,2-dichloroethene is present. Concentrations of PCE have ranged from an estimated concentration of 2 μg /L to 120 μg /L. FCE concentrations have ranged from an estimated concentration of 2 μg /L to 39 μg /L. Offsite monitoring well MW-47 and piezometer PZ-04 has revealed that southwest of the MI relatively high concentration slugs of PCE have migrated through the fluvial aquifer. PCE was detected at 200 μg /L in a March 2000 sample from MW-47. Sampling of MW-47 since then has revealed PCE at only estimated levels less than 1 μg /L

Groundwater analytical data for Treatability Study Area 1 has been recently supplemented with analytical data from the 2001 LTOA investigation (Tables 2-1 and 5-3). Results from LTOA monitoring wells MW-100 and MW-101 indicate that contamination by PCF and TCE of this area of the fluvial aquifer is greater than previously known. Specifically, in MW-101, PCE was revealed as high as $530\,\mu g/L$, a concentration approximately 4.5 times greater than previously detected in MW-21. In addition, the contamination appears to be spread throughout the aquifer, not just within the lower portion of the aquifer, and is, on average, at higher concentrations in the center of the aquifer

Average depth to water in Treatability Study Area 1 is approximately 99 ft below ground surface. The aquifer is estimated to be approximately 35 ft thick and bounded by an

underlying clay. Hydraulic gradient for the area, as measured from MW-22 to MW-101, is 3 3E-03 ft/ft. The hydraulic conductivity for monitoring wells MW-21, MW-22, and MW-47, as reported in the MI RI, were found to be 1 7E-02, 9.4E-03, and 7 7E-03 centimeters per second, respectively, which is equal to 48, 27, and 22 ft/day, respectively. These values correspond to hydraulic conductivities reported by Driscoll (1989) and Fetter (1988) for a well-sorted silt and sand with groundwater. As reported in the MI RI, the fluvial aquifer in the southwestern corner of the MI is composed of gravel with clay silt or sand. Assuming an effective porosity of 30 percent and an average hydraulic conductivity of 32 ft/day, groundwater flow in this portion of the fluvial aquifer is, on average, 0 35 ft/day or approximately 128 ft/year.

5.3.2 MI Southeast Corner – Treatability Study Area 2

The groundwater sample data presented in Tables 2-1, 5-2a, and 5-3 reveal that groundwater contamination in the southeast corner of the MI is comparable to contaminant levels in the southwest corner. As a result, one of the study areas will be placed in this location, specifically the area centered around monitoring wells MW-86 to MW-92 (Figure 5-3).

Average PCE concentrations detected in monitoring wells installed during the LTOA investigation in the southeast corner of the MI (i.e., MW-85, -86, -88, -92, and -96) were found to range from below laboratory detection limit to 198 μg /L in monitoring well MW-86. The highest concentration of PCE detected was 280 μg /L in MW-86. Average TCE concentrations in these same wells were found to range from below laboratory detection limit to 23 μg /L in monitoring well MW-85. The highest TCE concentration was revealed within MW-85 at 26 μg /L. The wells in Treatability Study Area 2 also contained significant levels of cis-1,2-DCE, the highest average concentration was revealed at 53 μg /L in MW-86. Also, carbon tetrachloride was revealed as high as 140 μg /L in MW-85. An additional finding of the analytical data is that, just as in Treatability Study Area 1, contamination by CAHs is spread throughout the entire thickness of the aquifer, but is, on average, at higher concentration in the central portions of the aquifer.

Average depth to water in Treatability Study Area 2 is approximately 99 ft below ground surface. The aquifer is estimated to be approximately 13 ft thick and bounded by an underlying clay. Hydraulic gradient for the area, as measured from MW-86 to MW-26, is 7.8E-03 ft/ft. The hydraulic conductivities for monitoring wells MW-25, MW-26, MW-50, and MW-52, as reported in the MI RI, were found to be 2.7E-03, 1.6E-03, 2.9F-03, and 5.9E-03 centimeters per second, respectively, which is equal to 7.6, 4.5, 8.2, and 16.7 ft/day, respectively. These values correspond to hydraulic conductivities reported by Driscoll (1989) and Fetter (1988) for a well-sorted silt and sand with groundwater. As reported in the MI RI, the fluvial aquifer in the southeastern corner of the MI is composed of gravel with clay silt or sand. Assuming an effective porosity of 30 percent and an average hydraulic conductivity of 9 ft/day, groundwater flow in this portion of the fluvial aquifer is, on average, 0.23 ft/day or approximately 85 ft/year.

5.4 Electron Donor Decision Summary

The Defense Logistics Agency decided that vegetable oil could be used as one of the reductive dechlorination substrates, based upon the results of the June 2001 Final Remedial Optimization Report developed by Parsons Engineering Science, Inc. (Parsons) for the Memphis Depot. The decision was based on the successful enhancement of reductive dechlorination by vegetable oil at other sites with underlying aquifers contaminated by CAHs, as reported by Parsons (personal communication, 2002). CH2M HILL has also used vegetable oil as a substrate at several sites and has reported little to moderate reduction in contaminant levels as a result. An emulsion of vegetable oil (specifically food-grade soybean oil) and liquid lecithin (a food grade surfactant) as supplied by Central Soya Company of Fort Wayne, Indiana will be used as an EBT electron donor source in Treatability Study Area 1

A process of elimination was used to determine the second substrate based on data collected from other enhanced reductive dechlorination sites. Several factors important to the decision making process included use of substrate at other sites, contaminant concentrations at the EBT Treatability Study in comparison to other sites, aquifer characteristics versus viscosity of the substrate, equipment required for delivery of the substrate, and general success level at other sites. Table 5-4 presents the summary of this data analysis and comparison. Based on these factors, hydrogen sparging was eliminated due to the complexity of donor delivery. High viscosity substrates such as HRC® and molasses were eliminated, due to depth to the water table and potential distribution problems in a matrix with a clay content. Although lactate, butyrate acid, and ethanol are all considered effective, consistently fast and effective results were reported in both field test and microcosm studies with the lactate. Therefore, lactate in the form of 60 percent sodium lactate as supplied by JRW. I echnologies of Lenexa, Kansas has been chosen as the second electron donor substrate for the field evaluation. The lactate will be injected at Treatability Study Area 2.

6.0 Experimental Design and Procedures

This section describes the activities and processes required to complete the EBT Treatability Study and to meet the study objectives. The effectiveness of reductive dechlorination through addition of vegetable oil will be evaluated against the effectiveness of lactate, based on groundwater data collected from test sites.

6.1 Overview

The design and execution of enhanced bioremediation must reliably distribute the electron donor through the treatability study test area, without displacing contaminated groundwater within the testing zone with injected solutions. Options for application of the vegetable oil emulsion and lactate include:

- Dual Well or Trench Recirculation extraction and reinjection of groundwater through groundwater wells
- Injection Only Systems injection through groundwater wells or direct push points

Based on the depth to groundwater and concentrations of VOCs, "injection only" through injection wells was selected for the EBT Treatability Study. The advantages of the injection only system alternative are that wells provide the option of electron donor addition, bioaugmentation, or a batch electron donor feed mechanism at several points in the source area or along the plume length typically at lower costs than establishing a stationary recirculation system.

Treatability Study Area 1 will be the soybean oil and lecithin emulsion test site. In Treatability Study Area 2, a substrate mixture consisting of 60 percent food-grade sodium lactate will be injected. The proposed injection point and monitoring well configuration for the two test areas are illustrated in Figures 6-1 and 6-2, respectively

6.2 Preliminary Study Activities

Table 6-1 lists the preliminary activities associated with the EBT Treatability Study Section 14 presents the schedule of activities for the study effort. Preliminary study activities associated with the implementation of the treatability study include.

- Coordination with Memphis Depot personnel on the location of utilities in the area;
- Coordination with the Depot Redevelopment Corporation (DRC) and the appropriate tenants;
- Baseline groundwater sampling event;
- Definition of the electron donor injection quantities,
- Treatability study monitoring and injection well installation and sampling;

- Designation of areas for temporary storage of equipment and materials; and
- · Site-specific security and safety concerns.

Applications will be submitted for any required drilling and groundwater injection permits. Injection of the electron donor substrate is considered to be the start of the EBT Treatability Study test period

6.2.1 Utility Locating

The field engineer will mark locations of approximately 19 additional monitoring wells and 7 injection wells at least 2 weeks prior to commencement of the activity. All locations will be approved by Memphis Depot and DRC representatives, and all utilities will be marked by a professional utilities locating service prior to the start of drilling. The preliminary monitoring and injection well locations are depicted in Figures 6-1 and 6-2 but final locations will be based on the results of the baseline groundwater sampling event (see next section) and utility locations and conditions encountered in the field. The installation of the monitoring and injection wells is the only intrusive activity planned for this field effort.

6.2.2 Baseline Groundwater Sampling Event

A baseline groundwater sampling event encompassing all existing monitoring wells (except for those recently sampled as part of the LTOA investigation) and piezometers on- and off-site of the MI will be conducted as a preliminary activity. The workplan describing the basis for this baseline event and well purging and sampling procedures is included as Appendix A (Baseline Groundwater Sampling Plan for Main Installation Monitoring Wells) to this workplan Samples will be analyzed for VOC content and several important geochemical parameters, as shown in Table 6-2.

Analytical results from this sampling event will be used to (1) establish monitoring well and injection point locations for the FBT Treatability Study; (2) provide up-to-date VOC contaminant concentration data for the fluvial and intermediate aquifer, (3) provide up-to-date geochemical parameter data for the fluvial aquifer; and (4) refine the quantity of electron donor needed to enhance reductive dechlorination within the fluvial aquifer.

6.2.3 Electron Donor Injection Quantity Determination

After analytical data from the baseline sampling event have been reviewed and tabulated, the data will be used along with other geologic and hydrogeologic data from the fluvial aquifer to define the dose of electron donor to be injected at the test areas. Factors to consider in the development of the dosage level are contaminant concentrations, effective porosity of the aquifer, aquifer matrix (i.e., sand, silt, or clay), area of influence, geochemistry of the aquifer, and delivery method.

Preliminary dosage estimates to be injected at the two test sites during the EBT Treatability Study tests are described within Section 7.0

6.2.4 Treatability Study Monitoring and Injection Well Installation and Sampling

Approximately 19 monitoring wells will be installed within the two test areas as part of the preliminary activities to serve as downgradient monitoring points from the injection zones

In addition, approximately 7 injection wells will be installed sequentially (Figures 6-1 and 6-2). Each well will be installed by Prosonic Corporation using rotasonic drilling methods. Rotasonic drilling was selected because it is the most effective method for boring advancement and well installation under the site hydrogeologic conditions. The depth to water (e.g., 95 to 105 feet below ground surface [ft bgs] on average) and geologic characteristics of the fluvial aquifer (i.e., tight sands mixed with gravel up to cobble size) may cause problems with installation of the wells using other drilling methods. Final locations of each well will be based partially on the results of a baseline groundwater sampling event scheduled to take place as part of the MIRD in February and March 2002. The procedures and specifications that will be followed during well installation are presented in Appendix B – EBT Treatability Study Monitoring and Injection Well Installation Procedures.

As shown in Figures 6-3 and 6-4, monitoring wells will be located downgradient no closer than 5 feet and no greater than 40 feet from the injection area to intercept the potential radius of influence as the injected substrate begins to migrate from each point. Each monitoring well will have no more than fifteen feet of screen and the position of the screened interval within the aquifer will be dependent upon the following: (1) thickness of the fluvial aquifer as determined by field personnel, (2) CAH contaminant distribution within the aquifer as determined by the baseline groundwater sampling results and LTOA groundwater sample analysis results, and (3) CAH contaminant distribution within the aquifer matrix as determined by soil sampling. Where applicable, monitoring wells will be set as pairs at each location. During the drilling effort, soil samples will be collected from the vadose zone wherever Organic Vapor Analyzer/Flame Ionization Detector (OVA/FID) measurements are above 20 ppm or wherever there appears to be obvious staining in the soil profile. No more than one sample will be collected from each boring. In addition soil samples will be collected from the aquifer and analyzed for TOC content. Final locations of each well will be based partially on the results of the baseline groundwater sampling event to be conducted in February and March 2002

At both study areas, the screens for monitoring wells will be set at specific zones within the thickness of the aquifer. The depth of each zone is based on a review of historical analytical data for the MI, particularly the 2001 LTOA data that indicated the entire aquifer thickness is contaminated by CAI is and the center portion of the aquifer contains, on average, higher levels of contamination than either the upper or lower portion of the aquifer. For Treatability Study Area 1, where the aquifer thickness is approximately 35 feet, screens are to be set within the upper, middle, and lower zones of the aquifer in the well closest to the injection area. This is to ensure that analytical data is being developed across the entire aquifer. The monitoring well within the upper zone will utilize a 15-foot-long screen while the remaining two zones will have wells with 10-foot-long screens only. For the other monitoring well locations in Treatability Study Area 1, the screens will be set in the central portion of the aquifer to ascertain representative changes in the contaminant and chemistry of the groundwater.

For Treatability Study Area 2, the aquifer thickness is on average 13 feet. However, based on data collected from MW-86 during the LTOA study, the aquifer can be as thick as approximately 19 feet. Therefore, screens will be placed in both the upper and lower zone for all monitoring wells. The final length of each screen will depend upon the thickness of the aquifer as defined during the drilling effort. However, no screen will be greater than 10 feet

in length. Two wells to the south of MW-86 are an exception to this. Based on hydrogeologic data from the LTOA investigation, these wells are likely to be installed within a portion of the aquifer with average thickness and for that reason will utilize 15-foot-long screens.

Injection wells will be placed perpendicular to the groundwater flow direction in each study area. Since information developed during the LTOA effort on the vertical distribution of the CAH plume in each study area indicates that contamination by CAHs is spread throughout the aquifer, the screen interval for each injection well will be set across the entire thickness of the aquifer. However, for Treatability Study Area 1, the well screens will be placed 10 feet below the top of the water table to hinder possible "floating" of the injected substrate

Monitoring and injection well points will be sampled after each has been developed as a baseline event prior to injection of the electron donor substrate. The samples will be collected and analyzed according to the procedures presented in Appendix A and list of parameters shown in Table 6-2.

6.2.5 Other Preliminary Activities

Prior to commencement of field activities, CH2M HILL representatives will contact personnel at the Memphis Depot and DRC to locate temporary storage facilities that will be accessible during the entire 6-month testing period. The facilities will be used to store field equipment required for sampling activities or other well maintenance tools. During the discussions with the Memphis Depot and DRC personnel, site-specific security and safety of personnel and equipment will be reviewed. The information gained from these discussions will also be included within the site-specific Health and Safety Plan for further reference

6.3 EBT Treatability Study Process

The EBF Treatability Study will begin with introduction of the electron donor substrate into the fluvial aquifer via injection points and will conclude with the last groundwater sampling event at the end of a 6-month monitoring period.

6.3.1 Substrates and Tracer

As stated in Section 5.4, the electron donor substrates will consist of an emulsion of vegetable oil (specifically food-grade soybean oil) and liquid lecithin in Treatability Study Area 1 and lactate in the form of 60 percent sodium lactate as the second electron donor substrate at Treatability Study Area 2. The electron donors are available commercially Quantities of substrate are presented in Section 7.0

In addition to the substrate, a tracer will be injected that will allow for monitoring of the movement of groundwater away from each of the injection wells. Sodium bromide, a salt with high solubility in water, will be used as the tracer and will be mixed with both of the electron donors prior to injection. Once injected, the bromide ion will be analyzed for in all groundwater samples collected from the downgradient monitoring wells

6.3.2 Substrate Injection Method

6.3.2.1 Substrate Preparation

The preparation process will begin with the loading of potable water from the City of Memphis into onsite mixing tanks. A temporary water meter will be obtained from the city for this purpose. The water, which is free of turbidity and potential contaminants, will be used to mix with each electron donor. The vegetable oil emulsion mixture and sodium lactate that is brought to the site will be placed within the storage tanks for initiation of the mixing process. In addition to the substrate, a tracer will be injected that will allow for monitoring of the movement of groundwater away from each of the injection wells. Sodium bromide, a salt with high solubility in water, will be used as the tracer.

Prior to injection, the in-tank mixers will be activated to properly mix the soybean oflecithin mixture or sodium lactate, the bromide tracer, and water in preparation for injection.

6.3.2.2 Substrate Injection

The electron donor substrate will be injected into the fluvial aquifer via the 2-inch-diameter injection wells. The fluids will be pumped by a Watson Marlow SPX-40 high-pressure hose pump capable of producing 20 gallons per minute, down through the well casing, and through a 2-foot "travelling screen block". The pumping will beginning at the bottom of the well and move upwards, pushing the electron donor out into the fluvial aquifer at an approximate rate of 3 gallons per minute. Prior to injection of the vegetable oil emulsion, a high shear mixer will be used to form a micro-emulsion of each fluid with droplets less than 10 micrometers in diameter.

Pressure gauges connected to the injection pipeline will allow observers at the surface to note the amount of resistance to the fluid being pumped into the aquifer. Injection pressure is expected to be less than 100 pounds per square inch. The pumping will continue until the prescribed quantity of substrate has been pumped into the aquifer. Current estimated quantity to pump into the injection wells is 21,138 gallons in Treatability Study Area 1 and 10,569 gallons in Treatability Study Area 2 (see Section 7). Water obtained from the fluvial aquifer will be used to flush the remaining electron donor from the injection pipeline.

Assuming the volumes of emulsion/water mixture and volume of water flush can be successfully injected into the formation equally and radial along the entire length of the injection screen, and assuming a 30 percent effective porosity in the fluvial aquifer, the column of substrate formed in the aquifer should be approximately 10 feet in diameter around each injection well. The effective soybean oil/lecithin saturation in the subsurface after injection is complete is targeted at 25 percent of the effective porosity. For the sodium lactate, this target is 15 percent of the effective porosity.

During the course of injection, water samples from downgradient wells will be monitored to check for emulsion/water breakthrough. The presence of phase-separated oil emulsion in each well and the impact on the groundwater table will be measured with an oil-water interface probe. The presence of soybean oil or soybean oil emulsion in each well will also be checked visually using by collecting samples with a clear polyethylene bailer

6.3.3 Performance Verification Monitoring

After the electron donor has been injected into the fluvial aquifer, a period of time will be required before an increase in the enhanced bioremediation process can be confirmed. During and after this process, CH2M HILL will collect groundwater samples from each test area monitoring well. Samples will be collected on a bi-weekly basis for the first month and monthly for the next 5 months from each treatability study monitoring well and existing monitoring wells, where applicable Sample collection methods will be the same as those presented in Appendix A Samples will be analyzed for VOCs as well as several geochemical parameters, as described in Table 6-2, by Kemron Analytical Services.

6.3.4 Bioaugmentation

A number of microorganisms can be used to promote the reductive dechlorination process if the system does not proceed past the degradation of a daughter product. For example, if PCE were degraded to cis-1,2-dichloroethene but not degraded beyond that to other products such as vinyl chloride to ethene, then microorganisms could be added to the system to enhance the process. For the fluvial aquifer, the need to bioaugment may occur because relatively high levels of DO may keep the system aerobic or the system may only have limited amounts of microorganisms that exist in an aerobic environment. Anaerobic dechlorinating microorganisms that may be applicable include *Dehalococcus ethegenes* strain 195 or the Pinellas-type.

In most cases, such bioaugmentation results in the establishment of non-native bacterial populations that decrease within days or weeks due to competitive pressures or other environmental factors. At this time, there are no plans to implement bioaugmentation at either test area, however, if this approach is instituted, an addendum to this workplan will be submitted to the BCI for review and approval.

7.0 Equipment and Materials

Other than standard field equipment necessary for field activities, the field equipment required for the implementation of the EBT Treatability Study will include a drilling rig to install the monitoring and injection wells and pumps and ancillary equipment to inject the electron donor substrate. Groundwater sampling equipment is described in Appendix A. Additional materials necessary for this project include the quantity and type of electron donor substrate.

Monitoring and injection wells will be drilled via rotasonic drilling techniques. Rotasonic drilling was selected because it is the most effective method for boring advancement and well installation under the site hydrogeologic conditions. The depth to water (e.g., 95 to 105 feet below ground surface [ft bgs] on average) and geologic characteristics of the fluvial aquifer (i.e., tight sands mixed with gravel up to cobble size) may cause problems with installation of the wells using other drilling methods. Also, heaving sands and gravel up to cobble size have caused serious problems for hollow-stem auger equipped rigs at the Depot in the recent past. Air rotary style drilling has not been used because of the heaving sand problem. Mud rotary style drilling might be applicable in some instances, however, the time spent handling investigative derived waste and generating fluids for the drilling process decrease the likelihood of using this drilling method

The method of injection will be the same for both test areas and will include the use of a Watson Marlow SPX-40 high-pressure hose pump capable of producing 20 gallons per minute effectively delivering the substrate to the subsurface. Prior to injection, the material will be mixed in an onsite mixing tank. For further mixing and shearing of the soybean oil/lecithin electron donor, a high shearing mixer will be placed in the injection pipeline to form a microemulsion

Tables 7-1 and 7-2 present the preliminary estimates for the dose of electron donor substrate to be injected at both test sites. The total quantity to be injected was based on the highest level of PCE detected to date, $530\,\mu g/L$. An electron donor substrate dosage of four times the highest contaminant level was estimated as the quantity required to stimulate the reductive dechlorination process. Therefore, the minimum substrate concentration in groundwater after injection into the aquifer will not be less than $2\,m g/L$.

8.0 Sampling and Analysis

The sampling and analysis procedures presented below outline required activities associated with the EBT Treatability Study to define its effectiveness in decreasing CVOC concentrations in groundwater underlying the Memphis Depot. In addition, the information below outlines locations, frequency, and analyses for soil and groundwater to be collected during and after installation activities and system operation as well as analyses required for disposal characterization for wastes generated during removal activities.

8.1 Data Quality Objectives

The data quality objectives (DQOs) detailed in Table 8-1 are established to achieve objectives outlined in Section 4

TABLE 8-1
Data Quality Objectives

Data Quality Objectiv	es		
Objective Vertical profile of CAH distribution Electron donor effectiveness	Qualitative DQO	Quantitative DQO	Method to Obtain DQO
Objective Vertical profile of CAH distribution	Develop vertical profile of CAH distribution within fluvial aquifer	Analyze groundwater samples collected during baseline and monitoring events Analyze all by SW-846 Method 82608 In addition, analyze groundwater samples for geochemical parameters	Collect groundwater samples from monitoring wells during site-wide groundwater baseline sampling event, samples from injection and monitoring wells during baseline event, and samples from monitoring wells during periodic monitoring events
	Companson of CAH levels prior to injection to CAH levels post-injection and comparison of parent/daughter ratios of CAHs from previous to subsequent injections	Compare results of groundwater sample analysis for VOC and geochemical parameters for pre- and post-injection samples	Collect groundwater samples from monitoring wells in pre- and post-injection events and analyze according to SW-846 Method 8260B and geochemical parameters. Obtain results and compare in tabular form
Evaluate transport of reductive dechlorination enhancement materials within aquifer	Develop understanding of concentration changes and flow patterns within aquifer	Analyze downgradient groundwater samples results for CAH levels, geochemical parameters, and groundwater tracer	Inject groundwater tracer prior to injection of electron donor substrate Install monitoring wells and collect groundwater samples according to SW-846 Method 8260B and analyze for patterns of results in each downgradient well
Estimate radius of influence	Define volume effected by introduction of electron donor substrate material	Analyze downgradient groundwater samples to determine concentration change of contaminants and geochemical parameters as well as tracer component	Install monitoring wells and collect groundwater samples according to SW-846 Method 8260B and for bromide and analyze for patterns of results in each downgradient well

TABLE 8-1
Data Quality Objectives

Objective	Qualitative DQO	Quantitative DQO	Method to Obtain DQO
Rate of reduction of CAH levels and time required for reduction to regulatory levels	Define the time elapsed since introduction of electron donor substrate and compare baseline levels of CAHs to end of test levels to provide estimate of time required to reduce entire plume to required levels	Analyze downgradient groundwater samples to determine concentration change of contaminants and geochemical parameters. Compare concentrations after end of test to baseline levels and time elapsed, and using rate of flow from tracer test, define time required to reduce entire plume to regulatory levels.	Install injection wells Install monitoring wells and collect baseline groundwater samples according to SW-846 Method 8260B. Inject groundwater tracer prior to injection of electron donor substrate. Collect groundwater samples from monitoring wells and analyze for patterns of results in each downgradient well.
Effect of injection pressures	Determine if injection of electron donor substrate results in mounding of water/substrate above static top of water table	Utilize pressure or water level transducers or depth to water measuring instrument in surrounding injection and monitoring wells to determine if mounding results from injection	Install injection and monitoring wells and prepare each with transducers connected to data logger except for injection well. Set transducers for static water level and inject material From response of water level, determine if mounding results from injection.
Depletion of electron donor substrate in aquifer	Define the time elapsed since introduction of electron donor substrate and compare baseline levels of CAHs. Also, determine if substrate continues to appear in monitoring wells as product.	Analyze downgradient groundwater samples to determine concentration change of contaminants and geochemical parameters. Compare concentrations after end of test to baseline levels and time elapsed.	Install injection wells. Install monitoring wells and collect baseline groundwater samples according to SW-846 Method 8260B. Also analyze for substrate content. Inject electron donor substrate. Collect groundwater samples from monitoring wells and analyze for patterns of results in each downgradient well.

8.2 Soil

8.2.1 Soil Core Sampling

During the drilling of each boring for monitoring and injection wells, soil cores will be collected in continuous sampling mode from land surface to the bottom of each boring. The core samples will be collected in plastic tube bags placed at the end of the core barrel subsequent to drilling each 10- to 20-foot length. The core samples will be cut open and examined for geologic characteristics immediately upon return to the surface. Headspace field screening (see field screening SOP in Technical Memorandum SA.01 – Data Collection Plan for Long-Term Operational Areas (L1OAs), Main Installation, Memphis Depot) will be conducted over each core using an Organic Vapor Analyzer-Flame Ionization Detector (OVA-FID) until the last core is removed from the boring.

Soil samples will be collected from the vadose zone wherever OVA-FID measurements are above 20 ppm or wherever there appears to be obvious staining in the soil profile. No more

than one sample will be collected from each boring. In addition, one soil samples will be collected from the aquifer from each boring and analyzed for TOC content.

8.3 Groundwater Sampling

8.3.1 Baseline

A baseline sampling event will be conducted across the MI prior to the locating and drilling of monitoring and injection wells associated with the EBT Treatability Study. All on-site and off-site monitoring wells and piezometers, except for those recently sampled as part of the LTOA Investigation, will be sampled. All samples will be analyzed for VOC content. In addition, 18 wells will be selected for geochemical analysis sampling. Additional information on this sampling event is provided in Table 6-2 and Appendix A

8.3.2 Pre-Injection

Prior to injection and after development of each of the newly installed monitoring and injection wells, groundwater samples will be collected from each location. Groundwater samples will be collected according to procedures described in Appendix A. Groundwater samples intended for analysis of VOC content will be collected through the use of polyethylene diffusion bags. Groundwater samples intended for geochemical analysis will be collected by a low-flow bladder pump system. All groundwater samples for VOC analysis will be analyzed according to EPA Method SW8260B.

8.3.3 Post-Injection

Seven groundwater sampling events will take place after the electron donor substrate has been injected into the fluvial aquifer. The first two events will be bi-weekly followed by monthly events for the next 5 months. Groundwater will be sampled from each EBI monitoring well and samples will be analyzed for VOC and geochemical analyte content (Table 6-2). Sampling procedures will be similar to those described in Appendix A except that collection of the diffusion bags will take place on a 2-week basis instead of three

In addition to collecting samples for VOC and geochemical content, samples will be collected for electron donor substrate or breakdown product distribution in the aquifer, including

- Metabolic acids to detect lactic acid
- EPA Method 1664 to detect soybean oil.

9.0 Data Management, Analysis, and Interpretation

9.1 Data Description

Information generated from the EBT Treatability Study will include geologic, hydrogeologic, and geochemical data. In addition, biologic information may also be generated if bioaugmentation procedures are implemented during the study. Geologic data will be derived from the installation of monitoring and injection wells and will include:

- Lithologic and stratigraphic characteristics of the loess and fluvial deposits that overlie
 the fluvial aquifer;
- Lithologic and stratigraphic characteristics of the fluvial aquifer.

Hydrogeologic data will derive from review of samples collected for analysis of the groundwater tracer that is to be injected prior to start of the injection phase. The data will include definition of the groundwater flow rate within the fluvial aquifer. Geochemical information from this study will derive from analysis of all groundwater samples collected for VOC and geochemistry. These data are critical for determination of the effectiveness of enhanced bioremediation in the fluvial aquifer. If necessary, biologic information will also be gathered during the study and will reflect the type of microorganisms present in the aquifer as well as the type required for augmentation.

9.2 Data Management

Data management for the EBT Treatability Study will match the requirements of the DQOs presented in Section 8. Most of the field data will be obtained through the efforts of field screening, which includes use of direct-reading instruments, and laboratory analysis of samples. The information presented in this section is considered supplemental to the *Final Generic QAPP* for the Memphis Depot activities

9.2.1 Sample Numbering System

During sampling events conducted for the EBT Treatability Study, nomenclature will be used to distinguish between categories of sampling events, sample locations, and, where appropriate, depth of sample collection. Sample numbering protocol will be as shown in Table 9-1.

TABLE 9-1 Sample Numbering Protocol

Sample Event	Type of Sample(s) and Location	Sample Number Description	Example Sample Number
Baseline Groundwater Sampling for VOCs and Geochemistry	Groundwater; Sitewide across Main Installation	For VOC samples, sample numbers will reflect depth of diffusion bag sampler located in each well. Samples for geochemistry will reflect sample location only	For VOCs. MW92_95- 100-BL. For Geochemistry MW92-BL
Monitoring and Injection Well Installation	Soil, In both study areas	Samples will reflect location and depth of sample collection	MW109_100-110 MW110_110-120
Baseline Sampling of Monitoring and Injection Wells	Groundwater, In both study areas	All samples will have an EBT-B designation to reflect this baseline event. For VOC samples, sample numbers will also reflect depth of diffusion bag sampler located in each well. Samples for geochemistry will also reflect sample location only.	For VOCs MW92- EBT-B_95-100 For Geochemistry MW92-EBT-B
Treatability Study Sampling Events of EBT Monitoring Wells	Groundwater, In both study areas	All samples will have an EBT-TS designation followed by an number (beginning with 1) reflecting the sequential sampling events. For VOC samples, sample numbers will also reflect depth of diffusion bag sampler located in each well. Samples for geochemistry will also reflect sample location only.	For VQCs MW92- EBT-TS-1_95-100 For Geochemistry MW92-EBT-TS-1

For Duplicate samples, a "D" will be inserted at the end of the sample number. Matrix spike/matrix spike duplicates will be denoted with an "MS/MSD" at the end of the sample number. Equipment, field, and trip blanks will be designated with "EB", "FB", and "TB", respectively.

9.2.2 Field Screening Data Management

Field screening efforts will include ambient air screening around monitoring and injection wells with an OVA-FID and screening of groundwater during purging procedures with portable direct-reading instruments. The data collected from these instruments will require the full attention of the operator to ensure that reported values are not misinterpreted or misunderstood. Data that will be recorded with each measurement include the following

- Date and time;
- Elapsed time since test began, as necessary;
- Location of measurement/location where the sample was collected, as necessary, and
- Instrument measurement.

Each measurement will be handwritten into a bound field notebook and, after the entire test has been completed, the data will be transferred into an electronic file for use within the EBT Treatability Study report.

Other field notes to be collected during performance of the Treatability Study and written in the field notebook(s) include: weather information; personnel present during onsite activities; subcontractor names and activities; sketches of the test system used during the study, notes on the proximity of the system to established facilities within the MI; and all other pertinent information that may effect study results. This information will be included in the Treatability Study report, as necessary.

9.2.3 Analytical Laboratory Data Management

Multiple samples will be submitted to an analytical laboratory for VOC and geochemical analysis and reporting. During collection of groundwater and soil samples, the date, time, location of sample collection, and sample number will be recorded in the field notebook. This information will be transferred, as required, to the Chain-of-Custody (COC) documents. Copies of the COC will be kept at the site until the study is over and will be transferred to the site files for record keeping.

After the analytical data have been received from the laboratory, the data will be stored electronically, summarized, and reproduced for the EBT technical memorandum. Prior to this, however, the data will be reviewed by a project chemist for quality assurance (QA). If there are any differences between the chemist's and the laboratory's review of the data, a letter report will be issued describing the differences and any potential results from the study. Electronic Deliverable Data will be delivered according to FDMS 4.0.

9.3 Data Analysis And Interpretation

The data collected during the study will be tabulated and graphed to observe trends in relevant groundwater parameters. Data collected at each monitoring location will be compiled to provide an overview of the changes that occurred throughout the test plots. In addition, a statistical analysis will be performed to determine if observed changes in measured concentrations are statistically significant. These changes will be compared to the variation observed in the water extracted from the observation well. A t-test with a 5 percent significance level (α = 0.05) will be used to compare the mean value of measured concentrations from separate sampling events

All data and resulting interpretation will be presented and described within the EBT technical memorandum and each Remedial Design document for the MI. The data will also be used as a basis for the design of the groundwater remedy.

10.0 Health and Safety

A site-specific HASP for the tasks presented herein was prepared by CH2M HILL in February 2002. Issues particular to the EBT study are discussed within the HASP. These issues may include but not be limited to the following.

- Groundwater Sampling: Use of Pumping Equipment The use of equipment to obtain samples includes air-operated bladder-type pumps, electrical generators, tubing, diffusion bags, and portable direct-reading instruments. The work will require effort around potentially hazardous environments and will require controls on ambient air hazards.
- Monitoring and Injection Well Installation: Drilling The installation of wells at the MI will require the use of rotasonic equipped drill rigs. The use of this equipment has inherent hazards, including rotating mechanical equipment, potential hazardous atmospheres, noise, and potential slips, trips, and fall possibilities.
- Soil Sampling Soil from the fluvial aquifer may potentially contain levels of VOCs hazardous to personnel exposed to the vapors. Screening with field equipment will be necessary to keep the hazards below action levels.
- Ambient Air Monitoring Action Levels The existing HASP provides action levels for upgrading levels of personnel protection from Level D to Level C and LEVFI. B However, employing engineering controls to prevent VOC emissions is preferable to using personnel protective equipment. If the action levels for Level D are exceeded during the operation of this study, the study work efforts will be revised for corrective actions. Actions may include changing ambient air measurement locations or bringing in equipment to reduce the hazards

11.0 Residuals Management

Waste handling will be dealt with during the Treatability Studies. Waste may be classified as noninvestigative waste or investigative/field-generated waste.

Noninvestigative waste, such as litter and household garbage, will be collected on an asneeded basis to maintain the site in a clean and orderly manner. This waste will be containerized and transported to the designated sanitary landfill or collection bin. Acceptable containers will be sealed containers or plastic garbage bags.

Investigative/field-generated waste will be properly containerized and temporarily stored at each site, prior to transportation. Depending on the constituents of concern, fencing or other special marking may be required. The number of containers will be estimated on an as-needed basis. Acceptable containers will be sealed, U.S. Department of Transportation-approved steel 55-gallon drums or roll-off box-type containers. The containers will be transported in a manner to prevent spillage or particulate loss to the atmosphere. To facilitate handling, the containers will be no more than half full when moved.

The investigative/field-generated waste will be segregated at the site according to matrix (solid or liquid) and means of derivation (drill cuttings and decontamination fluids). Each container will be properly labeled with site identification, sampling point, depth, matrix, constituents of concern, and other pertinent information for handling

Soil cuttings generated from the monitoring point installation procedures will be placed in drums or other appropriate storage devices and stored at the site. The soil will be sampled for final disposal purposes according to methods and analyses required by the accepting corporation. Once the soil analytical data have been obtained, the soil will be removed from the MI within 60 days. Previous IDW soil samples were analyzed by TCLP methods and were found to be non-hazardous. The soil did not require special procedures for transportation and disposal

Wastewater generated from well development, purging, sampling and equipment decontamination activities must also be stored at the site prior to removal from the MI. Once analytical data have been obtained, the water will be removed from the MI within 60 days. During past investigation activities at the MI, IDW water was disposed of in the City of Memphis sewer system after a temporary permit had been obtained from the City of Memphis Public Works Department. The permit provided an explanation that the water contained concentrations of contaminants similar to the effluent from the operating Dunn Field groundwater extraction system, which discharges into the City's sewer system.

12.0 Community Relations

The Memphis Depot has an active community involvement that monitors the events that occur at the Memphis Depot site as well as the MI. The EBT Treatability Study will occur with the knowledge of members of the community, many of which live just beyond the perimeter of the MI. It is imperative that this study be conducted according to the specifications presented herein and that if any changes are necessary proper notification is followed along with discussions with all stakeholders.

It is anticipated that the plans for the treatability study will be presented to the Memphis Depot Restoration Advisory Board (RAB) prior to field activities. In addition, prior to initiation of field activities, fact sheets describing the treatability test and duration of the fieldwork will be distributed to the local community members that live in the area surrounding the MI. The findings from the study will also be presented to the RAB members once they are finalized.

13.0 Reports

An EBT Treatability Study technical memorandum will provide the necessary documentation of the completed Treatability Study process. CH2M HILL will complete the technical memorandum according to the schedule presented in Section 14.0. The technical memorandum will include, but not be limited to the following

- A description of the EBT system construction and additional monitoring and injection well installation,
- Description of methods, including injection, monitoring, and sampling, enacted during the study and electron donor substrate performance;
- Field measurement methods,
- Summary of field and laboratory analytical data as presented in graphs and tables,
- Results of analysis of the analytical data via computer models, including contaminant concentrations, groundwater geochemistry, change in contaminant concentration versus baseline concentrations; and
- Recommended parameters for the final design.

The EBT technical memorandum will also contain a separate section that covers the data quality and validity. At a minimum, the following information will be included in this section:

- Assessment of measurement data precision, accuracy, and completeness,
- System and performance audit results;
- Potential QA problems and corrective actions implemented, and
- Copies of documentation, such as memos and reports.

14.0 Schedule

14.1 Preliminary Schedule

The following preliminary schedule (Table 14-1) is presented for the EBT Treatability Study fieldwork and preparation of the final technical memorandum.

TABLE 14-1 Preliminary Schedule

Task	Date Completed
Submit Rev 0 EBT Treatability Study (TS) Workplan as part of the RD Workplan to the U.S. Army Corps of Engineers and BCT	January 14, 2002
Conduct Baseline Groundwater Sampling Event	February 19, 2002
Receive Comments on Rev 0 TS Workplan from Agencies and USACE	March 15, 2002
Submit Rev. 1 TS Workplan	April 14, 2002
Contact Utility Locators (Tenn Utilities Hotline at 800-351-1111)	March 30, 2002
nstall Monitoring and Injection Wells within each Treatability Study Area (Event ncludes well development and baseline sampling of each new well)	May 15, 2002
Analyze Baseline Samples of Monitoring and Injection Wells	May 25, 2002
njection of Electron Donor Substrate into Study Areas	June 25, 2002
Performance Monitoring of Substrate Effect	January 15, 2003
Conduct Laboratory Analyses of Final Groundwater Samples	January 15, 2003
Conduct Final Laboratory Data Evaluation	January 31, 2003
Prepare EBT Technical Memorandum for submittal with MI Intermediate RD report	February 15, 2003
Submit Weekly Field Status Report to USACE & BCT and Conduct Monthly Feleconferences to Discuss Field/Lab Results	February through January 2003

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Tables

Charles Char	Part Part	Analytical Lab Data (Sampled	val 8ag 7 Inderval 8ag 8 Interval 8ag 9 Interval 8ag 10 Interval PCE cts 1,2-OCE	OC) (#8TOC) (#8TOC) (#8TOC) (#8TOC) (wg/L) (110.9 My Coronentston 49 23 28 27 28 20 21	1115 1115 1115 1115 1115 1115 1115 111	23 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	110 0 12 12 15 15 15 15 15 15 15 15 15 15 15 15 15		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000000000000000000000000000000000000	115.5 117.5	44 - 08 J 10 U 10 U 10 U 10 U 10 U 10 U 10 U 10	
		Diffusion Sample	Lowery Unam Lower House Lower House Lowery Lower	100; (#810c) (#810c) (#810c) (#810c)	1029 1079 1029 1049 1069 1069 1089	101 5 103 5 105 5 105 5 107 5 107 5 107 5 109 5	63 67 69 69 69	96 100 102 102 104 108	25 26 101 101 28 28 101 101 103	106.5	855 875 805 895 815 805 895 915 835	103 5 105 5 107 5 107 5 109 5 109 5 109 5	139 141 143 145 145 145 145	935 855 89.5 87.5 87.5 99.5 101.5

Table 3-1 LTOA Diffusion Bag Sample Data VOCs Howanther & December 2000

No. 1 Merchis Dept Man beliebetin (B) Trestailly State	Total Contraction	ton (3) Treated	Py Stay Photops																					
	E B	Monitoring Well Details	Details					Diffusion S	Diffusion Sampler Details								Analydcal t	ab Data (San	Analytical Lab Data (Sampled on November and December 2001)	nber and Dec	ember 2001)			
Monthoring	Screen	Screen Interval	Depth to	Bag 1 Interval	Beg 2 Interval	Bag 3 Interval	Beg 4 Interval	Bag Straterval	Bag 6 Interval	Bag 7 Interval	A Bag 6 Interval	Bag 9 Interval	Bag 10 Interval	ğ	TCE.	c4s-1,2-DCE	E trans 1,2-DCE	DCE 1,1-DCE	CE 1,1-0CA	1,2.0CA	KA 1,1224CA	PCA Chloroform		Carbon
₩.	and C	Lome	Water	Upper Lower	Upper Lower U	Upper Lower L	Upper Lower	Upper Lower	Upper Lower	r Upper Lower	w Upper Lower	5	ş						-				Tetra	Tetrachioride
9	(ft.BTOC)	_	(m BTOC) (m BTOC)	(ABT	(n BTOC)	(ft STOC)	(R BTOC)	(ft BTOC)	(# BTOC)	(# BTOC)	(# BTOC)	(R BTOC)	(# BTOC)	(vg/L)	ਵ	(JOA)	(V60)	T/On)	-		L) (WOL	֓֟֟֟֝֟֟֟֝֟ <u>֚</u>		Į.
M 100	t07 S	127.5	3	1075 1095	1095 1115	1115 1136								= = 4	\$ 58 E	==2:		555	222	2525	777	• • • •	222	0000
							1135 1155	1155 1175	117.5 119.5				MW-100		2 2 2	2 5 5	2 2 2				- 0 0		5 5 5	
										1195 1215	1215 1235	5 1235 1255			3 6 8	222	250	777			355		222	
													125 S 127.5 Avg Concentration		2 E		0.2						- v	
MACTOR MACTOR Screens	8 <u>5</u> 5	\$ <u>5</u> 5	26 28	Low-Flow Sampling Techniques	sarbres							Upper interval Modde Interval Lower Interval	MW-101	8 2 8 0 0 0		388	200	2 2 2		3 2 3	3 2 2	2 2 2	7 2 7	2 2 2
MW 102	5051	140 5	106	120 5 122 5	360 360								Avg Concentration	_	8 0 0	500				*	5 5 5	9	<u> </u>	
	 -				_	1265 1285	128.5 128.5	285 1305					MW-102		366	222						222		
									130 \$ 132 \$	132.5 134.5	1345 1365			222		2000	222	222		2223		2000	2222	0000
-												1365 1385	138 5 140 5 Avg Concentration		0	0 0 0	>	,	v	•	6	20.	 v	
MW-103	2	8	89 43	77 07	72 74	74 78									603	0 - 0 - 0		333	D 0 0 7 1 1 0 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	10 10	007	222		5555
							P 22	78 60	29 09	23			MW-103			9 0 0		222	9 2 2	222		2 2 2 2 2		2 2 2 2
											91 79	98	88 90 And Conceptions		4 2 2 4 2 3 4 5	* * * * *	v	222			v	222		J J J J
MW 104	70.5	\$ C#	6301	70 5 77 5	77 5 745	74.5 76.5								200	60	200	555	222	30 7 0 0 7 0 0 7 0	227	222	222		2223
							(8)	78 \$ 80 \$	808 828	200			MW-104	2 2 2 2	2 4 6 6	2 6 5 6		- 6	~-					
											84.5 86.5	86.5 88.5	865 \$05 And Congression		<u>-</u>	0 0 0 0	200 7	222	4 4 8		222		***	
MW-107	128	3	11443	Low Flow Sampling Techniques	sanbita									7 01	2.8	Γ	9-	2	L	<u>-</u>	n 10	-0	50 f	Г
Somers	ž	ž											Ang Concentration	7 20 0	27	 6	° ;	5 £	<u>.</u> .		0 -		?	ر و و
MW-108	160	170	11371	Low Flow Sampling Techniques	nechee								MW-108	7 9 ₹	. 79	0.2	01	0 1	01 1 10	10	U 10	U 64	10	5

Detected concentration
 Detected concentration below detection limits
 No detected concentration below detection limits
 No detected concentration below detection limits
 Underlined and shuded values are from sample bags not s

		PCE	TCE	┝	chs 1,2-DCE	trans 1,2-OCE	1,100	3	1.1-DCA	-	1,2-OCA	-	1,2,2 PCA	Chloro	Ę	2	ş
																Tetrachloride	8
Duplicate of	Sample 10	7	3		(Mg/L)	(MOAL)	(Mg/L)	_	(Mg/L)		(165)		(100)	(00)	2	3	7
LOW 86 G	17-44-41	240	22	6	3	20			0.1	2	2.9	Ļ	101	U 85	٩	26	f
MW 92 2	MW-82-28	ŝ	4.5	•	20	0,	0.	5	•	>	-	_	•	2	4	R	
MW 93-5	05-C9-AU	5.8	07	_	0.	•	2	5	0	2	0	2	0.0	-	2	•	_
1-96-MM	BTK-86-10	•	0.7	=	0	-	2	3	•)	•	_	•	-	•	9-	
MAY 99-5	05-69-MM	10	5	3	0	01	-	3	0	_	•	5	•	5	_	-	_
MW 99-10	BEN-61-100	•	•	3	0	2	2	5	-	b	01	_	•	5	_	•	_
MW 100 8	Mry 100-60	\$	3	c	1.2	0.5	2	2	-	3	0.5	_	70	-	2	•	_
Mrw 102-8	MW 162-40	0.	2	5	0.	•	0.	3	0	2	0	_	-	9	_	•	_
MW 103-5	MW-183-50	-	7	•	•	•	-	•	~	•	0.5	_	-	2	•	•	=
								-		_					_		

Table 5-1

Geochemical Markers of the Fluvial Aquifer Underlying the MI

Rev 1 Memphis Depot Main Installation EBT Treatability Study Workplan

Geochemical Marker	Reported Range*	Background Values	Units	Biodegradation Activity?
Soluble Chloride Ion	11 - 24	10	mg/L	Supportive
ORP	145 - 238	209	mV	Not supportive
Dissolved hydrogen	1 39 - 3 13	1 19	nm/L	Supportive
Dissolved oxygen	5 45 - 7 56	6 51	mg/L	Not supportive
Nitrate	18-29	2 1	mg/L	Not supportive
Ferrous(Fe ^{2*}) iron	ND	ND	mg/L	Not supportive
Fernc (Fe3+) iron	ND	ND	mg/L	Supportive
Manganese	ND	ND	mg/L	Supportive
Sulfate/Sulfide	4 3 - 18/ND	30/ND	mg/L	Supportive
Methane	0 002142 - 0 005964	0 000067	mg/L	Not supportive
Alkalinity	45 - 90	95	ppm	Supportive
рH	5 78 - 5 79	6 17	su	Supportive
Temperature	19 96 - 21 38	18 44	degrees C	Supportive
Ammonia	ND - 0 5	0 2	ppm	Not supportive
Total Organic Carbon	ND	ND	mg/L	Not supportive
BOD	ND	ND	mg/L	
CAH daughter products	present	ND	ug/L	Supportive

*Range is reported for wells within the plume area

ORP = Oxidation/Redox Potential

BOD = Biochemical Oxygen Demand

CAH = Chlorinated Aliphatic Hydrocarbons

mg/L = milligrams per liter

mV = milivoits

nm/L = nanometers per liter

ppm = parts per million

su = standard units

C = centigrade

ug/L = micrograms per liter

Table 5-2 Summary of Mislorical Volutie Organic Compound Data Monitoring Wells MW-21, MW-22 MW-47 and P2-04 Rev. 1 Merchs Dapor As EBT Treasably Study Workson

Locati	Location 1D	P0204	MW21	LEW21	LRS231	, CANA	1000	100000	
Date Collected	ected	1./03/1996	**/18/1993	02/10/1996	06/20/1997	7007/1997	5	10.19.701	03055000
Paremeter Name 1, F.	r.: Unna	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	7 7 7 7	37 37 6 79 56	50 - 17 To 12	1 1 1 1 1 1 1 1		V. 5. 1.	
1122 TETRACHLORCETHANE	γ	o ⊗5 L	2 100	0.50	71.00	ŀ	11100	1	
1.1 DICHLOROETHENE	호	C 000 C	0.000	⊃.5¢	200	200	200	7.66	7.7
ACETONE	정	0010	?	3316	0 100	0100	0100	500	7
CARBOND SULFIDE	٠	0 000 ∪	\$	2 E0 C	0.00	0100	100	7.00	: -
CARBON TETRACHLORIDE	7,	0 000 U	⊃.∞•	0 to 0	0100	2100	200	0 60	, 7
CHLOROFORM	ş	0 000	0.00	0 01 0	0 100	2100	0.00	0.00	
cs 1.2 Dichloroby ene	ş	:	•	2	2	2	5	,	
cs 130 CHLOROPROPENE	Ę,	n 500 c	2.00	0 21 0	0.21.0	n.00	0 000	0.100	
STYRENE	성	0 200 D	:	0 00	0.010	0.00	0.00	0.00	2
"ETRACHLORCETVIVLENE(PCE)	ξ'n.	\$:	25	3	62•		-0.2	
"O"AL 12 DICHLORCETHENE	ģ	0 000	2	0.50	0.50	0.100	0 00 0	. 7	: 2
Kans 12 DICHLOROETHENE	દુ	7	0.00	•	2	2	2		•
PRICHLOROETHYLENE (TCE)	ğ	0 000	4 42•	2	•	120	•	;	•

Location ID		VW22	WW22	MW22	WW22	MW22	ZZMIN	WW22	L0W22
Data Collected	ected	11/17/1993	11/17/1983	02/10/1996	06/19/1997	09/25/1997	03/28/1998	10/19/1908	000000
1. 1. 3. 3 Parameter Name 13,35.55	UNITE	現れたよう。	4 . 18 . 24	せんさん	一年後によって 1をまし	4.7 1	南方をの一をないというとして、	-402	1. A. C. C.
1 1.2.2-TETRACHLOROETHANE	'n	0 100 0	0.000	0 100	0000	2 103	0.010	0 10 0	1
1 NO CHLORDETHENE	ት ት	D 100 0	0.000	0 CT U	0.00	2.63	0 10 0	0.00	2
ACE TONE	કુ	2	2	0 10 0	0 100	0 100	0 10 0	U 100	- S
CARBON DISULFIDE	ż	2	2	001 L	0 60	0010	0 10 0	O 100	710
CARBON TETRACHLORIDE	支	0 001 U	0.000	C 01 U	0 100	0 00 0	٥٥، د	0.00	2
CHLCROFORM	정	0.000	0.0010	0 100	0.000	2100	0 S. L	ر د.د	2
cs 12 Ochbrohy ene	ዿ	2	ŧ	7	7	2	2	:	180
Car 3 D CHLOROPROPENE	亥	0.000	n .00 o	0 10 0	3010	0016	0.55	0 100	2
STYRENE	奏	:	2	0 10 0	3010	J 100	7.00	0.00	2
TETRACHLOROETHYLENE(PCE)	ğ	۰۵۰ د	2.800	2	0 100	2	0.00	0 10 0	760
TOTAL 12 DICHLOROETHENE	섫	2	2	0010	0 00 0	0 01 C	200	0 10 0	7
9911 1 2 DICHLOROETHENE	성	3 001 L	2.000	2	2	ŧ	:	•	2
TR CHLOROETHYLENE (TCE)	υgγ	1 24=	0.000	2	2	3	7	0 100	

TRICKLORUSE INTERFERENCE (INTERFERENCE)

J. Behmend de action Contentian defected at or before intorestory despon that if a nor intuded in stall of analysis.

Oi noteson	O u	WW47	F-W47	MW47	MV447	MVV47	NV/47	MW47	VW47	MW47
Date Collected	cted	02/09/1996	06/22/1997	09/26/1997	03/28/1998	8661/6./0.	03/23/2000	03/09/2001	31	10000000
・・ころう Pacameter Name ストント・	mun.	-71 : "1	1 1	; ;	A STANDARD	では、このなるのでは	Т	3 3		
1122 TETRACHLOROETHANE	7,6n	0 10 2	0.00	J 100	D 001 C	0 10 0	7.	7 75 0	710	
1 1-DICH_OROETHENE	궣	0 10 0	2 63	0 100	0.00	0 01 U	2	2	2	0.
ACETONE	ž	D 60	000	0 to 0	0010	D 100	200	7.	24.1	7.6.4
CARBON DISULFIDE	Š	0 0 0	000	0 00 0	0 100	O 10 0	2	2	'n	<u> </u>
CARBON TETRACH, ORIDE	ξ	0 60 0	000	0 00 0	0.100	0 01 U	·	٠.	י מי	2 -
CHLORCFORM	ş	0 00 0	0010	0 20 0	0 100	0 000		۔ د	n.	2
ca-1 2-Cichlorothylene	ş	2	•	2	2	2	;	۸.	7	
C4+13-DICH, OROPROPENE	귷	0 00 0	0 100	0 10 0	U 100	0.000	2	- د	2	2
STYRENE	젛	0 10 0	0100) io	U 100	0 100	-	2		2
TETRACHLOROE"HYLENE(PCE)	3	å	2	•	<u> </u>	2	002	0.57	2	2 =
TOTAL 12-D CHLOROETHENE	ş	2	2000	3	2	2	2	2		: a
rare 12 DICHLOROETHENE	젛	2	2	•	•	:	2	2	2	2
TRICHLOROETHYLENE (TCE)	νcη	2	0.50	3	6.0	0 010		2		2

1899 5-2a Burnt ary of Mistorical Valeria Organic Compound Dasa Monitoring Wei is MM-23 MM-28 MM-50 and MM-44 Per I Mercent Oppo Mc EST Transcray S.c.y. Mexicon

Location ID	0	VV125	MW25	MW25	WW25	MW25	WW25
Date Collected	Peted	11/13/1993	2/9/1998	6/19/1997	9/25/1997	3/25/1998	13/16/1998
* 1. 1. Parameter Name 195 C	Units	* - KEY 7.2	; ;	A. 18. 17.	1 1 W		- 24
1122 TETRACHLORDETHANE	761	0 000 0	0.00	7.90	0 100	0010	٥٠.٥٥
1.1 DICHLOROETHENE	ş	7.000	0.00	0010	0 100	0010	0.00
ACETONE	ć	\$	0.00	0.00	0 21 U	0.00	0310,
CARBON D SULFIDE	ş	\$	0.00	000	0.00	0010	0.00
CARBON TETRACHLORIDE	ş	5000	, , , ,	.001 <u>0</u>	· : :	1	2.3
CHLOROFORM	3	2 60 2	0 00 0	0010	0 001 U	0.50	0010
Crb-1 2 Dichlorochytene	3	2			, 2	2	2
CALT 3-DICHLOROPROPENE	ş	0 193 0	200	0 10 3	0 000	0 100	0.00
TETRACHLOROETHYLENE(PCE)	ğ	11.2 -	. •		==	7	-
TOTAL 12 DICHLORDETHENE	ş	• 	0010	_ C01 U	- L.00	0.00	0010
Vans-1 2-DICHLOROETHENE	Z	0.000	12		1	1	
TRICHLORDET HYLENE (TCE)	J.	0 001 U	0010	- 0 to 0	1.00	0.010	0.00

(*) Deliving desection.

J. Eliminard defection. Consumers defected ali or below laboratory desection limit fine a rice included in it. of bring/fes.

Locati	Location 10	MW26	MW26	HW26	MW26	NW26	MW26
Data Collected	ected	179.993	2/8/1996	620/1997	9,26/1997	328/1998	10/20/1998
A Parameter Name's A	· Unite it	h- 150,	ال المراد ماركود	Att		A 17. 2. 14	¥ . 4 %, 1.X C.
1122 TETRACHLOROETHANE	No.	r.000	0 10 0	0.00	0 01 0	0 100	0 100
11 OCHLOROETHENE	ş	0 0 0 0	0 00 0	00:00	0000	0010	0 601 U
ACETONE	3	2	0.00	0.00	0010	0010	0 01 U
CARBON D SULFIDE	ž	•	00.0	0 001 U	000	0010	0 10 0
CARBON "E"RACHLORIDE	ż	3.16	7	7	7	7	7
CHLOROFORM	ş	2 100 0	Ţ	2	0 00 0	7	?
cs-1 2 Dichbrothylene	ig S	5	ŧ	2	2	2	ē
CER 1 3-DICHLOROPROPENE	궣	0.000	0.00	0 22 0	0 00 0	D 100	0 10 O
TETRACH_OROETHYLENE(PCE)	ž	9 2	1.	12.	=	÷	- 91
TOTAL 12-D CHLOROETHENE	ş	2	0.00	0 000	0 63 0	0010	O 10 0
(Mane-1 2-3 CHLOROETHENE	ş	0 000	2	ę	2	6	2
TR CH. OROETHYLENE (FCE)	ş	2.	2	72	77	77	2.7

(s, Def s) a descript.

2.8 EF mend descript. Consumment descript at or ballow laboratory, descript lamm.

As - 10t included in Fit of prasyrs.

QI uoparoon	يا يو	MWSO	MNYSO	MWSG	MWSO	NW SO	NW64
Date Collected	cted	2/11/1996	6/19/1997	9/24/1997	325/1998	10/16/1998	10/25/1998
Parameter Name 125	tijun:	12.15.2	2 7 7	* 1869; 3840	2	r 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	11-7-11
1122-TETRACHLOROETHANE	γđn	0010	r.00	0 10 0	0 10 0	0 100	7
1.1 DICHLOROETHENE	765	0 001 U	000	0.000	0010	-001 Ū	0 01 0
ACETONE	ž	0.048 U	C 10 3	0 100	0 00 0	C 01 UJ	0 00
CARBON DISULFIDE	정	000	0 100	000	0.00	0100	
CARBON TETRACHLORIDE	દુ	D 000	265	000	0 21 0	000	77
СНЕОЯЗГОВМ	성	1000	100	1000	. D160	0010	: } :
ca . 2-Cichorathy and	Į,	2	5		.	, 2	2
CHI 3-C CHLOROPROPENE	Š	00:0	000	000	U 1C 0	0010	0.00
TETRACHLOROETHYLENE(PCE)	દ્ર	0.60	0 00 0	0 00 0	0.00	0 100	10
TOTAL 12-DICHLOROETHENE	ş	0.00	0010	0010	0,010	00010	7:00
"rens 1.2 DICHLOROETHENE	3	2	2	=	. 2	; 2	?
TRICHLORGETHYLENE (TCE)	λgn	0 00	0010	0 00 0	7 60	0010	- 32

(*) Dakwa okecnon J.e Esmaket devecton. Cantamment descried al or ballon laboratory desection limit na e nos noblobel in list of enlayes

Table 5-3 Summary of LTOA Groundwater Semple Analytical Results - VOCs Ary 1 Werpha Dept Ven Intreason EBT Treatably Stof, Montan

5						50,004	And Call and Call				
	Upper to Lower Bag	PCE	TCE	cls-1,2-DCE	trans-1,2-DCE	1.1-DCE	1,1-DCA	1.2-DCA	11,2,2-PCA	Chlorotorm	Carbon
											Tetrachloride
4	,	(ng/L)	(ng/L)	(vg/L)	(vg/L)	(vg/L)	(ug/L)	(UD/L)	(na/r)	(ug/L)	(na/L)
	.00 9 to 11C 9	4	23	28	0.7	, ,		-	-	2	122
	99 S to 115 5	198	20	S		·	Ţ	36	Ţ	4	12
	81 to 97	107	2.4	£.		ţ	Ţ		V	-	
	90 to 108	8	7	99	0.7	ī	Ţ	0	V	- wi) -
	103 to 107	Ţ	•	Ţ	Ţ		Ţ		V		• 7
	108 5 to 1 · 0 5	-	ţ	ÿ	Ţ	•	Ţ		· •		
	83 5 to 95 5	Ţ	-	Ţ	-	·	-	Ţ	V		
	101 5 to 117 5	÷	60	Ţ	Ţ	Ţ	Ţ	V	-		, ,
WW-98	137 to *47	•	80	Ţ	v	Ţ		Ţ	Ţ	- 2	7 🗸
	91 5 to 109 5	Ç	- 60	Ţ	ţ	Ţ	Ţ		Ţ	. 6	
_	*07 5 to 125 5	옶	70	12	0 2	03	÷	0.5		· •	. 🗸
	.¥X	480	30	3.5	Ţ	V	V	١.	; ₹	- 20	Ţ
	120 5 to 138 5	Ţ	0.7	Ţ	Ţ	ţ	·	Ţ			
	70 to 88	Ţ	0 7	50	Ţ	1.2		60	: 7	÷	
	70 5 to 88 S	Ţ	=	90	-	-	50	V	Ţ	2	7
	Y	80	2.7	03	₹	Ţ	. 5	v	V	0.2	
MW.108	NA:	2.6	•	0 2 3	⊽	₹	Ţ	⊽	v	; ••	₹ ₹

Detected concentrations are in bode and impressed in the season beginning and performing with Detail of Heat's period can be found in Table 2.1.

These we's contain mid personal and interesting to the performance of cases.

These we's contain mid personal and interesting to the performance of cases.

The season beginning to the season of cases.

Figure and obtained containing the performance of reporting into VOCa = Votall & Organic Compounds.

Table 5-4
Practicality of Electron Donor Substrates
Rev 1 Memphis Depot Main installation EBT Treatability Study Workplan

Substrate Type	Substrate Use at Other Sites	Contaminant Concentrations vs. Concentration at Memphis Depot	Aquifer Characteristics vs. Viscosity of Substrate	Equipment Required for Delivery	Success Level
Lactate	MCLB-Albany, GA	TCE = 760 mg/L	Laboratory Test	Direct injection	Reduction of confaminant occurred after 0.5 month period
Molasses	AVCO Lycoming Superfund Site	TCE = 67 ug/L, DCE =7 ug/L, VC = <1 H gh permeability aquifer vs ug/L Low viscosity substrate		Direct in ection through injection weils	TCE and DCE levels below cleanup goals
HRC	Vanous Sites	Concentrations comparable or greater Sandy silt aquifers to sand than at Memphis Depot aquifers	Sandy silt aquifers to sand aquifers	Injection through pumping	Injection through pumping Contaminant levels vary after injection, some sites show marked decrease and show no decrease
Vegetable OII	Demo Site, Cape Canaveral FL	TCE = 100,000 mg/L, VC = 330 mg/L. Sancy aquifer, viscosity of oil Injection and dependent upon mixing Recirculation	Sandy aquiter, viscosity of oil dependent upon mixing	System	After six-month period, TCE levels decreased to 160 mg/L. Daughter product levels increased along with total VC levels
Hydrogen sparging	AFCEE - Cape Canavera. Av. Station	TCE ± 48 mg/l cs-DCE = 143 mg/L	Sandy aquifer gas - high viscosity substrate	Gas pu sed through three injection points	Gas pulsed through three Affer one week - extensive biological univation of hydrogen. Affer 4 months date indicate significant reductions in TCE and cis-DCE concentrations compared to a control point (injected with nitrogen only)

Table 6-1
List of Preliminary Activities of the MI EBT Treatability Study
Rev 1 Memphis Depol MI EBT Treatability Study Workplan

Activity	Description	Purpose
Utility Locating	Location of site utilities prior to intrusive activities.	Ensure that no service lines or other utilities may be present in the locations selected for monitoring or injection wells
Baseline Groundwater Sampling	Sampling of all exisiting on- and offsite monitoring wells and piezometers and analyze samples for VOC, metals, and geochemical parameters	Define current VOC plume configuration in the fluvial aquifer and set baseline for reductive dechlorination and long-term natural attenuation monitoring studies, as defined by the MI ROD.
Electron Donor Injection Quantily Determination	Determination of quantity required to inject into the fluvial aquifer to ehance reductive dechlorination processes.	Quantity of material to inject is vital to enhancement of the reductive dechlorination process
Monitoring and Injection Well Installation and Sampling	Install 19 monitoring and 7 injection wells in two EBT study areas using rotasonic methods Screened intervals for each type well will be located for most effective sample and injection results	Wells required as part of study activities. Sampling of groundwater subsequent to injection will be critical to define if reductive dechlorination is progressing and reducing current levels of CAHs in fluvial aquifer.
Other Field Activities (Site communications, temporary storage, security)	Communicate with DRC and personnel at Memphis Depot Business Park regarding communications, storage needs, and site security	Establish roles and chain-of- command, storage for equipment required during study, and security of equipment and personnel

Table 6-2
Analytical Protocols for EBT Samples
Rev 1 Memphis Depot Main Installation EBT Treatability Study Workplan

Matrix and Analytes	Method	Field (F) or Analytical (L) Laboratory
Groundwater*		-
Redox Potential	Direct-reading meter	F
Dissolved Oxygen	Direct-reading meter	F
pH	Direct-reading meter	F
Specific Conductance	Direct-reading meter	F
Temperature	Direct-reading meter	F
VOCs	SW8260B	L
Dissolved Gases (ethene,	RSK175	1
ethane, and methane)		_
Dissolved organic carbon	SW9060	L
Nitrate, nitrite	SW9056	L
Sulfate	SW9056	L
Sulfide	E376.1	L
Carbon dioxide	CHEMetrics Method 4500	F
Bromide	E320.1	Ļ
Chloride	SW9056	L
Ferrous fron	Hach Kits	F
Manganese	SW6010B	L
Alkalinity	E310 1	L
Metabolic Fatty Acids	E300 0	L
Oil in Water	SW1664	Ł
<u>Soil</u>		
Total Organic Carbon	SW9060	L
Vegetable Oil, Lactate, and		
Tracer	[
VOCs	8260B	L

^{*}Reported in sequence of sample collection

Table 7-1
Treatability Study Area 1 (MI Southwest Corner) Injection Scenario
Rev 1 Memphis Depot Main Installation EBT Treatability Study Workplan

	<u> </u>											
Well	Oil/Wate	Oll/Water Mixture	Emulsifier (agent)	Water Flush Amount	Total Volume	Final Percent Oil	Screened Radius of Emulsion Interval influence Flow Rate (feet) (feet)	Radius of Influence	Radius of Emulsion Influence Flow Rate (feet) (npm)	Emulsion Injection Time	Water Flush Flow Rate	Water Flush Flow Rate
	ō	Water			2					(hours)	(mdb)	(hours)
	(gallons) (gallons	(gallons)										
Test Area -	lest Area - Entire Aquifer	'er										
INJ-1	1762	5230	Lecithin	55	7046	25	40	2	3	39.1	~	0.3
INJ-2	1762	5230	Lecithin	55	7046	25	40	5	3	39.1	3	0.3
INJ-3	1762	5230	Lecithin	55	7046	25	40	5	3	39.1	3	0.3
	5285	15689		165	21138					117.4		6
Assumptions												;

Assumptions

1 An effective porosity of 30 percent for the fluvial aquifer

2 Fluid will be injected into two wells at the same time

3. Water for mixture will include a sodium bromide tracer as a groundwater tracer

gpm = gallons per mirute

Treatability Study Area 2 (MI Southeast Corner) Injection Scenario Rev 1 Memphis Depot Main installation EBT Treatability Study Workplan Table 7-2

Well	Lactate Mix	Lactate/Water Mixture	Water Flush Amount	Total Volume	Final Percent	Screened Interval	Radius of Substrate Influence Flow Rate	Radius of Substrate Influence Flow Rate	Substrate Injection Time	Water Flush Flow Rate	Water Flush Flow Rate
	Lactate (gallons)	Water (gallons)				()	(20)	(111.48)	(hours)	(mdB)	(hours)
Test Area-	est Area- Entire Aquifer										
NJ-4	661	1927	55	2642	15	15	5	3	14.7	٣	٥ م
NJ-5	661	1927	55	2642	15	15	2) (r)	14.7		80
9-fN	661	1927	55	2642	15	15	5	3	14.7) C	800
NJ-7	661	1927	55	2642	15	15	5	8	14.7	8	033
	2642	2022	220	10569					58.7		12

1 An effective porosity of 30 percent for the fluvial aquifer

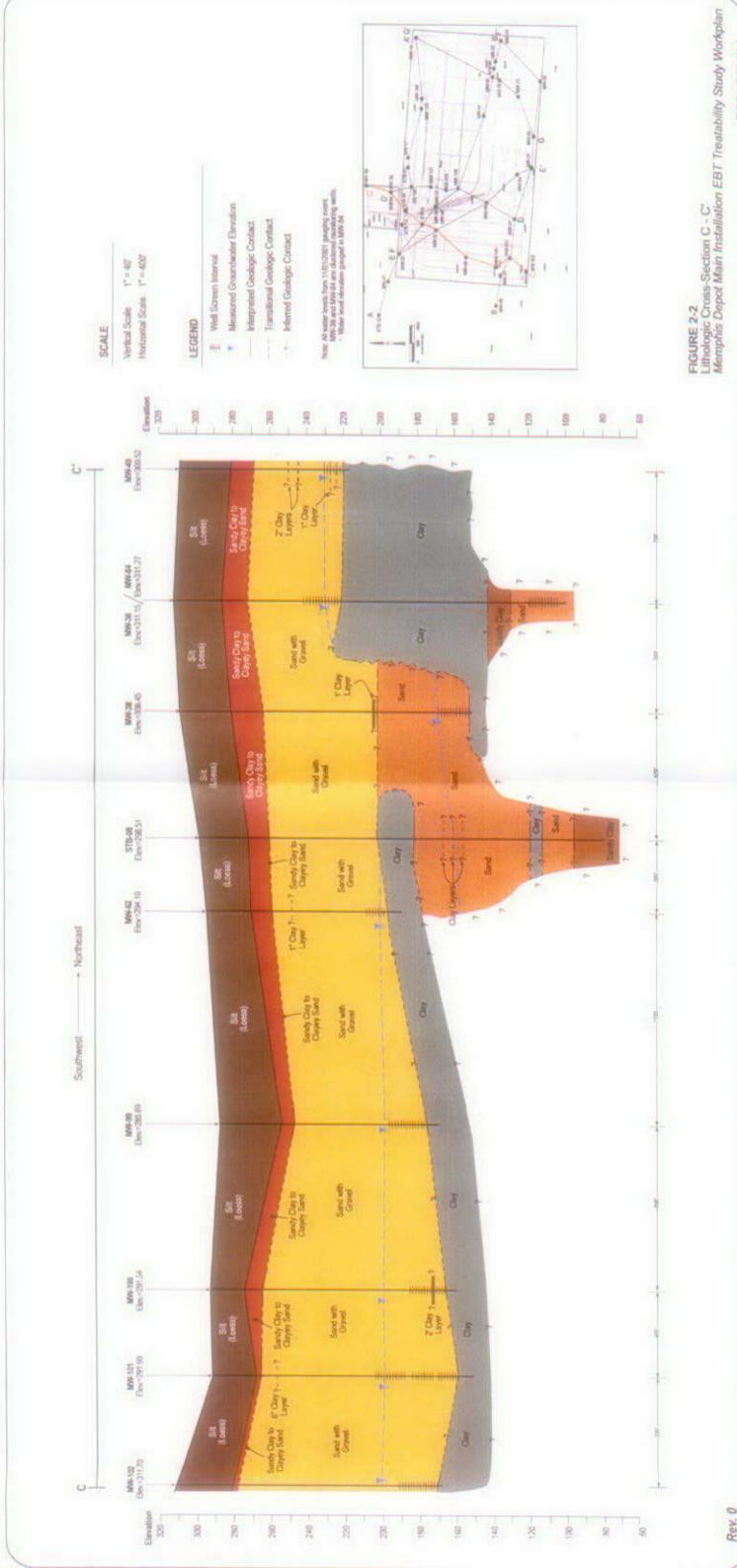
2 Fluid will be injected into two wells at the same time

3 Water for mixture will include a sodium bromide tracer as a groundwater tracer

gpm = gallons per minute

Figures





Rev. 0

CHZMHILL

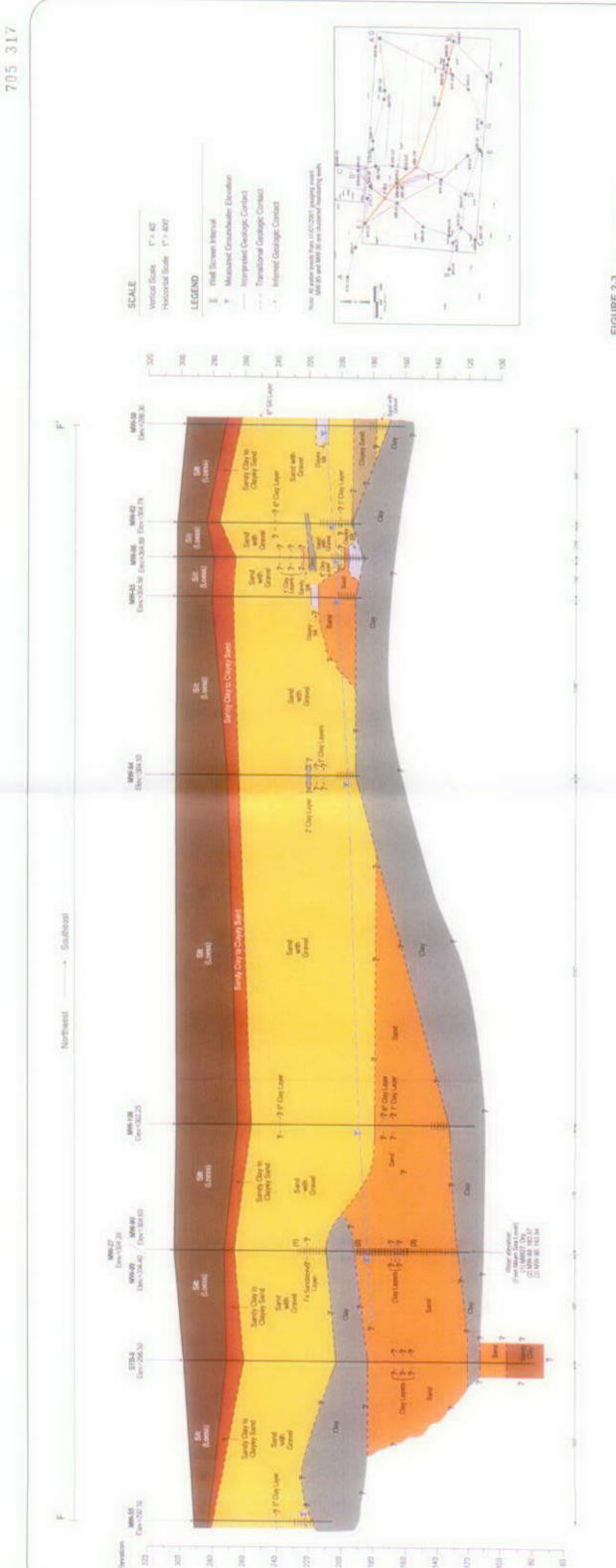
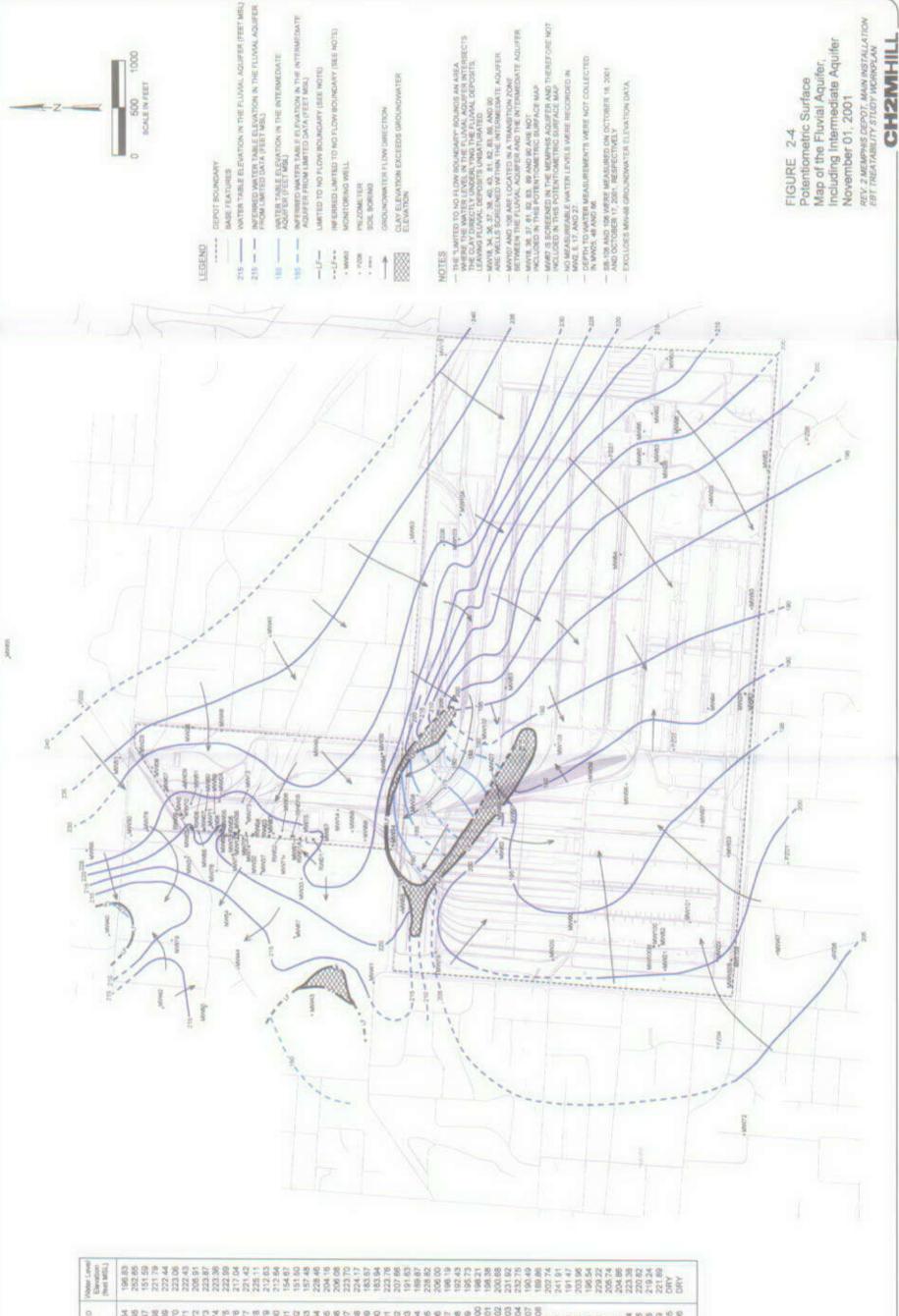


FIGURE 2-3
Lithologic Cross-Section F - F
Memphis Depot Main Installation EBT Treatability Study Workplan CHZIMHILL

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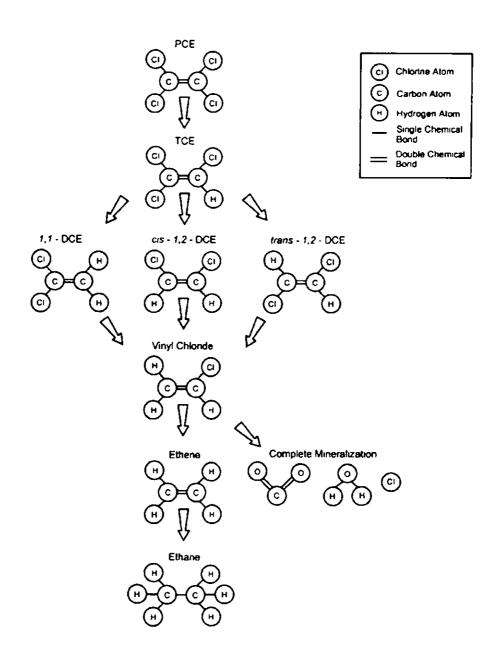
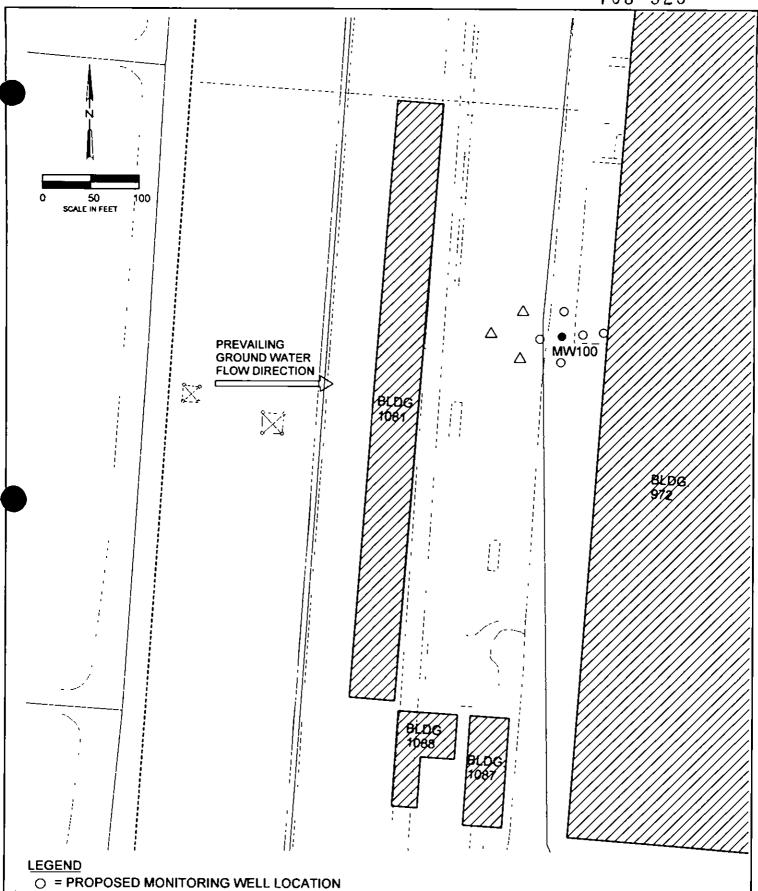


Figure 3-1
Anaerobic reductive dechlorination pathways (Wiedemeier et al 1997).
Rev. 1 Memphis Depot Main Installation EBT Treatability Study Workplan



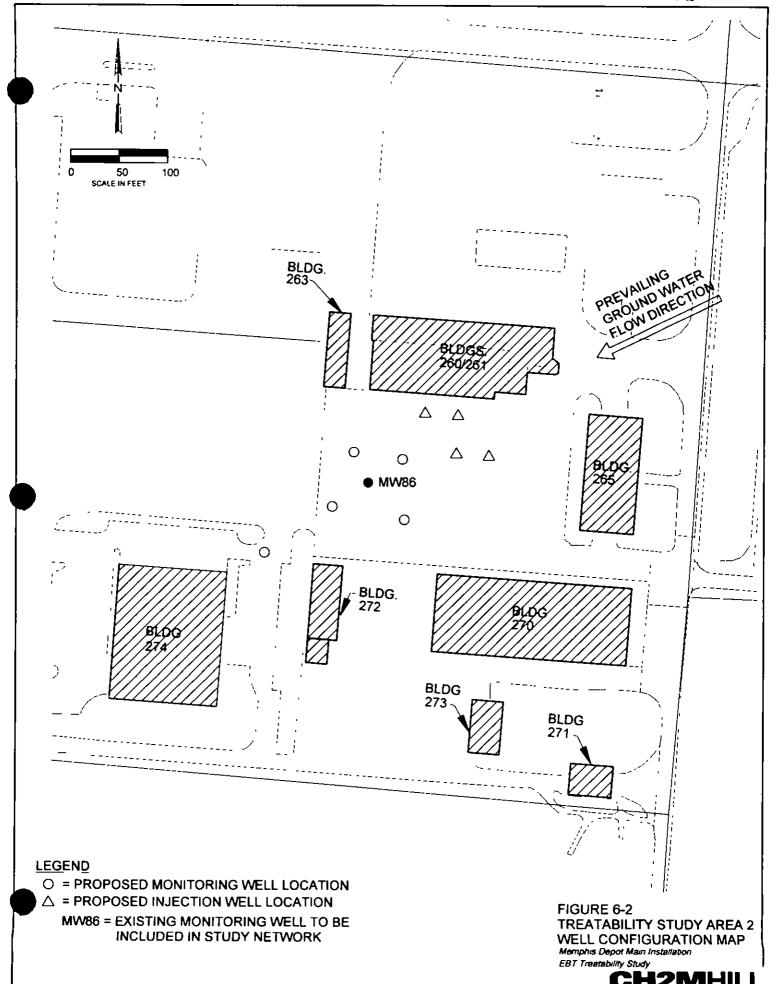


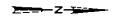


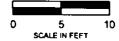
- △ = PROPOSED INJECTION WELL LOCATION
- MW100 = EXISTING MONITORING WELL TO BE INCLUDED IN STUDY NETWORK

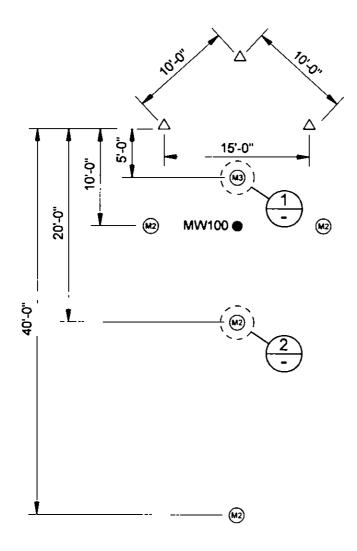
FIGURE 6-1
TREATABILITY STUDY AREA 1
WELL CONFIGURATION MAP
Memphis Depot Main Installation
EBT Treatability Study

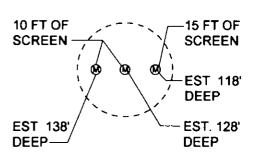
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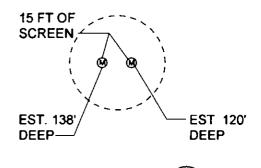








M3 DETAIL 1



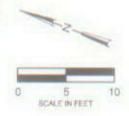
M2 DETAIL 2

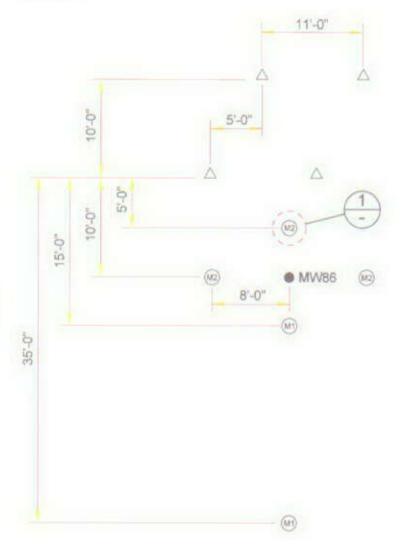
LEGEND

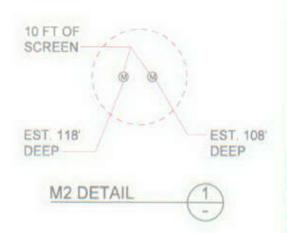
- (W2) = PROPOSED MONITORING WELL LOCATION 2 WELLS
- (M) = PROPOSED MONITORING WELL LOCATION 3 WELLS
- △ = PROPOSED INJECTION WELL LOCATION
- MW100 = EXISTING MONITORING WELL TO BE INCLUDED IN STUDY NETWORK

FIGURE 6-3
INJECTION AND MONITORING WELL
CONFIGURATION DETAIL MAP
TREATABILITY STUDY AREA 1
Memphis Depot Main Installation
EBT Treatability Study

CH2MHILL







LEGEND

- (II) = PROPOSED MONITORING WELL LOCATION 1 WELL
- @ = PROPOSED MONITORING WELL LOCATION 2 WELLS
- △ = PROPOSED INJECTION WELL LOCATION
- MW86 = EXISTING MONITORING WELL TO BE INCLUDED IN STUDY NETWORK

FIGURE 6-4
INJECTION AND MONITORING WELL
CONFIGURATION DETAIL MAP
TREATABILITY STUDY AREA 2

Rev. 1 - Memphis Depot Main Installation EBT Study Workplan

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Appendix A - Baseline Groundwater Sampling Plan Technical Memorandum

Baseline Groundwater Sampling Plan for Main Installation Monitoring Wells

TO:

U.S. Army Engineering and Support Center, Huntsville

COPIES

Defense Distribution Center (Memphis)

U.S. Environmental Protection Agency (USEPA), Region 4

Tennessee Department of Environment and Conservation (TDEC)

FROM

CH2M HILL

DATE.

January 14, 2002

Introduction

This Baseline Groundwater Sampling Plan (BGSP) has been prepared as part of the Enhanced Bioremediation Treatment (FBT) Treatability Study Workplan for the Main Installation (MI) and describes groundwater sampling activities needed in preparation for the EBI study. Recent groundwater sampling events have focused on individual sites within the MI while occurring at different periods, no complete groundwater study has been performed within the MI since October 1998. To develop a comprehensive understanding of the current groundwater contaminant extent, all pertinent monitoring wells (MW) and piezometers (PZ) associated with the MI, both onsite and offsite, will be sampled.

Subsequent to the analysis of all samples, the data from this event will be used to formulate the final quantity of electron donor substrate material to inject into the aquifer for the EBT study and other phases of the MI Remedial Design. In addition, the information gained from this sampling event will be used to define long term monitoring needs at the MI.

Objectives of Baseline Groundwater Sampling Plan

The objectives of the BGSP are to

- Collect groundwater samples from all MW and PZ locations associated with the MI.
- Analyze groundwater samples for volatile organic compound (VOC) content as well as various geochemical parameters required for an understanding of the reductive dechlorination activity in the fluvial aquifer

The analytical results will be used to: (1) define monitoring well locations for the EBT Treatability Study, (2) provide up-to-date VOC contaminant concentration data for the fluvial aquifer; (3) provide up-to-date geochemical parameter data for the fluvial aquifer, and (4) refine the quantity of nutrient source needed to enhance reductive dechlorination within the fluvial aquifer

Data Quality Objectives

The data quality objectives (DQOs) are found in Table 1 and have been established to achieve the sampling objectives. Three sampling methods will be used during the sampling event to ensure that the DQOs are satisfied and that the data is usable for the entire RD. These sampling methods have been utilized during other MI groundwater sampling events and have proven effective for data collection. Sample analysis methods are EPA-approved laboratory analytical methods.

Twenty-eight monitoring wells and five piezometers will be sampled for VOCs during this event. In addition, eighteen monitoring wells will be sampled for various geochemical parameters. Table 2 lists all MI monitoring wells and piezometers and identifies those that will be included in the baseline sampling event. Figure 1 presents the location of the sampling points. Sixteen monitoring wells were sampled for VOCs using diffusion bag samplers during the Long-Term Operational Area (LTOA) investigation (November and December 2001) and this data will be used to supplement information gathered during this baseline event. Groundwater samples will be analyzed according to methods described in Table 3.

Field Activities Methodology

Field activity procedures will follow methods described herein. The following site-specific plans should be used for further reference on applicable methods and procedures:

- Operable Units 2, 3, and 4 and Screening Sites: Field Sampling Plan Addenda (CH2M HILL, September 1998)
- Operable Unit 2 Field Sampling Plan (CH2M HILL, September 1995)
- Operable Unit 3 Field Sampling Plan (CH2M HILL, September 1995)
- Operable Unit 4 Field Sampling Plan (CH2M HILL, September 1995)
- Screening Sites Field Sampling Plan (CH2M HILL, September 1995)
- Generic Remedial Investigation (RI)/Feasibility Study (FS) Work Plan (CH2M HILL, August 1995)
- Hazardous and Toxic Waste Health and Safety Plan (CH2M HILL, August 1995)
- Generic Quality Assurance Project Plan (QAPP) (CH2M HILL, February 1995)

Groundwater Sampling

The methods and procedures used in the field will adhere as closely as possible to procedures described in the U.S. EPA Region 4 Science and Ecosystems Services Division, Environmental Investigations Standard Operating Procedures and Quality Assurance Manual (EISOPQAM), dated May 1996 (revised in 1997) as well as sampling and purging procedures presented in Low-Flow (Minimal Drawdown) Groundwater Sampling Procedures (Puls and Barcelona, 1996), Sections 7.2.2 and 7.3.3.

All VOC samples will be collected through the use of polyethylene diffusion bags. Diffusion bag samplers allow for collection of discrete water samples associated with longer screened wells. Diffusion bag samplers consist of polyethylene bags filled with deionized or distilled water, which are lowered into the well screen interval. The concentration gradient between the VOCs in the well and the water-filled bag results in diffusion of contaminants into the

sampler. Diffusion bag samplers will be located in each well as described in Table 2 Construction, installation, and sampling of the diffusion bag samplers will follow guidance developed by the U.S. Geological Survey (2001) in User's Guide for Polyethylene-Based Passive Diffusion Bag Samplers to Obtain Volatile Organic Compound Concentration in Wells. Diffusion bags will remain in each monitoring well for a three week period

Collection of groundwater samples from piezometers will differ from monitoring wells. The small diameter (0.5 inches) of the piezometer casing necessitates the use of a small diameter bailer instead of a bladder pump. Before sampling, each piezometer will have at least three well volumes purged using the bailer. Field measurements of DO, ORP, turbidity, pH, temperature, and SC will be made during the purging process until stabilization Piezometers will also be sampled using the same bailers. Each bailer will be discarded after each use.

All geochemical samples will be collected using a bladder pump system in order to minimize agitation of the groundwater and sample turbidity. The bladder pump will be equipped with high-density polyethylene (HDPE) tubing lined with Teflon® and the pump will be positioned within selected wells as described in Table 2. Field measurements of DO, ORP, turbidity, pH, temperature, and SC will be made every five minutes. These parameters will be measured using an airtight flow-through cell. Purging will continue until field measurements are stable according to the following standards, plus or minus 0.1 pH, plus or minus ten millivolts ORP, plus or minus 3 percent for specific conductance, and plus or minus 10 percent for turbidity and dissolved oxygen.

All samples will be preserved as required in Table 4 and will be delivered to a laboratory within the appropriate holding period.

In addition to groundwater samples, QA/QC samples will be collected during the field effort. The QA/QC samples include field duplicates, matrix spike/matrix spike duplicate, ambient blanks, equipment blanks, and trip blanks. The quantity of QA/QC samples collected at the site will be in accordance with guidelines in Section 5.13.11 and 5.13.12 of the EISOPQAM and as presented in Table 4.

Investigation-Derived Waste (IDW)

Purge water will be contained in drums and transferred to the Groundwater Extraction System located at Dunn Field No drums will be staged on-site.

Logistics

Equipment, supplies, and personnel required to complete the baseline sample event at the MI will mobilize after approval of this BGSP. The Hazardous and Toxic Waste Health and Safety Plan (CH2M HILL, August 1995) for Memphis Depot will be amended prior to the start of field activities.

References

CH2M HILL. February 1995. Final Generic Quality Assurance Project Plan. Defense Distribution Depot Memphis, Tennessee. Prepared for the United States Army Engineering Support Center, Huntsville, Alabama.

CH2M HILL, Inc. August 1995 Generic Remedial Investigation/Feasibility Study Work Plan. Prepared for U.S. Army Engineering and Support Center Huntsville, Alabama.

CH2M HILL, Inc. August 1995 Hazardous and Toxic Waste Health and Safety Plan. Prepared for U.S. Army Engineering and Support Center Huntsville, Alabama

CH2M HILL. September 1995. Operable Unit 2 Field Sampling Plan. Defense Distribution Depot Memphis, Tennessee Prepared for the U.S. Army Engineering Support Center, Huntsville, Alabama

CH2M HILL. September 1995. Operable Unit 3 Field Sampling Plan. Defense Distribution Depot Memphis, Tennessee Prepared for the U.S. Army Engineering Support Center, Huntsville, Alabama.

CH2M HILL September 1995 Operable Unit 4 Field Sampling Plan. Defense Distribution Depot Memphis, Tennessee Prepared for the U.S. Army Engineering Support Center, Huntsville, Alabama.

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CH2M HILL. September 1998b. OUs 2, 3, and 4 and Screening Sites. Field Sampling Plan Addenda. Prepared for the U.S. Army Engineering Support Center, Huntsville, Alabama.

Puls, R. and Barcelona, M., April 1996. Low-Flow (Minimal Drawdown) Groundwater Sampling Procedures. Office of Solid Waste and Emergency Response. U.S. Environmental Protection Agency

U.S. Environmental Protection Agency, Science and Ecosystems Services Division. Environmental Investigations Standard Operating Procedures and Quality Assurance Manual. May 1996 (revised 1997).

U.S. Geological Survey, Vroblesky, D.A. User's Guide for Polyethylene-Based Passive Diffusion Bag Samplers to Obtain Volatile Organic Compound Concentrations In Wells, Part 1: Deployment, Recovery, Data Interpretation, and Quality Control and Assurance. Water Resources Investigations Report 01-4060. 2001

Table 1 Sampling, Analysis, and Data Quality Objectives

Memphis Depot Main Installation Baseline Groundwater Sampling Plan

Sampling Method	Associated Well Numbers	Data Quality Objective Category	Data Qauality Objective/Purpose
Diffusion Bag Samplers	MW-16, 19, 20, 21, 22, 23, 24, 26, 34, 36, 38, 39, 47, 50, 52, 53, 55, 62, 63, 64, 66, 72, 81, 82, 83, 84, 89, and 90	Definitive	Quantify VOC contamination in fluvial aquifer by ensuring sampling methods are consistent with recent sampling events. Also, provide additional information on the stratification of conaminants in the fluvial aquifer.
Tellon Bailer	PZ-04, 05, 06, 07, and 08	Definitive	Same as previous objective. In addition, only productive method for sampling groundwater from piezometers with 0.75 inch ID casing in a water table greater than 33 feet below ground surface.
Low-Flow Techniques (Bladder Pump)	MW-16, 21, 22, 47, 50, 72, 83, 85, 86, 88, 92, 93, 96, 97, 98, 100, 101, and 102	Definitive	Determine current reductive dechlorination activity in fluvial aquifer for EBT study and Remedial Design Acceptable sampling method for geochemical parameters

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Table 3
Analytical Protocols for Samples

Memphis Depot Main Installation Baseline Groundwater Sampling Plan

Matrix and Analytes	Analytical Methods	Field (F) or Analytical (L) Laboratory
Groundwater*		
Redox Potential	Direct-reading meter	F
Dissolved Oxygen	Direct-reading meter	F
pH, turbidity	Direct-reading meter	F
Specific Conductance	Direct-reading meter	F
Temperature	Direct-reading meter	F
VOCs	SW8260B	L
Dissolved Gases (ethene, ethane, and methane)	RSK175	L
Dissolved total organic carbon	SW9060	L
Nitrate, nitrite	SW9056	L
Sulfate	SW9056	L
Sulfide	E376 1	L
Carbon dioxide	CHEMetrics Method 4500	F
Bromide	E320 1	L
Chlonde	SW9056	L
Ferrous Iron	SM 3500 FED	Ĺ
Manganese	SW6010B	Ł
Alkalinity	E310 1	L
Metabolic Fatty Acids	E300 0	Ĺ

^{*}Reported in sequence of sample collection

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Appendix B - EBT Treatability Study Monitoring and Injection Well Installation <u>Procedures</u>

Main Installation EBT Treatability Study Monitoring and Injection Well Installation Procedures

TO:

U.S Army Engineering and Support Center, Huntsville

COPIES.

FROM

CH2M HILL

DATE

April 8, 2002

Introduction

This memorandum has been developed to outline the procedures to be used in the field during monitoring and injection well installation for the EBT Treatability Study within the Main Installation (MI) of the Memphis Depot. Each monitoring and injection well boring will be drilled using rotasonic drilling methods and each well will be constructed according to procedures and specifications described herein.

Objectives of Monitoring and Injection Well Installation

The objectives of the installation activities are to:

- Install and complete injection wells for the application of the electron donor substrate into the fluvial aquifer
- Install and complete monitoring wells downgradient of the anticipated electron donor substrate injection area
- Incorporate findings of monitoring well installation effort into the EBT Treatability Study Technical Memorandum. The data will be used in conjunction with groundwater sample analysis results within the Intermediate and Prefinal/Final MI Remedial Design documents

After installation and prior to the application of the electron donor substrate, the monitoring and injection wells will be sampled to represent baseline groundwater conditions. During application of the electron donor substrate, the wells will be sampled during at least seven other events to monitor the effects of the application.

Data Quality Objectives

The data quality objectives (DQOs) detailed below are established to achieve the sampling objectives

Activity	Data Quality Objective Category	Purpose
Monitoring and injection well installation	Definitive	Injection wells will be used during treatability study and, possibly, for future injection events to enhance the reductive dechlorination process. Monitoring wells will be used during the entire treatability study testing period for collection of groundwater samples to evaluate the effectiveness of the introduction of electron donor substrate to enhancing reductive dechlorination in the fluvial aquifer.

Monitoring and Injection Well Installation Procedures

Up to 28 monitoring and 22 injection wells will be installed using rotasonic drilling methods. Rotasonic drilling was selected because it is the most effective method for boring advancement and well installation under the site hydrogeologic conditions. The relatively large depth to water (i.e., 95 to 105 feet below ground surface (ft bgs) on average) and geologic characteristics of the fluvial aquifer (i.e., tight sands mixed with gravel up to cobble size) likely would cause problems with installation of the wells using other drilling methods.

Well screen intervals will be positioned at different depths within the fluvial aquifer but will always be located above the clay-confining unit that underlies the aquifer. The estimated depth of the wells ranges from 110 to 135 ft bgs. The final location of these wells will be dependent upon the results of baseline groundwater sampling event, as described in Appendix A to the EBT Treatability Study Workplan.

Installation Procedures

Monitoring and injection well installation will be performed in accordance with US Army Corps of Engineers OE EM 1110-1-4000 and US Environmental Protection Agency Region IV, Science and Ecosystems Services Division *Environmental Investigations Standard Operating Procedures Quality Assurance Manual* (EISOPQAM), May 1996 (revised in 1997). The wells will be constructed within rotasonic drill casing as the casing is withdrawn from the boring. Borehole diameters will be a minimum of 7 inches. The inside diameter of the rotasonic drill casing will be at least 4 inches larger than the outside diameter of the well casing and screen to facilitate proper installation of the well. Therefore, the rotasonic drill casing will require an inner annulus that is 6 1/4-inch diameter or larger.

The new wells will be constructed of 2-inch inside diameter (I.D.) PVC casing and screens. Each well will have a filter pack around the screen, a bentonite seal above the filter pack,

and cement grout to ground surface installed through the drill casing. The wells will be straight and plumb to allow passage of pumps or sampling devices.

The documentation record and forms will document the following information for each boring:

- Boring or well identification Begin with well # MW-109
- Purpose of the boring (e.g., soil sampling, monitoring well)
- Location in relation to an easily identifiable landmark
- Names of drilling subcontractor and logger
- Start and finish dates and times
- Drilling method
- Types of drilling fluids and depths at which they were used, if applicable
- Diameters of surface casing, casing type, and methods of installation
- Depth at which saturated conditions were first encountered
- Lithologic descriptions and depths of lithologic boundaries
- Sampling-interval depths
- · Zones of caving or heaving
- Depth at which drilling fluid was lost and the amount lost
- Changes in drilling fluid properties
- Drilling rate
- Drilling rig reactions (e.g., chatter, rod drops, and bouncing)

Prior to drilling activities and between each well location, all drilling equipment and the rig will be decontaminated using a high pressure steam cleaning wash as described in the Decontamination Section

Logging of Boreholes

Samples for lithologic description will be collected continuously at 10-foot intervals beginning at the ground surface. Lithologic descriptions of unconsolidated materials encountered in the boreholes will generally be described in accordance with the 1990 American Society for Testing and Materials (ASTM) D-2488-90, Standard Practice for Description and Identification of Soils (Visual-Manual Procedure) Descriptive information to be recorded in the field will include:

- Identification of the predominant particles size and range of particle sizes
- Percent of gravel, sand, fines, or all three
- Description of grading and sorting of coarse particles
- Particle angularity and shape

Maximum particle size or dimension.

Plasticity of fines description include.

- Color using Munsell Color System
- Moisture (dry, wet, or moist)
- Consistency of fine grained soils
- Structure of consolidated materials
- Cementation (weak, moderate, or strong)

Identification of the Unified Soil Classification System (USCS) group symbol will be used Additional information to be recorded is: depth to the water table, caving or sloughing of the borehole, changes in drilling rate, depths of laboratory sample collection, presence of organic materials, presence of fractures or voids in consolidated materials, and other noteworthy observations or conditions, such as the locations of geologic boundaries.

The headspace of soil samples will be screened with a flame ionization detector-organic vapor monitor (e.g., FID-OVA). The headspace samples will be brought (if necessary) to a temperature of between 20°C (68°F) and 32°C (90°F), and the reading will be obtained five minutes thereafter. The soil sample will be split into two jars and readings will be made with the FID (unfiltered) on one jar. If the FID reading is greater than 10 parts per million (ppm), a reading will be made on the second jar with an activated charcoal filter on the FID. A total corrected hydrocarbon measurement of the sample will be calculated by subtracting the filtered reading from the unfiltered reading. Analytical instruments must be calibrated in accordance with the manufacturer's instructions. The headspace samples will be collected and analyzed using the following procedure.

- 1 From the sample location, remove the top 1 to 2 inches of soil using a decontaminated stainless steel spoon
- 2. Fill ½ of two decontaminated 16-ounce mason jars with soil from the resulting hole using the stainless steel spoon
- 3. Cover the jars immediately with aluminum foil and fasten the jar lids.
- Allow the sample vapors to equilibrate in the jars (approximately 5 minutes).
- 5. Punch a hole in the aluminum foil with the tip of a calibrated FID
- 6 Record the highest reading.
- 7 If the FID reading is > 10 ppm, repeat Steps 5 and 6 with the active charcoal filter on the calibrated FID to the second jar

All measurements will be recorded on the logging form at the corresponding depths. The samples will be handled in such a way as to minimize the loss of volatiles. Soil cuttings will be examined for their hazardous characteristics. If suspected samples are encountered, they will be noted on the boring log form for reference during investigative derived waste (IDW) sampling.

Casing Requirements

The casing requirements that will be followed include:

- All casing will be new, unused, decontaminated, 2-inch inside diameter, schedule 40 polyvinyl chloride (PVC) with internal flush joined threaded joints.
- The PVC will conform to the ASTM Standard F-480-88A or the National Sanitation Foundation Standard 14 (Plastic Pipe System)
- Glue or solvent-welded joints will not be used to join casing.

Well Screen Requirements

Well screen requirements are as follows.

- All requirements that apply to casing will also apply to well screen, except for strength requirements.
- Monitoring wells will not be screened across more than one water-bearing unit.
- The screen sections will be factory slotted or wire wrapped with 0 040-inch openings and no less than 10-ft in length.
- A threaded PVC cap or point will be placed at the bottom of the screen will be joined to the screen by threads.

Filter Pack Requirements

The filter pack material will be clean, bagged, sieve sized, silica sand, (supplier certified to be free of contaminants), inert, hard, well rounded (less than 2 percent flat particles), and free from roots, trash, and other deleterious material. The sand will be certified free of contaminants by vendor or contractor. The filter pack will extend from the bottom of the hole to at least 2 ft above the top of the well screen. The vendor will be required to use Unimim Filter Seal No. 2

The filter pack will be installed with a bottom-discharge tremie pipe. The tremie pipe will be lifted from the bottom of the hole at the same rate the filter pack is set. The contractor will record the volume of the filter pack emplaced in the well. Potable water may be used, with the approval of FTL, to emplace the filter pack so long as no contaminants are introduced.

Bentonite Seal Requirements

Following filter pack placement, a minimum 2-foot-thick bentonite seal will be placed above the sandpack. The 100% sodium bentonite seal will consist of 1/4-inch or 3/8-inch diameter dry bentonite pellets or chips. The bentonite seal will be installed by gravity methods. The bentonite seal will be allowed to hydrate for a minimum of 4 hours prior to the installation of the cement grout.

Casing Grout Requirements

The casing grout requirements are as follows

Cement grout will be placed in the annular space above the bentonite seal to ground surface. The grout will be pumped through a side-discharge tremie pipe and the length will be no more than 5 feet from the top of the level of grout at all times. The pumping will continue until grout has returned to the surface. No method will be permitted that does not force grout from the bottom of the borehole to the surface. The grout seal will be Type II

Portland cement or American Petroleum Institute Class A cement with no more than 4 percent bentonite. The grout will be mixed in the following proportions: 94 lbs. of neat cement, not more than 4 lbs. of 100 percent sodium bentonite powder, and not more than 8 gallons of potable water. The grout will have a mixed minimum specific density of 9.4 pounds per gallon (lb/gal) or the manufacturer's recommended density. A mud balance will be used to ensure the density of the mixture conforms to the manufacturer's standards. Prior to installation of the well completions, the boreholes will be topped off with grout to approximately 1 to 2 feet bgs.

Surface Completion Requirements

Wells will be set as flush-mounted completions. The casing will be cut approximately 3 inches bgs and a watertight casing cap will be placed on the well. A small diameter (e.g., 1/4-inch) vent hole will be placed in the upper portion of the casing, or a ventilated well cap will be used. A small notch will be cut in the top of the casing to be used as a measuring point for water levels.

A freely draining 10-inch inner diameter manhole cover with a locking lid will be placed over the casing. The top of the casing will be at least 6 inches above the bottom of the box. The manhole will be centered in a 3-foot diameter, 4-inch thick concrete pad that slopes away from the manhole at ¼-inch per foot. The identity of the well will be permanently marked on the concrete pad. Where heavy traffic may pass over the well or for other reasons, the concrete pad and valve box/lid assembly will be constructed to meet the strength requirements of surrounding surfaces.

When a well is not installed in a concrete or asphalt drive or parking area, four 3-inch diameter concrete-filled steel guard posts will be installed. The guard posts will be 5 feet in total length and installed at the corners of the well pad. The guard posts must be recessed approximately 2 feet into the ground and set in concrete. Do not install the guard posts in the concrete pad placed at the well base. The protective sleeve and guard posts will be painted a high visibility yellow.

Wells will be secured as soon as possible after drilling with corrosion resistant locks. The locks must either have identical keys or be keyed for opening with one master key

A well completion diagram will be submitted for each monitoring well or injection point installed. It will include the following information

- Well identification (this will be identical to the boring identification described)
- Drilling method
- Installation date(s)
- Elevations of ground surface and the measuring point notch
- Total boring depth
- Lengths and descriptions of the screen and casing
- Lengths and descriptions of the filter pack, bentonite seal, casing grout, and any backfilled material

6

- Elevation of water surface before and immediately after development
- Summary of the material penetrated by the boring

The locations and elevations of the monitoring and injection wells will be surveyed by a licensed surveyor upon completion.

Monitoring Well Development

The wells will be developed with a surge block in conjunction with a pump and or bailers. No air, detergents, soaps, acids, bleaches, or additives will be used during well development. Well development will be initiated no sooner than 24 hours following grout installation.

Development will continue until clear, sediment free formation water is produced from the well and until pH, conductivity, turbidity, and temperature measurements have stabilized. Stabilization is defined by the pH is within + or - 01, the conductivity is + or - 3%, and the turbidity remains less than 10 NTUs for at least 30 minutes. Parameter measurement and development data will be documented.

Equipment Decontamination Procedures

All downhole drilling equipment as well as other equipment will be decontaminated according to procedures presented in Appendix B of the EISOPQAM Decontamination of the drill rig, rotasonic drilling equipment, pipes, bits, tools, and all downhole equipment will be conducted between each well installation. Decontamination of development equipment will be performed between each well developed. Decontamination will consist of the following.

- High pressure, low volume steam-cleaning
- Wash and scrub with non-phosphate detergent (Liquinox) and potable water
- · Rinse with tap water
- Rinse with deionized (or analyte free) water
- Rinse with laboratory grade isopropyl alcohol (PVC or plastic material will not be rinsed with solvent)
- Rinse with organic free water
- Air dry to the extent practical
- Wrap in plastic sheeting or aluminum foil

Decontamination activities will be conducted on a concrete decontamination pad at the site.

Standard procedures for field equipment are described below.

Well Sounders and Groundwater Measurement Tapes: Decontamination procedures for Teflon™, PVC, stainless-steel, and glass tubing used for groundwater sampling are listed below

- Wash with laboratory detergent and tap water.
- Rinse with tap water.
- Rinse with analyte-free (deionized) water

7

Wrap equipment in aluminum foil

<u>Field Parameter Measurement Probes</u>: Field parameter measurement probes, (e.g., pH or specific ion electrodes, geophysical probes, or thermometers) that come in direct contact with the sample will be decontaminated using the procedures listed below, unless manufacturer's instructions indicate otherwise. Probes that make no direct contact (e.g., OVA equipment) will be wiped with clean paper towels.

- Rinse with tap water.
- Rinse with analyte-free (deionized) water.
- Solvent rinse if obvious contamination remains after rinsing and if solvent will not damage probe.
- Rinse with analyte-free (deionized) water.

<u>Sampling Equipment for Organic and Metal Analysis:</u> Teflon™, stainless-steel, glass, or metal sampling equipment used to collect samples for organic and metal analysis will be cleaned between sample locations as listed below.

- Wash and scrub equipment thoroughly with laboratory detergent and tap water
- Rinse thoroughly with tap water.
- Rinse thoroughly with deionized, analyte-free water.
- Rinse with solvent (pesticide-grade isopropanol). Note. Do not rinse PVC or plastic materials with solvent.
- Rinse with organic-free water and allow to air dry as long as possible
- Wrap with aluminum foil to prevent contamination

Investigation-Derived Waste (IDW)

All soil cuttings will be placed in roll-off boxes located in a central staging area at the site. Soil cuttings may be temporarily staged at drill location on and covered by plastic sheeting, prior to placement in roll-off boxes. Drilling fluids, development water, and wastewater from equipment decontamination produced during the drilling operation will be containerized in 55-gallon drums approved by Department of Transportation (DOT) (supplied by the Subcontractor). The drums will permanently marked with a weatherproof label, signifying the date, site number, and well number. Drums will be staged at a central location at the site.

Representative samples of the IDW will be collected for chemical characterization by the FTL for off-site disposal. Once analytical results of the IDW are available, the IDW will be disposed of off-site in accordance with federal, state, and local regulations. The IDW will be removed from the site within 60 days following of the receipt of analytical results.

Logistics

Equipment, supplies, and personnel required to complete the monitoring well installation effort at the Site will mobilize after approval of the RD workplan and the EBT Treatability Study Workplan. The Hazardous and Toxic Waste Health and Safety Plan (CH2M HILL, August 1995) for Memphis Depot will be amended prior to the start of field activities.

References

American Society for Testing and Materials (ASTM) D-2488-90 Standard Practice for Description and Identification of Soils (Visual-Manual Procedure).

CH2M HILL February 1995 Final Generic Quality Assurance Project Plan. Defense Distribution Depot Memphis, Tennessee Prepared for the United States Army Engineering Support Center, Huntsville, Alabama.

CH2M HILL, Inc. August 1995. *Hazardous and Toxic Waste Health and Safety Plan*. Prepared for U.S. Army Engineering and Support Center Huntsville, Alabama.

U.S. Environmental Protection Agency, Science and Ecosystems Services Division Environmental Investigations Standard Operating Procedures and Quality Assurance Manual. May 1996 (revised 1997).

TAB

Appendix C

Appendix C – August 1995 Final Generic Quality Assurance Project Plan (amended)

Standard Operating Procedures (SOPs) Adopted Since the Completion of the August 1995 Generic Quality Assurance Project Plan (QAPP), Memphis Depot

PREPARED FOR:

QAPP (1995)

PREPARED BY.

Bryan Burkingstock/ATL

DATE

February 15, 2002

Since the inception of the 1995 QAPP, new protocols have been accepted by BCT members for various Memphis Depot field activities. SOPs located in the following site-specific plans should be used for further reference on applicable methods and procedures:

- Operable Units 2, 3, and 4 and Screening Sites: Field Sampling Plan Addenda (CH2M HILL, September 1998)
- Sampling and Analysis Plan for Evaluation of Biodegradation of VOCs in Groundwater at the Memphis Depot (CH2M HILL, March 13, 2000)
- Data Collection Plan for Long Term Operational Areas (LTOAs), Main Installation, Memphis Depot (CH2M HILL, June 5, 2001)
- Well Construction and Sampling Techniques for Long-Term Operational Area (LTOA)
 Monitoring Wells Associated with SS42/SS43, NE6 (Building T702), and SS80 (CH2M HILL,
 September 5, 2001)

SOPs included as an Addendum to the 1995 QAPP include:

- 1) Low-Flow (Minimal Drawdown) Groundwater Sampling Procedures (Puls and Barcelona, 1996)
- 2) User's Guide for Polyethylene-Based Passive Diffusion Bag Samplers to Obtain Volatile Organic Compound Concentration in Wells (USGS 2001)
- 3) Standard Operating Procedure for Soil Headspace Field Screening Using an OVA/FID at Dunn Field (CH2M HILL, May 5, 2000)
- 4) Standard Operating Procedure for Collecting Soil Samples for Volatile Organic Compounds (VOCs) (CH2M HILL, August 16, 2001)
- 5) Standard Operating Procedure for Collecting Soil Samples for Volatile Organic Compounds (CH2M HILL, May 5, 2000)
- Standard Operating Procedure for QED® Bladder Pumps (CH2M HILL, March 10, 2000)
- 7) Standard Operating Procedure for Sudan IV Dye Testing (CH2M HILL, May 5, 2000)



Ground Water Issue

LOW-FLOW (MINIMAL DRAWDOWN) GROUND-WATER SAMPLING PROCEDURES

by Robert W. Puls¹ and Michael J. Barcelona2

Background

The Regional Superfund Ground Water Forum is a group of ground-water scientists, representing EPA's Regional Superfund Offices, organized to exchange information related to ground-water remediation at Superfund sites. One of the major concerns of the Forum is the sampling of ground water to support, site assessment and remedial performance monitoring objectives. This paper is intended to provide background information on the development of low-flow sampling procedures and its application under a variety of hydrogeologic settings. It is hoped that the paper will support the production of standard operating procedures for use by EPA Regional personnel and other environmental professionals engaged in ground-water sampling.

For further information contact. Robert Puls, 405-436-8543, Subsurface Remediation and Protection Division, NRMRL, Ada, Oklahoma

I. Introduction

The methods and objectives of ground-water sampling to assess water quality have evolved over time. Initially the emphasis was on the assessment of water quality of aquifers as sources of drinking water. It arge water-bearing

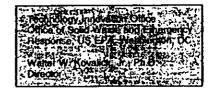
units were identified and sampled in keeping with that objective. These were highly productive aquifers that supplied danking water via private wells or through public water supply systems. Gradually, with the increasing awareness of subsurface pollution of these water resources, the understanding of complex hydrogeochemical processes which govern the fate and transport of confaminants in the subsurface increased. This increase in understanding was also due to advances in a number of scientific disciplines and improvements in tools used for site characterization and ground-water sampling. Ground-water quality investigations where pollution was detected initially borrowed ideas, methods, and materials for site characterization from the water supply field and water analysis from public health practices. This included the materials and manner in which monitoring wells were installed and the way in which water was brought to the surface, treated, preserved and analyzed The prevailing conceptual ideas included convenient generalizations of ground-water resources in terms of large and relatively homogeneous hydrologic units. With time it became apparent that conventional water supply generalizations of homogeneity did not adequately represent field data regarding pollution of these subsurface resources. The important role of heterogeneity became increasingly clear not only in geologic terms, but also in terms of complex physical,

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chemical and biological subsurface processes. With greater appreciation of the role of heterogeneity, it became evident that subsurface pollution was ubiquitous and encompassed the unsaturated zone to the deep subsurface and included unconsolidated sediments, fractured rock, and aquitards or low-yielding or impermeable formations. Small-scale processes and heterogeneities were shown to be important in identifying contaminant distributions and in controlling water and contaminant flow paths.

It is beyond the scope of this paper to summanze all the advances in the field of ground-water quality investigations and remediation, but two particular issues have bearing on ground-water sampling today aquifer heterogeneity and colloidal transport. Aguiller heterogeneities affect contaminant flow paths and include variations in geology, geochemistry, hydrology and microbiology. As methods and the tools available for subsurface investigations have become increasingly sophisticated and understanding of the subsurface environment has advanced, there is an awareness that in most cases a primary concern for site investigations is characterization of contaminant flow paths rather than entire aguifers. In fact, in many cases, plume thickness can be less than well screen lengths (e.g., 3-6 m) typically installed at hazardous waste sites to detect and monitor plume movement over time. Small-scale differences have increasingly been shown to be important and there is a general trend toward smaller diameter wells and shorter screens

The hydrogeochemical significance of colloidal-size particles in subsurface systems has been realized during the past several years (Gschwend and Reynolds, 1987; McCarthy and Zachara, 1989, Puls, 1990, Ryan and Gschwend, 1990) This realization resulted from both field and laboratory studies that showed faster contaminant migration over greater distances and at higher concentrations than flow and transport model predictions would suggest (Budderneier and Hunt, 1988; Enfield and Bengisson, 1988, Penrose et al., 1990) Such models typically account for interaction between the mobile aqueous and immobile solid phases, but do not allow for a mobile, reactive solid phase. It is recognition of this third phase as a possible means of contaminant transport that has brought increasing attention to the manner in which samples are collected and processed for analysis (Puls et al., 1990, McCarthy and Degueldre, 1993, Backhus et al., 1993, U.S. EPA, 1995) If such a phase is present in sufficient mass, possesses high sorption reactivity, large surface area, and remains stable in suspension, it can serve as an important mechanism to facilitate contaminant transport in many types of subsurface systems

Colloids are particles that are sufficiently small so that the surface free energy of the particle dominates the bulk free energy. Typically, in ground water, this includes particles with diameters between 1 and 1000 nm. The most commonly observed mobile particles include, secondary clay minerals; hydrous iron, aluminum, and manganese oxides; dissolved and particulate organic materials, and viruses and bacteria.

These reactive particles have been shown to be mobile under a variety of conditions in both field studies and laboratory column experiments, and as such need to be included in monitoring programs where identification of the *total* mobile contaminant loading (dissolved + naturally suspended particles) at a site is an objective. To that end, sampling methodologies must be used which do not artificially bias naturally suspended particle concentrations.

Currently the most common ground-water purging and sampling methodology is to purge a well using bailers or high speed pumps to remove 3 to 5 casing volumes followed by sample collection. This method can cause adverse impacts on sample quality through collection of samples with high levels of turbidity. This results in the inclusion of otherwise immobile artifactual particles which produce an overestimation of certain analytes of interest (e.g., metals or hydrophobic organic compounds). Numerous documented problems associated with filtration (Danielsson, 1982, Laxen and Chandler, 1982; Horowitz et al., 1992) make this an undesirable method of rectifying the turbidity problem, and include the removal of potentially mobile (contaminant-associated) particles during filtration, thus artificially biasing contaminant concentrations low. Sampling-induced furbidity problems can often be mitigated by using low-flow purging and sampling techniques

Current subsurface conceptual models have undergone considerable retinement due to the recent development and increased use of field screening tools. So-called hydraulic push technologies (e.g., cone penetrometer, Geoprobe®, OEÐ HydroPunch®) enable relatively fast screening site characterization which can then be used to design and install a monitoring well network. Indeed, alternatives to conventional monitoring wells are now being considered for some hydrogeologic settings. The ultimate design of any monitoring system should however be based upon adequate site characterization and be consistent with established monitoring objectives.

If the sampling program objectives include accurate assessment of the magnitude and extent of subsurface contamination over time and/or accurate assessment of subsequent remedial performance, then some information regarding plume delineation in three-dimensional space is necessary pnor to monitoring well network design and installation. This can be accomplished with a variety of different tools and equipment ranging from hand-operated augers to screening tools mentioned above and large drilling rigs. Detailed information on ground-water flow velocity, direction, and honzontal and vertical variability are essential baseline data requirements. Detailed soil and geologic data are required prior to and during the installation of sampling points. This includes historical as well as detailed soil and geologic logs which accumulate during the site investigation. The use of borehole geophysical techniques is also recommended. With this information (together with other site characterization data) and a clear understanding of sampling objectives, then appropriate location, screen length, well diameter, slot size, etc. for the monitoring well network can be decided. This is especially critical for new in situ remedial approaches or natural attenuation assessments at hazardous waste sites.

In general, the overall goal of any ground-water sampling program is to collect water samples with no alteration in water chemistry; analytical data thus obtained may be used for a variety of specific monitoring programs depending on the regulatory requirements. The sampling methodology described in this paper assumes that the monitoring goal is to sample monitoring wells for the presence of confaminants and it is applicable whether mobile colloids are a concern or not and whether the analytes of concern are metals (and metalloids) or organic compounds.

II. Monitoring Objectives and Design Considerations

The following issues are important to consider prior to the design and implementation of any ground-water monitoring program, including those which anticipate using low-flow purging and sampling procedures.

A. Data Quality Objectives (DQOs)

Monitoring objectives include four main types detection, assessment, corrective-action evaluation and resource evaluation, along with *hybrid* variations such as site-assessments for property transfers and water availability investigations. Monitoring objectives may change as contamination or water quality problems are discovered. However, there are a number of common components of monitoring programs which should be recognized as important regardless of initial objectives. These components include.

- Development of a conceptual model that incorporates elements of the regional geology to the local geologic framework. The conceptual model development also includes initial site characterization efforts to identify hydrostratigraphic units and likely flow-paths using a minimum number of borings and well completions.
- Cost-effective and well documented collection of high quality data utilizing simple, accurate, and reproducible techniques, and
- Refinement of the conceptual model based on supplementary data collection and analysis

These fundamental components serve many types of monitoring programs and provide a basis for future efforts that evolve in complexity and level of spatial detail as purposes and objectives expand. High quality, reproducible data collection is a common goal regardless of program objectives.

High quality data collection implies data of sufficient accuracy, precision, and completeness (i.e., ratio of valid analytical results to the minimum sample number called for by the program design) to meet the program objectives. Accuracy depends on the correct choice of monitoring tools and procedures to minimize sample and subsurface disturbance from collection to analysis. Precision depends on the repeatability of sampling and analytical protocols. It can be assured or improved by replication of sample analyses including blanks, field/lab standards and reference standards.

B. Sample Representativeness

An important goal of any monitoring program is collection of data that is truly representative of conditions at the site. The term representativeness applies to chemical and hydrogeologic data collected via wells, borings, piezometers, geophysical and soil gas measurements, lysimeters, and temporary sampling points. It involves a recognition of the statistical variability of individual subsurface physical properties, and contaminant or major ion concentration levels, while explaining extreme values. Subsurface temporal and spatial variability are facts. Good professional practice seeks to maximize representativeness by using proven accurate and reproducible techniques to define limits on the distribution of measurements collected at a site. However, measures of representativeness are dynamic and are controlled by evolving site characterization and monitoring objectives. An evolutionary site characterization model, as shown in Figure 1, provides a systematic approach, to the goal of consistent data collection

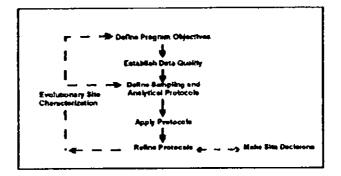


Figure 1 Evolutionary Site Characterization Model

The model emphasizes a recognition of the causes of the variability (e.g., use of inappropriate technology such as using bailers to purge wells; imprecise or operator-dependent methods) and the need to control avoidable errors

1) Questions of Scale

A sampling plan designed to collect representative samples must take into account the potential scale of changes in site conditions through space and time as well as the chemical associations and behavior of the parameters that are targeted for investigation. In subsurface systems, physical (i.e., aquifer) and chemical properties over time or space are not statistically independent. In fact, samples taken in close proximity (i.e., within distances of a few meters) or within short time periods (i.e., more frequently than monthly) are highly auto-correlated. This means that designs employing high-sampling frequency (e.g., monthly) or dense spatial monitoring designs run the risk of redundant data collection and misleading inferences regarding frends in values that aren't statistically valid. In practice, contaminant detection and assessment monitoring programs rarely suffer these over-sampling concerns. In corrective-action evaluation programs, it is also possible that too little data may be collected over space or time. In these cases, false interpretation of the spatial extent of contamination or underestimation of temporal concentration variability may result.

2) Target Parameters

Parameter selection in monitoring program design is most often dictated by the regulatory status of the site. However, background water quality constituents, purging indicator parameters, and contaminants, all represent targets for data collection programs. The tools and procedures used in these programs should be equally rigorous and applicable to all categories of data, since all may be needed to determine or support regulatory action.

C. Sampling Point Design and Construction

Detailed site characterization is central to all decision-making purposes and the basis for this characterization resides in identification of the geologic framework and major hydro-stratigraphic units. Fundamental data for sample point location include—subsurface lithology, head-differences and background geochemical conditions. Each sampling point has a proper use or uses which should be documented at a level which is appropriate for the program's data quality objectives. Individual sampling points may not always be able to fulfill multiple monitoring objectives (e.g., detection, assessment, corrective action).

Compatibility with Monitoring Program and Data Quality Objectives

Specifics of sampling point location and design will be dictated by the complexity of subsurface lithology and variability in contaminant and/or geochemical conditions. It should be noted that, regardless of the ground-water sampling approach, few sampling points (e.g., wells, drive-points, screened augers) have zones of influence in excess of a few

feet. Therefore, the spatial frequency of sampling points should be carefully selected and designed.

2) Flexibility of Sampling Point Design

In most cases well-point diameters in excess of 1 7/8 inches will permit the use of most types of submersible pumping devices for low-flow (minimal drawdown) sampling It is suggested that short (e.g., less than 1 6 m) screens be incorporated into the monitoring design where possible so that comparable results from one device to another might be expected. Short, of course, is relative to the degree of vertical water quality variability expected at a site.

3) Equilibration of Sampling Point

Time should be allowed for equilibration of the well or sampling point with the formation after installation. Placement of well or sampling points in the subsurface produces some disturbance of ambient conditions. Drilling techniques (e.g., auger, rolary, etc.) are generally considered to cause more disturbance than direct-push technologies. In either case, there may be a period (i.e., days to months) during which water quality near the point may be distinctly different from that in the formation. Proper development of the sampling point and adjacent formation to remove fines created during emplacement will shorten this water quality recovery period.

III. Definition of Low-Flow Purging and Sampling

It is generally accepted that water in the well casing is non-representative of the formation water and needs to be purged prior to collection of ground-water samples. However, the water in the screened interval may indeed be representative of the formation, depending upon well construction and site hydrogeology. Wells are purged to some extent for the following reasons, the presence of the air interface at the top of the water column resulting in an oxygen concentration gradient with depth, loss of volatiles up the water column, leaching from or sorption to the casing or filter pack, chemical changes due to clay seals or backfill, and surface infiltration.

Low-flow purging, whether using portable or dedicated systems, should be done using pump-intake located in the middle or slightly above the middle of the screened interval. Placement of the pump too close to the bottom of the well will cause increased entrainment of solids which have collected in the well over time. These particles are present as a result of well development, prior purging and sampling events, and natural colloidal transport and deposition. Therefore, placement of the pump in the middle or toward the top of the screened interval is suggested. Placement of the pump at the top of the water column for sampling is only recommended in unconfined aquifers, screened across the water table, where this is the desired sampling point. Low-

flow purging has the advantage of minimizing mixing between the overlying stagnant casing water and water within the screened interval

A. Low-Flow Purging and Sampling

Low-flow refers to the velocity with which water enters the pump intake and that is imparted to the formation pore water in the immediate vicinity of the well screen. It does not necessarily refer to the flow rate of water discharged at the surface which can be affected by flow regulators or restrictions. Water level drawdown provides the best indication of the stress imparted by a given flow-rate for a given hydrological situation. The objective is to pump in a manner that minimizes stress (drawdown) to the system to the extent practical taking into account established site sampling objectives. Typically, flow rates on the order of 0.1 - 0.5 L/min. are used, however this is dependent on site-specific hydrogeology Some extremely coarse-textured formations have been successfully sampled in this manner at flow rates to 1 L/min. The effectiveness of using low-flow purging is intimately linked with proper screen location, screen length, and well construction and development techniques. The reestablishment of natural flow paths in both the vertical and honzontal directions is important for correct interpretation of the data. For high resolution sampling needs, screens less than 1 m should be used. Most of the need for purging has been found to be due to passing the sampling device through the overlying casing water which causes mixing of these stagnant waters and the dynamic waters within the screened interval. Additionally, there is disturbance to suspended sediment collected in the bottom of the casing and the displacement of water out into the formation immediately adjacent to the well screen. These disturbances and impacts can be avoided using dedicated sampling equipment, which precludes the need to insert the sampling device prior to purging and sampling

Isolation of the screened interval water from the overlying stagnant casing water may be accomplished using low-flow minimal drawdown techniques. If the pump intake is located within the screened interval, most of the water pumped will be drawn in directly from the formation with little mixing of casing water or disturbance to the sampling zone However, if the wells are not constructed and developed properly, zones other than those intended may be sampled. At some sites where geologic heterogeneities are sufficiently different within the screened interval, higher conductivity zones may be preferentially sampled. This is another reason to use shorter screened intervals, especially where high spatial resolution is a sampling objective.

B. Water Quality Indicator Parameters

It is recommended that water quality indicator parameters be used to determine purging needs prior to sample collection in each well. Stabilization of parameters such as pH, specific conductance, dissolved oxygen, oxida-

tion-reduction potential, temperature and turbidity should be used to determine when formation water is accessed during purging. In general, the order of stabilization is pH, temperature, and specific conductance, followed by oxidation-reduction potential, dissolved oxygen and turbidity. Temperature and pH, while commonly used as purging indicators, are actually quite insensitive in distinguishing between formation water and stagnant casing water; nevertheless, these are important parameters for data interpretation purposes and should also be measured. Performance criteria for determination of stabilization should be based on water-level drawdown, pumping rate and equipment specifications for measuring indicator parameters. Instruments are available which utilize in-line flow cells to continuously measure the above parameters.

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It is important to establish specific well stabilization criteria and then consistently follow the same methods thereafter, particularly with respect to drawdown, flow rate and sampling device. Generally, the time or purge volume required for parameter stabilization is independent of well depth or well volumes. Dependent variables are well diameter, sampling device, hydrogeochemistry, pump flow rate, and whether the devices are used in a portable or dedicated manner if the sampling device is already in place (i.e., dedicated sampling systems), then the time and purge volume needed for stabilization is much shorter. Other advantages of dedicated equipment include less purge water for waste disposal, much less decontamination of equipment, less time spent in preparation of sampling as well as time in the field, and more consistency in the sampling approach which probably will translate into less variability in sampling results. The use of dedicated equipment is strongly recommended at wells which will undergo routine sampling over

If parameter stabilization criteria are too stringent, then minor oscillations in indicator parameters may cause purging operations to become unnecessarily protracted. It should also be noted that turbidity is a very conservative parameter in terms of stabilization. Turbidity is always the last parameter to stabilize. Excessive purge times are invariably related to the establishment of too stringent turbidity stabilization criteria. It should be noted that natural turbidity levels in ground water may exceed 10 nephelometric turbidity units (NTU).

C. Advantages and Disadvantages of Low-Flow (Minimum Drawdown) Purging

In general, the advantages of low-flow purging include:

- samples which are representative of the mobile load of contaminants present (dissolved and colloid-associated);
- minimal disturbance of the sampling point thereby minimizing sampling artifacts;
- · less operator variability, greater operator control,

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- · reduced stress on the formation (minimal drawdown),
- less mixing of stagnant casing water with formation water;
- reduced need for filtration and, therefore, less time required for sampling,
- smaller purging volume which decreases waste disposal costs and sampling time,
- better sample consistency, reduced artificial sample variability.

Some disadvantages of low-flow purging are:

- · higher initial capital costs,
- · greater set-up time in the field,
- need to transport additional equipment to and from the site.
- · increased training needs,
- resistance to change on the part of sampling practitioners
- concern that new data will indicate a change in conditions and trigger an action.

IV. Low-Flow (Minimal Drawdown) Sampling Protocols

The following ground-water sampling procedure has evolved over many years of experience in ground-water sampling for organic and inorganic compound determinations and as such summanzes the authors' (and others) expenences to date (Barcelona et al., 1984, 1994, Barcelona and Helfnch, 1986, Puls and Barcelona, 1989, Puls et al. 1990, 1992, Puls and Powell, 1992, Puls and Paul, 1995). Highquality chemical data collection is essential in ground-water monitoring and site characterization. The primary limitations to the collection of representative ground-water samples include imixing of the stagnant casing and fresh screen waters during insertion of the sampling device or groundwater level measurement device; disturbance and resuspension of settled solids at the bottom of the well when using high pumping rates or raising and lowering a pump or bailer; introduction of atmospheric gases or degassing from the water during sample handling and transfer, or inappropriate use of vacuum sampling device, etc.

A. Sampling Recommendations

Water samples should not be taken immediately tollowing well development. Sufficient time should be allowed for the ground-water flow regime in the vicinity of the monitoring well to stabilize and to approach chemical equilibrium with the well construction materials. This lag time will depend on site conditions and methods of installation but often exceeds one week.

Well purging is nearly always necessary to obtain samples of water flowing through the geologic formations in the screened interval. Rather than using a general but arbitrary guideline of purging three casing volumes prior to

sampling, it is recommended that an in-line water quality measurement device (e.g., flow-through cell) be used to establish the stabilization time for several parameters (e.g., pH, specific conductance, redox, dissolved oxygen, turbidity) on a well-specific basis. Data on pumping rate, drawdown, and volume required for parameter stabilization can be used as a guide for conducting subsequent sampling activities.

The following are recommendations to be considered before, during and after sampling

- use low-flow rates (<0.5 L/min), during both purging and sampling to maintain minimal drawdown in the well,
- maximize tubing wall thickness, minimize tubing length,
- place the sampling device intake at the desired sampling point;
- minimize disturbances of the stagnant water column above the screened interval during water level measurement and sampling device insertion;
- make proper adjustments to stabilize the flow rate as soon as possible;
- monitor water quality indicators during purging,
- collect unfiltered samples to estimate contaminant loading and transport potential in the subsurface system

B. Equipment Calibration

Prior to sampling, all sampling device and monitoring equipment should be calibrated according to manufacturer's recommendations and the site Quality Assurance Project Plan (QAPP) and Field Sampling Plan (FSP). Calibration of pH should be performed with at least two buffers which bracket the expected range. Dissolved oxygen calibration must be corrected for local barometric pressure readings and elevation.

C. Water Level Measurement and Monitoring

It is recommended that a device be used which will least disturb the water surface in the casing. Well depth should be obtained from the well logs. Measuring to the bottom of the well casing will only cause resuspension of settled solids from the formation and require longer purging times for turbidity equilibration. Measure well depth after sampling is completed. The water level measurement should be taken from a permanent reference point which is surveyed relative to ground elevation.

D. Pump Type

The use of low-flow (e.g., 0.1-0.5 L/min) pumps is suggested for purging and sampling all types of analytes. All pumps have some limitation and these should be investigated with respect to application at a particular site. Bailers are inappropriate devices for low-flow sampling.

1) General Considerations

There are no unusual requirements for ground-water sampling devices when using low-flow, minimal drawdown techniques. The major concern is that the device give consistent results and minimal disturbance of the sample across a range of low flow rates (i.e., < 0.5 L/min). Clearly, pumping rates that cause minimal to no drawdown in one well could easily cause *significant* drawdown in another well finished in a less transmissive formation. In this sense, the pump should not cause undue pressure or temperature changes or physical disturbance on the water sample over a reasonable sampling range. Consistency in operation is critical to meet accuracy and precision goals.

2) Advantages and Disadvantages of Sampling Devices

A variety of sampling devices are available for low-flow (minimal drawdown) purging and sampling and include penstaltic pumps, bladder pumps, electrical submersible pumps, and gas-driven pumps. Devices which lend themselves to both dedication and consistent operation at definable low-flow rates are preferred. It is desirable that the pump be easily adjustable and operate reliably at these lower flow rates. The peristaltic pump is limited to shallow applications and can cause degassing resulting in alteration of pH, alkalinity, and some volatiles loss. Gas-driven pumps should be of a type that does not allow the gas to be in direct contact with the sampled fluid.

Clearly, bailers and other grab type samplers are illsuited for low-flow sampling since they will cause repeated disturbance and mixing of stagnant water in the casing and the dynamic water in the screened interval. Similarly, the use of inertial lift foot-valve type samplers may cause too much disturbance at the point of sampling. Use of these devices also tends to introduce uncontrolled and unacceptable operator variability.

Summanes of advantages and disadvantages of vanous sampling devices are listed in Herzog et al. (1991), U. S. EPA (1992). Parker (1994) and Thumblad (1994).

E. Pump Installation

Dedicated sampling devices (fett in the well) capable of pumping and sampling are preferred over <u>any</u> other type of device. Any portable sampling device should be slowly and carefully lowered to the middle of the screened interval or slightly above the middle (e.g., 1-1.5 m below the top of a 3 m screen). This is to minimize excessive mixing of the stagnant water in the casing above the screen with the screened interval zone water, and to minimize resuspension of solids which will have collected at the bottom of the well. These two disturbance effects have been shown to directly affect the time required for purging. There also appears to be a direct correlation between size of portable sampling devices relative to the well bore and resulting purge volumes and times. The key is to minimize disturbance of water and solids in the well casing.

F. Filtration

Decisions to filter samples should be dictated by sampling objectives rather than as a fix for poor sampling practices, and field-filtering of certain constituents should not be the default. Consideration should be given as to what the application of field-filtration is trying to accomplish. For assessment of truly dissolved (as opposed to operationally dissolved (i.e., samples filtered with 0.45 µm filters)) concentrations of major ions and trace metals, 0.1 µm filters are recommended although 0.45 µm filters are normally used for most regulatory programs. Alkalimity samples must also be filtered if significant particulate calcium carbonate is suspected, since this material is likely to impact alkalimity titration results (although filtration itself may alter the CO₂ composition of the sample and, therefore, affect the results)

Although filtration may be appropriate, filtration of a sample may cause a number of unintended changes to occur (e.g. oxidation, aeration) possibly leading to filtration-induced artifacts during sample analysis and uncertainty in the results. Some of these unintended changes may be unavoidable but the factors leading to them must be recognized. Deleterious effects can be minimized by consistent application of certain filtration guidelines. Guidelines should address selection of filter type, media, pore size, etc. in order to identify and minimize potential sources of uncertainty when filtering samples.

In-line filtration is recommended because it provides better consistency through less sample handling, and minimizes sample exposure to the atmosphere. In-line filters are available in both disposable (barrel filters) and nondisposable (in-line filter holder, flat membrane filters) formats and various filter pore sizes (0 1-5 0 µm). Disposable filter cartridges have the advantage of greater sediment handling capacity when compared to traditional membrane filters Filters must be pre-rinsed following manufacturer's recommendations. If there are no recommendations for rinsing, pass through a minimum of 1 L of ground water following purging and prior to sampling. Once filtration has begun, a filter cake may develop as particles larger than the pore size accumulate on the filter membrane. The result is that the effective pore diameter of the membrane is reduced and particles smaller than the stated pore size are excluded from the filtrate. Possible corrective measures include prefiltering (with larger pore size filters), minimizing particle loads to begin with, and reducing sample volume

G. Monitoring of Water Level and Water Quality Indicator Parameters

Check water level periodically to monitor drawdown in the well as a guide to flow rate adjustment. The goal is minimal drawdown (<0.1 m) during purging. This goal may be difficult to achieve under some circumstances due to geologic heterogeneities within the screened interval, and may require adjustment based on site-specific conditions and personal expenence. In-line water quality indicator parameters should be continuously monitored during purging. The water quality

indicator parameters monitored can include pH, redox potential, conductivity, dissolved oxygen (DO) and turbidity. The last three parameters are often most sensitive. Pumping rate, drawdown, and the time or volume required to obtain stabilization of parameter readings can be used as a future guide to purge the well. Measurements should be taken every three to five minutes if the above suggested rates are used. Stabilization is achieved after all parameters have stabilized for three successive readings. In lieu of measuring all five parameters, a minimum subset would include pH, conductivity, and turbidity or DO. Three successive readings should be within ± 0.1 for pH, ± 3% for conductivity, ± 10 mv for redox potential, and ± 10% for turbidity and DO. Stabilized purge indicator parameter trends are generally obvious and follow either an exponential or asymptotic change to stable values during purging. Dissolved oxygen and turbidity usually require the longest time for stabilization. The above stabilization guidelines are provided for rough estimates based on expenence.

H. Sampling, Sample Containers, Preservation and Decontamination

Upon parameter stabilization, sampling can be initiated. If an in-line device is used to monitor water quality parameters, it should be disconnected or bypassed during sample collection. Sampling flow rate may remain at established purge rate or may be adjusted slightly to minimize aeration, bubble formation, turbulent filling of sample bottles, or loss of volatiles due to extended residence time in tubing Typically, flow rates less than 0.5 L/min are appropriate. The same device should be used for sampling as was used for purging. Sampling should occur in a progression from least to most contaminated well, if this is known. Generally, volatile (e.g., solvents and tuel constituents) and gas sensitive (e.g., Fe2. CH., H,S/HS, atkalinity) parameters should be sampled first. The sequence in which samples for most inorganic parameters are collected is immaterial unless filtered (dissolved) samples are desired. Filtering should be done last and in-line filters should be used as discussed above. During both well purging and sampling, proper protective clothing and equipment must be used based upon the type and level of contaminants present

The appropriate sample container will be prepared in advance of actual sample collection for the analytes of interest and include sample preservative where necessary Water samples should be collected directly into this container from the pump tubing

Immediately after a sample bottle has been filled, it must be preserved as specified in the site (OAPP). Sample preservation requirements are based on the analyses being performed (use site OAPP, FSP, RCRA guidance document [U S EPA, 1992] or EPA SW-846 (U.S. EPA, 1982]). It may be advisable to add preservatives to sample bottles in a controlled setting prior to entering the field in order to reduce the chances of improperty preserving sample bottles or

introducing field contaminants into a sample bottle while adding the preservatives.

The preservatives should be transferred from the chemical bottle to the sample container using a disposable polyethylene pipet and the disposable pipet should be used only once and then discarded.

After a sample container has been fifled with ground water, a TeflonTM (or tin)-lined cap is screwed on tightly to prevent the container from leaking. A sample label is filled out as specified in the FSP. The samples should be stored inverted at 4°C.

Specific decontamination protocols for sampling devices are dependent to some extent on the type of device used and the type of contaminants encountered. Refer to the site QAPP and FSP for specific requirements.

I. Blanks

The following blanks should be collected:

- (1) field blank, one field blank should be collected from each source water (distilled/deionized water) used for sampling equipment decontamination or for assisting well development procedures
- (2) equipment blank one equipment blank should be taken prior to the commencement of field work, from each set of sampling equipment to be used for that day. Refer to site QAPP or FSP for specific requirements.
- (3) trip blank: a tnp blank is required to accompany each volatile sample shipment. These blanks are prepared in the laboratory by filling a 40-mL volatile organic analysis (VOA) bottle with distilled/deionized water.

V. Low-Permeability Formations and Fractured Rock

The overall sampling program goals or sampling objectives will drive how the sampling points are located, installed, and choice of sampling device. Likewise, site-specific hydrogeologic factors will affect these decisions. Sites with very low permeability formations or fractures causing discrete flow channels may require a unique monitoring approach. Unlike water supply wells, wells installed for ground-water quality assessment and restoration programs are often installed in low water-yielding settings (e.g., clays, silts). Alternative types of sampling points and sampling methods are often needed in these types of environments, because low-permeability settings may require extremely low-flow purging (<0.1 L/min) and may be technology-limited. Where devices are not readily available to pump at such low flow rates, the primary consideration is to avoid dewatering of

the well screen. This may require repeated recovery of the water during purging while leaving the pump in place within the well screen.

Use of low-flow techniques may be impractical in these settings, depending upon the water recharge rates. The sampler and the end-user of data collected from such wells need to understand the limitations of the data collected; i.e., a strong potential for underestimation of actual contaminant concentrations for volatile organics, potential false negatives for filtered metals and potential false positives for unfiltered metals. It is suggested that compansons be made between samples recovered using low-flow purging techniques and samples recovered using passive sampling techniques (i.e., two sets of samples). Passive sample collection would essentially entail acquisition of the sample with no or very little purging using a dedicated sampling system instafled within the screened interval or a passive sample collection device.

A. Low-Permeability Formations (<0.1 L/min recharge)

1 Low-Flow Purging and Sampling with Pumps

- a "portable or non-dedicated mode" Lower the pump (one capable of pumping at <0.1 L/min) to mid-screen or slightly above and set in place for minimum of 48 hours (to lessen purge volume requirements). After 48 hours, use procedures listed in Part IV above regarding monitoring water quality parameters for stabilization, etc., but do not dewater the screen. If excessive drawdown and slow recovery is a problem, then alternate approaches such as those listed below may be better.
- b "dedicated mode" Set the pump as above at least a week prior to sampling, that is, operate in a dedicated pump mode. With this approach significant reductions in purge volume should be realized. Water quality parameters should stabilize quite rapidly due to less disturbance of the sampling zone.

2. Passive Sample Collection

Passive sampling collection requires insertion of the device into the screened interval for a sufficient time period to allow flow and sample equilibration before extraction for analysis. Conceptually, the extraction of water from low yielding formations seems more akin to the collection of water from the unsaturated zone and passive sampling techniques may be more appropriate in terms of obtaining "representative" samples. Satisfying usual sample volume requirements is typically a problem with this approach and some latitude will be needed on the part of regulatory entities to achieve sampling objectives.

B. Fractured Rock

In fractured rock formations, a low-flow to zero purging approach using pumps in conjunction with packers to isolate the sampling zone in the borehole is suggested. Passive multi-layer sampling devices may also provide the most "representative" samples. It is imperative in these settings to identify flow paths or water-producing fractures prior to sampling using tools such as borehole flowmeters and/or other geophysical tools.

After identification of water-bearing fractures, install packer(s) and pump assembly for sample collection using low-flow sampling in "dedicated mode" or use a passive sampling device which can isolate the identified water-bearing fractures.

VI. Documentation

The usual practices for documenting the sampling event should be used for low-flow purging and sampling techniques. This should include, at a minimum information on the conduct of purging operations (flow-rate, drawdown, water-quality parameter values, volumes extracted and times for measurements), field instrument calibration data, water sampling forms and chain of custody forms. See Figures 2 and 3 and "Ground Water Sampling Workshop.— A Workshop Summary" (U. S. EPA, 1995) for example forms and other documentation suggestions and information. This information coupled with laboratory analytical data and validation data are needed to judge the "useability" of the sampling data.

VII. Notice

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ject		Site		Y	_ Well No		Date		
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		Tubing type				Water Level			
		Other Infor							
npling Personnel									
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Information 2 in = 617 ml/ft, 4 in = 2470 ml/ft. $Vol_{e_{e_1}} = \pi r^e h_e \ Vol_{e_{e_{e_1}}} = 4/3\pi \ r^e$

Type of Samples Coflected

Figure 3 Ground Water Sampling Log (with automatic data logging for most water quality parameters)

Project	Site	Well No	Date	
Well Depth	Screen Length	Well Diame	eter Casing 1	ype
Sampling Device	Tubing ty	pe	Water Level _	
Measuring Point	Other	Infor		
Sampling Personnel_	· · · · · · · · · · · · · · · · · · ·			

Time	Pump Rate	Turbidity	Alkalinity	[] Conc	Notes
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Type of Samples Collected

Information. 2 in = 617 ml/ft, 4 in = 2470 ml/ft. $Vol_{ext} = \pi r^2 h_s \ Vol_{aphase} = 4/3\pi \ r^2$



USER'S GUIDE FOR POLYETHYLENE-BASED PASSIVE DIFFUSION BAG SAMPLERS TO OBTAIN VOLATILE ORGANIC COMPOUND CONCENTRATIONS IN WELLS

PART 1: DEPLOYMENT, RECOVERY, DATA INTERPETATION, AND QUALITY CONTROL AND ASSURANCE

Water-Resources Investigations Report 01-4060

Prepared in cooperation with the

U.S. AIR FORCE
U.S. NAVAL FACILITIES ENGINEERING COMMAND
U.S. ENVIRONMENTAL PROTECTION AGENCY
FEDERAL REMEDIATION TECHNOLOGIES ROUNDTABLE
DEFENSE LOGISTICS AGENCY
U.S. ARMY CORPS OF ENGINEERS and
INTERSTATE TECHNOLOGY REGULATORY COOPERATION WORK GROUP

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User's Guide for Polyethylene-Based Passive Diffusion Bag Samplers to Obtain Volatile Organic Compound Concentrations in Wells

Part 1: Deployment, Recovery, Data Interpretation, and Quality Control and Assurance

By Don A. Vroblesky

U.S. Geological Survey

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1 Compounds tested under laboratory conditions for use with passive diffusion bag samplers											

Conversion Factors, Vertical Datum, Acronyms, and Abbreviations

Multiply .	Ву	io obtain
	Length	
inch (in)	25 4	millimeter
foot (ft)	0 3048	meter
mule (mi)	1 609	kılometer
	Area	
square mile (mi ²)	2 590	square kilometer
·	Flow	
foot per day (ft/d)	0 3048	meter per day
foot squared per day (ft²/d)	0 09294	meter squared per day
gallon per minute (gal/min)	0 06308	liter per second
gallon per day (gal/d)	0 003785	cubic meter per day
inch per year (in/yr)	25 4	mıllımeter per year
	Volume	
gallon (gal)	3 785	liter

Temperature is given in degrees Celsius (°C), which can converted to degrees Fahrenheit (°F) by the following equation: °F = 9/5 (°C) + 32 Sea level refers to the National Geodetic Vertical Datum of 1929 (NGVD of 1929)—a geodetic datum derived from a general adjustment of the first-order level nets of the United States and Canada, formerly called Sea Level Datum of 1929.

Chemical concentration in water is expressed in metric units as milligrams per liter (mg/L) or micrograms per liter (µg/L)

	Additional Abbreviations
EDB	1,2-Dibromomethane
AFCEE	Air Force Center for Environmental Excellence
cDCE .	cis-1,2-Dibromoethene
ft³/d	cubic feet per day
ft³/mg	cubic feet per milligram
°C	degrees Celsius
g	gram
ПRC	Interstate Technology Regulatory Cooperation
LDPE	low-density polyethylene
L	liter
μg	microgram
μm	micrometer
μί.	microliter
- 1	milligram
mL	milliliter
m L/m in	milliliter per minute
MTBE	Methyl-tert-butyl ether
NAVFAC	Naval Facilities Engineering Command
NAPL	non-aqueous phase liquid
PDB	passive diffusion bag
PCE į	Tetrachloroethene
TCE	Trichloroethene
USEPA	U.S. Environmental Protection Agency
USGS	U.S. Geological Survey
VOA	Volatile organic analysis
voc	Volatile organic compound

User's Guide for Polyethylene-Based Passive Diffusion Bag Samplers to Obtain Volatile Organic Compound Concentrations in Wells

Part 1: Deployment, Recovery, Data Interpretation, and Quality Control and Assurance

By Don A. Vroblesky

EXECUTIVE SUMMARY

Water-filled passive diffusion bag (PDB) samplers described in this report are suitable for obtaining concentrations of a variety of volatile organic compounds (VOCs) in ground water at monitoring wells. The suggested application of the method is for long-term monitoring of VOCs in ground-water wells at well-characterized sites.

The effectiveness of the use of a single PDB sampler in a well is dependent on the assumption that there is horizontal flow through the well screen and that the quality of the water is representative of the ground water in the aquifer directly adjacent to the screen. If there are vertical components of intrabore-hole flow, multiple intervals of the formation contributing to flow, or varying concentrations of VOCs vertically within the screened or open interval, then a multiple deployment of PDB samplers within a well may be more appropriate for sampling the well.

A typical PDB sampler consists of a low-density polyethylene (LDPE) lay-flat tube closed at both ends and containing deionized water. The sampler is positioned at the target horizon of the well by attachment to a weighted line or fixed pipe.

The amount of time that the sampler should be left in the well prior to recovery depends on the time required by the PDB sampler to equilibrate with ambient water and the time required for the environmental disturbance caused by sampler deployment to return to ambient conditions. The rate that the water within the PDB sampler equilibrates with ambient water depends on multiple factors, including the type of compound being sampled and the water temperature. The concentrations of benzene, cis-1,2-dichloroethene,

tetrachlorethene, trichloroethene, toluene, naphthalene, 1,2-dibromoethane, and total xylenes within the PDB samplers equilibrated with the concentrations in an aqueous mixture of those compounds surrounding the samplers under laboratory conditions within approximately 48 hours at 21 degrees Celsius (°C) A subsequent laboratory study of mixed VOCs at 10 °C showed that tetrachloroethene and trichloroethene were equilibrated by about 52 hours, but other compounds required longer equilabration times. Chloroethane, cis-1,2-dichloroethene, trans-1,2-dichloroethene, and 1,1-dichloroethene were not equilibrated at 52 hours, but appeared to be equilibrated by the next sampling point at 93 hours. Vinyl chloride, 1,1,1-trichloroethane, 1,2-dichloroethane, and 1,1-dichloroethane were not equilibrated at 93 hours, but were equilibrated by the next sampling point at 166 hours. Different equilibration times may exist for other compounds. Differences in equilibration times, if any, between single-solute or mixed VOC solutions have not yet been thoroughly examined

The samplers should be left in place long enough for the well water, contaminant distribution, and flow dynamics to restabilize following sampler deployment. Laboratory and field data suggest that 2 weeks of equilibration probably is adequate for many applications; therefore, a minimum equilibration time of 2 weeks is suggested. In less permeable formations, longer equilibration times may be required. When applying PDB samplers in waters colder than previously tested (10 °C) or for compounds without sufficient corroborating data, a side-by-side comparison with conventional methodology is advisable to justify the field equilibration time

Following the initial equilibration period, the samplers maintain equilibrium concentrations with the ambient water until recovery. Thus, there is no specified time for sampler recovery after initial equilibration. PDB samplers routinely have been left in ground waters having concentrations of greater than 500 parts per million (ppm) of trichloroethene for 3 months at a time with no loss of bag integrity, and at one site, the PDB samplers have been left in place in VOC-contaminated ground water for 1 year with no reported loss of sampler integrity. The effects of long-term (greater than 1 month) PDB-sampler deployment on sampler and sample integrity have not yet been thoroughly tested for a broad range of compounds and concentrations, however Moreover, in some environments, development of a biofilm on the polyethylene may be a consequence of long-term deployment. Investigations of semipermeable membrane devices (SPMDs) have shown that the transfer of some compounds across a heavily biofouled polyethylene membrane may be reduced, but not stopped. If a heavy organic coating is observed on a PDB sampler, it is advisable to determine the integrity of the sample by comparison to a conventional sampling method before continuing to use PDB samplers for long-term deployment in that well.

Recovery consists of removing the samplers from the well and immediately transferring the enclosed water to 40-milliliter sampling vials for analysis. The resulting concentrations represent an integration of chemical changes over the most recent portion of the equilibration period (approximately 48 to 166 hours, depending on the water temperature and the type of compound).

The method has both advantages and limitations when compared to other sampling methods. Advantages include the potential for PDB samplers to eliminate or substantially reduce the amount of purge water associated with sampling. The samplers are relatively inexpensive and easy to deploy and recover. Because PDB samplers are disposable, there is no downhole equipment to be decontaminated between wells, and there is a minimum amount of field equipment required. The samplers also have the potential to delineate contaminant stratification in the formation across the open or screened intervals of monitoring wells where vertical hydraulic gradients are not present. In addition, the samplers integrate concentrations over time, which may range between about 48 to 166 hours depending on the compound of interest. Because the pore size of LDPE is only about

10 angstroms or less, sediment does not pass through the membrane into the bag. Thus, PDB samplers are not subject to interferences from turbidity. In addition, none of the data collected suggest that VOCs leach from the LDPE material, or that there is a detrimental effect on the VOC sample from the PDB material.

Water-filled polyethylene PDB samplers are not appropriate for all compounds. The samplers are not suitable for inorganic ions and have a limited applicability for non-VOCs and for some VOCs. For example, although methyl-tert-butyl ether and acetone and most semivolatile compounds are transmitted through the polyethylene bag, laboratory tests have shown that the resulting concentrations were lower than in ambient water. A variety of factors influence the ability of compounds to diffuse through the polyethylene. These factors include the molecular size and shape and the hydrophobic nature of the compound. Unpublished laboratory test data of semivolatile compounds in contact with PDB samplers showed a higher concentration of phthalates inside the PDB sampler than outside the PDB sampler, suggesting that the polyethylene may contribute phthalates to the enclosed water. Thus, the samplers should not be used to sample for phthalates.

VOC concentrations in PDB samplers represent concentrations in the vicinity of the sampler within the well screen or open interval. This may be a limitation for PDB samplers and some other types of sampling, such as low-flow sampling, if the ground-water contamination is above or below the screen or not in the sample intervals providing water movement to the PDB samplers. If there is a vertical hydraulic gradient in the well, then the concentrations in the sampler may represent the concentrations in the water flowing vertically past the sampler rather than in the formation directly adjacent to the sampler. Vertically spaced multiple PDB samplers may be needed in chemically stratified wells or where flow patterns through the screen change as a result of ground-water pumping or seasonal water-level fluctuations.

The purposes of this document are to present methods for PDB sampler deployment, and recovery; to discuss approaches to determine the applicability of passive diffusion samplers; and to discuss various factors influencing interpretation of the data. The intended audience for the methodology sections of this report is managers and field personnel involved in using PDB samplers. The discussion of passive diffusion sampler applicability and interpretation of the data is

suited for project managers, technical personnel, and the regulatory community. Part 2 of this report presents case studies of PDB sampler field applications.

INTRODUCTION

The use of PDB samplers for collecting ground-water samples from wells offers a cost-effective approach to long-term monitoring of VOCs at well-characterized sites (Vroblesky and Hyde, 1997; Gefell and others, 1999). The effectiveness of the use of a single PDB sampler in a well is dependent on the assumption that there is horizontal flow through the well screen and that the quality of the water is representative of the ground water in the aquifer directly adjacent to the screen. If there are vertical components of intra-borehole flow, multiple intervals of the formation contributing to flow, or varying concentrations of VOCs vertically within the screened or open interval, then deployment of multiple PDB samplers within a well may be more appropriate for sampling the well.

The samplers consist of deionized water enclosed in a LDPE sleeve (fig. 1) and are deployed adjacent to a target horizon within a screened or open interval of a well. The suggested application is for long-term monitoring of VOCs in ground-water wells Where the screened interval is greater than 10 feet (ft), the potential for contaminant stratification and/or intraborehole flow within the screened interval is greater than in screened intervals shorter than 10 ft. It is important that the vertical distribution of contaminants be determined in wells having 10-ft-long well screens. and that both the vertical distribution of contaminants and the potential for intra-borehole flow be determined in wells having screens longer than 10 ft. For many VOCs of environmental interest (table 1), the VOC concentration in water within the sampler approaches the VOC concentration in water outside of the PDB sampler over an equilibration period. The resulting concentrations represent an integration of chemical changes over the most recent part of the equilibration period (approximately 48 to 166 hours, depending on the water temperature and the type of compound being sampled). The approach is inexpensive and has the potential to eliminate or substantially reduce the amount of purge water removed from the well.

A variety of PDB samplers have been utilized in well applications (fig. 1). Although the samplers vary in specific construction details, a typical PDB sampler consists of a 1- to 2-ft-long LDPE tube closed at both ends and containing laboratory-grade deionized water (fig. 1). The typical diameter for PDB samplers used in a 2-inch-diameter well is approximately 1.2 inches; however, other dimensions may be used to match the well diameter. Equilibration times may be longer for larger diameter PDB samplers. On the outside of the PDB sampler, a low-density polyethylene-mesh sometimes is used for protection against abrasion in open boreholes and as a means of attachment at the prescribed depth. The PDB sampler can be positioned at the target horizon by attachment to a weighted line or by attachment to a fixed pipe.

PDB samplers for use in wells are available commercially. Authorized distributors as of March 2001 are Columbia Analytical Services (800-695-7222) and Eon Products (800-474-2490) A current list of vendors and PDB-sampler construction details can be obtained from the U.S. Geological Survey Technology Transfer Enterprise Office, Mail Stop 211, National Center, 12201 Sunrise Valley Drive, Reston, Virginia 20192 (telephone 703-648-4344; fax 703-648-4408). PDB samplers employ patented technology (U S patent number 5,804,743), and therefore, require that the user purchase commercially produced samplers from a licensed manufacturer or purchase a nonexclusive license for sampler construction from the U.S Geological Survey Technology Enterprise Office at the above address.

The purposes of this document are to present methods for PDB sampler deployment, and recovery, to discuss approaches for determining the applicability of passive diffusion samplers, and to discuss various factors influencing interpretation of the data. The intended audience for the methodology sections of this report is managers and field personnel involved in using PDB samplers. The discussion of PDB sampler applicability and interpretation of the data is suited for project managers, technical personnel, and the regulatory community. Part 2 of this report presents case studies of PDB-sampler field applications.

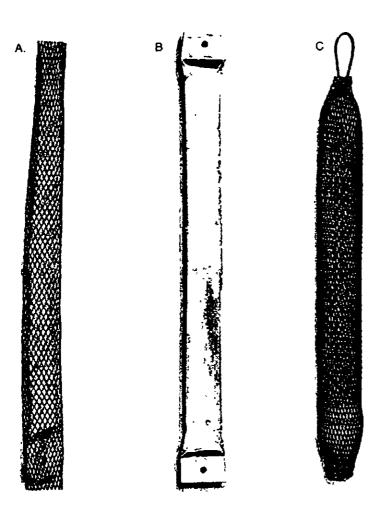


Figure 1. Typical water-filled passive diffusion bag samplers used in wells, including (A) diffusion bag with polyethylene mesh, (B) diffusion bag without mesh, and (C) bag and mesh attached to bailer bottom.

Table 1. Compounds tested under laboratory conditions for use with passive diffusion bag samplers [From Vroblesky and Campbell, 2001]

Benzene	, 2 Chlorovinyl ether	cis-1,2-Dichloroethene	1,1,1-Trichloroethane
Bromodichloromethane	Dibromochloromethane	trans-1,2-Dichlomethene	1,1,2-Trichloroethane
Bromoform	Dibromomethane	1,2-Dichloropropane	Trichloroethene
Chlorobenzene .	1,2-Dichlorobenzene	cis-Dichloropropene	Trichlorofluoromethane
Carbon tetrachioride	1,3-Dichlorobenzene	1-1,2-Dibromoethane	1,2,3-Trichloropropane
Chloroethane	1,4-Dichlorobenzene	trans-1,3-Dichloropropene	1,1,2,2-Tetrachloroethanc
Chloroform	Dichlorodifluoromethane	Ethyl benzene	Tetrachloroethene
Chloromethanc	1,2-Dichlomethane	Naphthalene	Vinyl chloride
	1,1-Dichloroethene	Toluene	Total xylenes
Testeo compounds sh between	owing poor correlation (aver en diffusion-sampler water	age tifferences in concentration in labor	atory tests of the second
Acetone* .	Methyl-tert-butyl ether	Styrene	,

^{*}T M Sivavec and S S Baghel, General Electric Company, written commun., 2000

User's Guide for Polyethylene-Based Passive Diffusion Bag Samplers to Obtain Volatile Organic Compound Concentrations in Wells—Part 1: Deployment, Recovery, Data Interpretation, and Quality Control and Assurance

Summary of Passive Diffusion Bag Sampler Advantages and Limitations

Advantages

- 1. PDB samplers have the potential to eliminate or substantially reduce the amount of purge water associated with sampling.
 - 2. PDB samplers are inexpensive.
 - 3. The samplers are easy to deploy and recover.
- 4. Because PDB samplers are disposable, there is no downhole equipment to be decontaminated between wells.
 - 5 A minimal amount of field equipment is required.
- 6. Sampler recovery is rapid. Because of the small amount of time and equipment required for the sampling event, the method is practical for use where access is a problem or where discretion is desirable (that is, residential communities, business districts, or busy streets where vehicle traffic control is a concern).
- 7. Multiple PDB samplers, distributed vertically along the screened or open interval, may be used in conjunction with borehole flow meter testing to gain insight on the movement of contaminants into and out of the well screen or open interval or to locate the zone of highest concentration in the well. Analytical costs when using multiple PDB samplers sometimes can be reduced by selecting a limited number of the samplers for laboratory analysis based on screening by using field gas chromatography at the time of sample collection
- 8. Because the pore size of LDPE is only about 10 angstroms or less, sediment does not pass through the membrane into the bag. Thus, PDB samplers are not subject to interferences from turbidity. In addition, none of the data collected suggest that VOCs leach from the LDPE material or that there is a detrimental effect from the PDB material on the VOC sample.

Limitations

1. PDB samplers integrate concentrations over time. This may be a limitation if the goal of sampling is to collect a representative sample at a point in time in an aquifer where VOC-concentrations substantially change more rapidly than the samplers equilibrate. Laboratory results obtained indicate that a variety of compounds equilibrated within 48 hours at 21 °C (Vroblesky and Campbell, 2001). Vinyl chloride, 1,1,1-trichloroethane, 1,2-dichloroethane, and 1,1-dichloroethane may require between 93 and 166 hours to equilibrate at 10 °C (T.M. Sivavec and S.S. Baghel, General Electric Company, written commun., 2000). The initial equilibration under field conditions may be longer to allow

well water, contaminant distribution, and flow dynamics to restabilize following sampler deployment.

- 2. Water-filled polyethylene PDB samplers are not appropriate for all compounds. For example, although methyl-tert-butyl ether and acetone (Vroblesky, 2000; Paul Hare, General Electric Company, oral commun., 2000) and most semivolatile compounds are transmitted through the polyethylene bag, laboratory tests have shown that the resulting concentrations were lower than in ambient water. A variety of factors influence the ability of compounds to diffuse through the polyethylene membrane. These factors include the molecular size and shape and the hydrophobic nature of the compound. Compounds having a cross-sectional diameter of about 10 angstroms or larger (such as humic acids) do not pass through the polyethylene because the largest (transient) pores in polyethylene do not exceed about 10 angstroms in diameter (Flynn and Yalkowsky, 1972; Hwang and Kammermeyer, 1975; Comyn, 1985). The samplers are not appropriate for hydrophilic polar molecules, such as inorganic ions. A detailed discussion of the relation between hydrophobicity and compound transport through polyethylene can be found in Gale (1998) Unpublished laboratory test data (D.A. Vroblesky, U.S. Geological Survey, written commun., 1998) of semivolatile compounds in contact with PDB samplers showed a higher concentration of phthalates inside the PDB sampler than outside the PDB sampler, suggesting that the polyethylene may contribute phthalates to the enclosed water. Thus, the samplers should not be used to sample for phthalates.
- 3. PDB samplers rely on the free movement of water through the well screen. In situations where ground water flows horizontally through the well screen, the VOC concentrations in the open interval of the well probably are representative of the aquifer water in the adjacent formation (Gillham and others, 1985; Robin and Gillham, 1987; Kearl and others, 1992; Powell and Puls, 1993; Vroblesky and Hyde, 1997). In these situations, the VOC concentration of the water in contact with the PDB samplers, and therefore, the water within the diffusion samplers, probably represents local conditions in the adjacent aquifer. However, if the well screen is less permeable than the aquifer or the sandpack, then under ambient conditions, flowlines may be diverted around the screen. Such a situation may arise from inadequate well development or from iron bacterial fouling of the well screen. In this case, the VOC concentrations in the PDB samplers may not represent concentrations in

the formation water because of inadequate exchange across the well screen. PDB samplers have not yet been adequately tested to determine their response under such conditions

- 4. VOC concentrations in PDB samplers represent ground-water concentrations in the vicinity of the screened or open well interval that move to the sampler under ambient flow conditions. This is a limitation if the ground-water contamination lies above or below the well screen or open interval, and requires the operation of a pump to conduct contaminants into the well for sampling.
- 5. In cases where the well screen or open interval transects zones of differing hydraulic head and variable contaminant concentrations, VOC concentrations obtained using a PDB sampler may not reflect the concentrations in the aquifer directly adjacent to the sampler because of vertical transport in the well. However, a vertical array of PDB samplers, used in conjunction with borehole flow meter testing, can provide insight on the movement of contaminants into or out of the well. This information then can be used to help determine if the use of PDB samplers is appropriate for the well, and to select the optimal vertical location(s) for the sampler deployment.
- 6. In wells with screens or open intervals with stratified chemical concentrations, the use of a single PDB sampler set at an arbitrary (by convention) depth may not provide accurate concentration values for the most contaminated zone. However, multiple PDB samplers distributed vertically along the screened or open interval, in conjunction with pump sampling (as appropriate), can be used to locate zone(s) of highest concentration in the well. Multiple PDB samplers also may be needed to track the zone of maximum concentration in wells where flow patterns through the screened interval change as a result of ground-water pumping or seasonal water-table fluctuations

PASSIVE DIFFUSION BAG SAMPLER DEPLOYMENT

A variety of approaches can be used to deploy the PDB samplers in wells. A typical deployment approach, described in this section, is to attach the PDB samplers to a weighted line. It also is acceptable to attach the weights directly to the PDB sampler if the attachment point is of sufficient strength to support the weight. The weights attached to the bottom of the

line are stainless steel and can be reused, but must be thoroughly decontaminated with a detergent before the first use or before using in a different well. Rope, such as 90 pound, 3/16 inch braided polyester, can be used as the line for single-use applications if it is of sufficient strength to support the weight and sampler, is nonbuoyant, and is subject to minimal stretch; however, the rope should not be reused because of the high potential for cross contamination. Stainless-steel or Teflon-coated stainless-steel wire is preferable. The weighted lines should not be reused in different wells to prevent carryover of contaminants. A possible exception is coated stainless-steel wire, which can be reused after sufficient decontamination. An alternative deployment approach, not discussed in this section, is to attach the PDB samplers to a fixed pipe in the well (Vroblesky and Peters, 2000, p. 3; also included in Part 2 of this publication). The PDB samplers should not contact non-aqueous phase liquid (NAPL) during deployment or retrieval to prevent cross contamination. An approach that can be utilized to deploy diffusion samplers through a layer of floating NAPL is described in the field test at Naval Station North Island, California (Vroblesky and Peters, 2000, p. 3-4; also included in Part 2 of this publication).

If the PDB sampler is to be compared with a conventional pumping approach to sampling, then it is suggested that both the pump and the PDB sampler be deployed at the same time, with the sampler attached near (such as directly below) the pump inlet. This approach eliminates potential concentration differences between the two methods that may result from well disturbance during equipment removal and deployment at the time of sampling. An alternative method is to deploy the PDB samplers independently of the pumps and recover the samplers immediately prior to placing the pump down the well.

PDB samplers are available either prefilled with laboratory-grade deionized water or unfilled. The unfilled samplers are equipped with a plug and funnel to allow for field filling and sample recovery. To fill these samplers, remove the plug from the sampler bottom, insert the short funnel into the sampler, and pour laboratory-grade deionized water into the sampler. The sampler should be filled until water rises and stands at least half way into the funnel. Remove excess bubbles from the sampler. Remove the funnel and reattach the plug. A small air bubble from the plug is of no concern.

The following steps should be used for deploying PDB samplers in wells:

- 1. Measure the well depth and compare the measured depth with the reported depth to the bottom of the well screen from well-construction records. This is to check on whether sediment has accumulated in the bottom of the well, whether there is a nonscreened section of pipe (sediment sump) below the well screen, and on the accuracy of well-construction records. If there is an uncertainty regarding length or placement of the well screen, then an independent method, such as video imaging of the well bore, is strongly suggested.
- 2. Attach a stainless-steel weight to the end of the line. Sufficient weight should be added to counterbalance the buoyancy of the PDB samplers. This is particularly important when multiple PDB samplers are deployed. One approach, discussed in the following paragraphs, is to have the weight resting on the bottom of the well, with the line taut above the weight. Alternatively, the PDB sampler and weight may be suspended above the bottom, but caution should be exercised to ensure that the sampler does not shift location. Such shifting can result from stretching or slipping of the line or, if multiple samplers are attached end-to-end rather than to a weighted line, stretching of the samplers
- 3. Calculate the distance from the bottom of the well, or top of the sediment in the well, up to the point where the PDB sampler is to be placed. A variety of approaches can be used to attach the PDB sampler to the weight or weighted line at the target horizon. The field-fillable type of PDB sampler is equipped with a hanger assembly and weight that can be slid over the sampler body until it rests securely near the bottom of the sampler. When this approach is used with multiple PDB samplers down the same borehole, the weight should only be attached to the lowermost sampler. An additional option is to use coated stainless-steel wire as a weighted line, making loops at appropriate points to attach the upper and lower ends of PDB samplers. Where the PDB sampler position varies between sampling events, movable clamps with rings can be used. When using rope as a weighted line, a simple approach is to tie knots or attach clasps at the appropriate depths. Nylon cable ties or stainless-steel clips inserted through the knots can be used to attach the PDB samplers. An approach using rope as a weighted line with knots tied at the appropriate sampler-attachment points is discussed below.
- (a) For 5-ft-long or shorter well screens, the center point of the PDB sampler should be the vertical midpoint of the saturated well-screen length. For example, if the well screen is at a depth of 55 to 60 ft below the top of casing, and the measured depth of the well is 59 ft, then the bottom of the well probably has filled with sediment. In this case, the midpoint of the sampler between the attachment points on the line will be midway between 55 and 59 ft, or at 57 ft. Thus, for a 1.5-ft-long sampler, the attachment points on a weighted line should be tied at distances of 1.25 ft (2 ft -0.75 ft) and 2.75 ft (2 ft +0.75 ft) from the top of the sediment in the well, or the bottom of the well, making adjustments for the length of the attached weight. When the PDB sampler is attached to the line and installed in the well, the center of the sampler will be at 57-ft depth. If, however, independent evidence is available showing that the highest concentration of contaminants enters the well from a specific zone within the screened interval, then the PDB sampler should be positioned at that interval.
- (b) For 5- to 10-ft-long well screens, it is advisable to utilize multiple PDB samplers vertically along the length of the well screen for at least the initial sampling (fig. 2) The purposes of the multiple PDB samplers are to determine whether contaminant stratification is present and to locate the zone of highest concentration. The midpoint of each sampler should be positioned at the midpoint of the interval to be sampled. For 1.5-ft-long samplers, at each sampling depth in the screened interval, make two attachment points on the weighted line at a distance of about 1.5 ft apart. The attachment points should be positioned along the weighted line at a distance from the bottom end of the weight such that the midpoint between the knots will be at the desired sampling depth along the well screen. Sampler intervals are variable, but a simple approach is to use the top knot/loop of one sampler interval as the bottom knot/loop for the overlying sampler interval.



Figure 2. Example of multiple PDB samplers prepared for deployment.

- (c) PDB samplers should not be used in wells having screened or open intervals longer than 10 ft unless used in conjunction with borehole flow meters or other techniques to characterize vertical variability in hydraulic conductivity and contaminant distribution or used strictly for qualitative reconnaissance purposes. This is because of the increased potential for cross contamination of water-bearing zones and hydraulically driven mixing effects that may cause the contaminant stratification in the well to differ from the contaminant stratification in the adjacent aquifer material. If it is necessary to sample such wells, then multiple PDB samplers should be installed vertically across the screened or open interval to determine the zone of highest concentration and whether contaminant stratification is present.
- 4. The samplers should be attached to the weights or weighted line at the time of deployment. For samplers utilizing the hanger and weight assembly,

- the line can be attached directly to the top of the sampler. PDB samplers utilizing an outer protective mesh can be attached to a weighted line by using the following procedure:
 - (a) Insert cable ties through the attachment points in the weighted line.
 - (b) At each end of the PDB sampler, weave the ends of the cable ties or clamp through the LPDE mesh surrounding the sampler and tighten the cable ties. Thus, each end of the PDB sampler will be attached to a knot/loop in the weighted line by means of a cable tie or clamp. The cable ties or clamps should be positioned through the polyethylene mesh in a way that prevents the PDB sampler from sliding out of the mesh.
 - (c) Trim the excess from the cable tie before placing the sampler down the well. Caution should be exercised to prevent sharp edges on the trimmed cable ties that may puncture the LDPE

- 5. When using PDB samplers without the protective outer mesh, the holes punched at the ends of the bag, outside the sealed portion, can be used to attach the samplers to the weighted line. Stainless-steel spring clips have been found to be more reliable than cable ties in this instance, but cable ties also work well.
- 6. Lower the weight and weighted line down the well until the weight rests on the bottom of the well and the line above the weight is taut. The PDB samplers should now be positioned at the expected depth. A check on the depth can be done by placing a knot or mark on the line at the correct distance from the top knot/loop of the PDB sampler to the top of the well casing and checking to make sure that the mark aligns with the lip of the casing after deployment.
- 7. Secure the assembly in this position. A suggested method is to attach the weighted line to a hook on the inside of the well cap. Reattach the well cap. The well should be sealed in such a way as to prevent surface-water invasion. This is particularly important in flush-mounted well vaults that are prone to flooding.
- 8 Allow the system to remain undisturbed as the PDB samplers equilibrate.

PASSIVE DIFFUSION BAG SAMPLER AND SAMPLE RECOVERY

The amount of time that the samplers should be left in the well prior to recovery depends on the time required by the PDB sampler to equilibrate with ambient water and the time required for environmental disturbances caused by sampler deployment to return to ambient conditions. The rate that the water within the PDB sampler equilibrates with ambient water depends on multiple factors, including the type of compound being sampled and the water temperature. The concentrations of benzene, cis-1,2-dichloroethene (cDCE), tetrachlorethene (PCE), trichloroethene (TCE), toluene, naphthalene, 1,2-dibromoethane (EDB), and total xylenes within the PDB samplers equilibrated with the concentrations in an aqueous mixture of those compounds surrounding the samplers under laboratory conditions within approximately 48 hours at 21 °C (Vroblesky and Campbell, 2001). A subsequent laboratory study of mixed VOCs at 10 °C showed that PCE and TCE were equilibrated by about 52 hours, but other compounds required longer equilibration times (TM, Sivavec and S.S. Baghel, General Electric Company, written commun., 2000). Chloroethane, cDCE, trans-1,2-dichloroethene, and 1,1-dichloroethene were not

equilibrated at 52 hours, but appeared to be equilibrated by the next sampling point at 93 hours. Vinyl chloride, 1,1,1-trichloroethane, 1,2-dichloroethane, and 1,1-dichloroethane were not equilibrated at 93 hours, but were equilibrated by the next sampling point at 166 hours. Different equilibration times may exist for other compounds. Differences in equilibration times, if any, between single-solute or mixed-VOC solutions have not yet been thoroughly examined.

Under field conditions, the samplers should be left in place long enough for the well water, contaminant distribution, and flow dynamics to restabilize following sampler deployment. The results of borehole dilution studies show that wells can recover to 90 percent of the predisturbance conditions within minutes to several hours for permeable to highly permeable geologic formations, but may require 100 to 1,000 hours (4 to 40 days) in muds, very fine-grained loamy sands, and fractured rock, and may take even longer in fractured shales, recent loams, clays, and slightly fractured solid igneous rocks (Halevy and others, 1967).

In general, where the rate of ground-water movement past a diffusion sampler is high, equilibration times through various membranes commonly range from a few hours to a few days (Mayer, 1976, Harrington and others, 2000). One field investigation showed adequate equilibration of PDB samplers to aquifer trichloroethene (TCE) and carbon tetrachloride (CT) concentrations within 2 days in a highly permeable aquifer (Vroblesky and others, 1999). In other investigations, PDB samplers recovered after 14 days were found to be adequately equilibrated to chlorinated VOCs (Obrien & Gere Engineers, Inc., 1997a, 1997b, Hare, 2000), therefore, the equilibration period was less than or equal to 14 days for those field conditions. Because it appears that 2 weeks of equilibration probably is adequate for many applications, a minimum equilibration time of 2 weeks is suggested. When applying PDB samplers in waters colder than previously tested (10 °C) or for compounds without sufficient corroborating field data, a side-by-side comparison with conventional sampling methodology is advisable to justify the field equilibration time.

In less permeable formations, longer equilibration times may be required. It is probable that water in the well bore eventually will equilibrate with the porewater chemistry; however, if the rate of chemical change or volatilization loss in the well bore exceeds the rate of exchange between the pore water and the well-bore water, then the PDB samplers may underestimate pore-water concentrations. Guidelines for equilibration times and applicability of PDB samplers in low-permeability formations have not yet been established. Therefore, in such situations, a side-by-side comparison of PDB samplers and conventional sampling methodology is advisable to ensure that the PDB samplers do not underestimate concentrations obtained by the conventional method. A detailed discussion of diffusion rates relevant to diffusion sampler equilibrium in slow-moving ground-water systems can be found in Harrington and others (2000)

Following the initial equilibration period, the samplers maintain equilibrium concentrations with the ambient water until recovery. Thus, there is no specified maximum time for sampler recovery. PDB samplers have routinely been left in ground waters having concentrations of greater than 500 ppm of TCE for 3 months at a time with no loss of bag integrity, and at one site, the PDB samplers have been left in place in VOC-contaminated ground water for 1 year with no reported loss of sampler integrity (Paul Hare, General Electric Company, oral commun., 2000). The effects of long-term (greater than 1 month) PDB-sampler deployment on sampler and sample integrity have not yet been thoroughly tested for a broad range of compounds and concentrations. Moreover, in some environments, development of a biofilm on the polyethylene may be a consequence of long-term deployment. Investigations of semipermeable membrane devices (SPMDs) have shown that the transfer of some compounds may be reduced, but not stopped, across a heavily biofouled polyethylene membrane (Ellis and others, 1995, Huckins and others, 1996; Huckins and others, in press). If a heavy organic coating is observed on a PDB sampler, it is advisable to determine the integrity of the sample by comparing contaminant concentrations from the PDB sampler to concentrations from a conventional sampling method before continuing to use PDB samplers for long-term deployment in that well.

Recovery of PDB samplers is accomplished by using the following approach:

- 1 Remove the PDB samplers from the well by using the attached line. The PDB samplers should not be exposed to heat or agitated.
- 2. Examine the surface of the PDB sampler for evidence of algae, iron or other coatings, and for tears in the membrane. Note the observations in a sampling field book. If there are tears in the membrane, the

- sample should be rejected. If there is evidence that the PDB sampler exhibits a coating, then this should be noted the validated concentration data.
- 3. Detach and remove the PDB sampler from the weighted line. Remove the excess liquid from the extenor of the bag to minimize the potential for cross contamination.
- 4. A variety of approaches may be used to transfer the water from the PDB samplers to 40-mL volatile organic analysis (VOA) vials. One type of commercially available PDB sampler provides a discharge device that can be inserted into the sampler. If discharge devices are used, the diameter of the opening should be kept to less than about 0.15 inches to reduce volatilization loss. Two options are presently available to recover water from the sample using discharge devices. One option involves removing the hanger and weight assembly from the sampler, inverting the sampler so that the fill plug is pointed upward, and removing the plug. The water can be recovered by directly pouring in a manner that minimizes agitation or by pouring through a VOC-discharge accessory inserted in place of the plug. The second approach involves piercing the sampler near the bottom with a small-diameter discharge tube and allowing water to flow through the tube into the VOA vials. In each case, flow rates can be controlled by tilting or manipulating the sampler. Alternatively, the PDB sampler can be cut open at one end using scissors or other cutting devices which have been decontaminated between use for different wells. Water can then be transferred to 40-ml VOA vials by gently pouring in a manner that minimizes water agitation. Acceptable duplication has been obtained using each method. Preserve the samples according to the analytical method. The sampling vials should be stored at approximately 4 °C in accordance with standard sampling protocol. Laboratory testing suggests that there is no substantial change in the VOC concentrations in PDB samplers over the first several minutes after recovery, however, the water should be transferred from the water-filled samplers to the sample bottles immediately upon recovery
- 5. A cost-effective alternative when using multiple PDB samplers in a single well is to field screen water from each sampler using gas chromatography. These results can be used to decide which of the multiple PDB samplers should be sent to an EPA-approved laboratory for standard analysis. Typically, at least the sample containing the highest concentration should be analyzed by a laboratory.

6 If a comparison is being made between concentrations obtained using PDB samplers and concentrations obtained using a conventional sampling approach, then the well should be sampled by the conventional approach soon after (preferably on the same day) recovery of the PDB sampler. The water samples obtained using PDB samplers should be sent in the same shipment, as the samples collected by the conventional approach for the respective wells. Utilizing the same laboratory may reduce analytical variability.

7. Any unused water from the PDB sampler and water used to decontaminate cutting devices should be disposed in accordance with local, state, and Federal regulations.

DETERMINING APPLICABILITY OF PASSIVE DIFFUSION BAG SAMPLERS AND INTERPRETATION OF DATA

When attempting to determine whether the use of PDB samplers is appropriate at a particular well, a common approach is to do a side-by-side comparison with a conventional sampling method during the same sampling event. This approach is strongly suggested in wells having temporal concentration variability. In a well having relatively low temporal concentration variability, comparison of the PDB-sampler results to historical concentrations may provide enough information to determine whether the PDB samplers are appropriate for the well. In general, if both PDB and conventional sampling produce concentrations that agree within a range deemed acceptable by local, state, and Federal regulatory agencies and meet the site-specific data-quality objectives, then a PDB sampler may be approved for use in that well to monitor ambient VOC concentrations. If concentrations from the PDB sampler are higher than concentrations from the conventional method, it is probable that concentrations from the PDB sampler adequately represent ambient conditions because there usually is a greater potential for dilution from mixing during sampling using conventional methods than during sampling using PDB samplers.

If, however, the conventional method produces concentrations that are significantly higher than those obtained using the PDB sampler, then it is uncertain whether the PDB-sampler concentrations represent local ambient conditions. In this case, further testing can be done to determine whether contaminant stratification and/or intra-borehole flow is present. Multiple sampling devices can be used to determine the pres-

ence of contaminant stratification, and borehole flowmeters can be used to determine whether intraborehole flow is present. When using flowmeters to measure vertical flow in screened boreholes, however, the data should be considered qualitative because of the potential for water movement through the sand pack. Borehole dilution tests (Halevy and others, 1967, Drost and others, 1968, Grisak and others, 1977; Palmer, 1993) can be used to determine whether water is freely exchanged between the aquifer and the well screen.

Once the source of the difference between the two methods is determined, a decision can be made regarding the well-specific utility of the PDB samplers Tests may show that VOC concentrations from the PDB samplers adequately represent local ambient conditions within the screened interval despite the higher VOC concentration obtained from the conventional method. This may be because the pumped samples incorporated water containing higher concentrations either from other water-bearing zones induced along inadequate well seals or through fractured clay (Vroblesky and others, 2000), from other water-bearing zones not directly adjacent to the well screen as a result of well purging prior to sampling (Vroblesky and Petkewich; 2000), or from mixing of chemically stratified zones in the vicinity of the screened interval (Vroblesky and Peters, 2000)

The mixing of waters from chemically stratified zones adjacent to the screened interval during pumping probably is one of the more important sources of apparent differences between the results obtained from PDB sampling and conventional sampling because such stratification probably is common. Vertical stratification of VOCs over distances of a few feet has been observed in aquifer sediments by using multilevel sampling devices (Dean and others, 1999; Pitkin and others, 1999), and considerable variation in hydraulic conductivity and water chemistry has been observed in an aquifer in Cape Cod, Massachusetts, on the scale of centimeters (Wolf and others, 1991, Smith and others 1991; Hess and others, 1992). Multiple PDB samplers have been used to show a change in TCE concentration of 1,130 (µg/L over a 6-ft vertical screened interval in Minnesota (Vroblesky and Petkewich, 2000). Tests using PDB samplers in screened intervals containing VOC stratification showed that the PDB-sampler data appeared to be point-specific, whereas the pumped sample integrated water over a larger interval (Vroblesky and Peters, 2000).

The decision on whether to use PDB samplers in such situations depends on the data-quality objectives for the particular site. If the goal is to determine and monitor higher concentrations or to examine contaminant stratification within the screened interval, then the PDB samplers may meet this objective. If the goal is to determine the average concentrations for the entire screened interval, then a pumped sample or an average from multiple diffusion samplers may be appropriate.

As an aid in the decision-making process, the following section examines the influences that hydraulic and chemical heterogeneity of an aquifer can have on sample quality in long-screened wells. Because VOC concentrations from PDB samplers commonly are compared to VOC concentrations from other sampling methodologies, the second section examines the differences in sample quality between these methodologies in situations of hydraulic and chemical heterogeneity.

Influences of Hydraulic and Chemical Heterogeneity on Sample Quality in Long-Screened Wells

Sampling biases and chemical variability in long-screened wells, which can be loosely defined as wells having significant physical and chemical heterogeneity within the screened interval and in the adjacent aquifer (Reilly and Leblanc, 1998), have been the subject of numerous investigations. Sources of chemical variability in such wells include non-uniform flow into wells (Robbins and Martin-Hayden, 1991; Reilly and Gibs, 1993; Chiang and others, 1995, Church and Granato, 1996; Reilly and LeBlanc, 1998), lithologic heterogeneity (Reilly and others, 1989, Robbins, 1989; Martin-Hayden and others, 1991; Gibs and others, 1993; Reilly and Gibs, 1993), and in-well mixing. In a well open across a chemically or hydraulically heterogeneous section of the aquifer, differences in the sampling methodology can produce significant differences in the sampling results

Long-screened wells have the potential to redistribute chemical constituents in the aquifer where there are vertical hydraulic gradients within the screened interval. Water can move into the well from one horizon and exit the well at a different horizon (Church and Granato, 1996, Reilly and LeBlanc 1998). If there is vertical flow in the screened or open interval, and the zone of low hydraulic head (outflow from

the well) is within the contaminated horizon, then the PDB samplers (or any standard sampling methodology) can underestimate or not detect the contamination. The reason is that, in this case, the contaminated horizon does not contribute water to the well under static conditions. Instead, water from other horizons with higher hydraulic head will invade the contaminated horizon by way of the well screen. Under pumped conditions, the majority of the extracted water will be from the most permeable interval, which may not be the contaminated zone. Even when pumping induces inflow from the contaminated interval, much of that inflow will be a reflection of the residual invaded water from other horizons. In this situation, a substantial amount of purging would be required before water representative of the aquifer could be obtained (Jones and Lerner, 1995). Such sampling is not likely to reflect a significant contribution from the contaminated zone, and concentrations in the contaminated zone probably will be underestimated.

Similarly, if VOC-contaminated water is flowing into the well and is exiting the well at a different horizon, then VOCs will be present along the screened interval between the two horizons. In this case, VOC concentrations in the screened interval may be representative of aquifer concentrations at the inflow horizon, but may not be representative of aquifer concentrations near the outflow horizon

In areas where vertical stratification of VOC concentrations are anticipated, using multiple PDB samplers may more fully characterize the contaminated horizon than using a single PDB sampler. This is particularly true in wells having screens 10 ft or longer; however, significant VOC stratification has been observed over intervals of less than 5 ft (Vroblesky and Peters, 2000). Because of the increased probability of vertical concentration or hydraulic gradients within the open interval of long-screened (greater than 10 ft) wells, it is advisable to determine the zones of inflow and outflow within the screened or open interval of these wells using borehole flowmeter analysis (Hess, 1982; 1984; 1986; 1990, Young and others, 1998).

Comparison of Passive Diffusion Bag Sampling Methodology to Conventional Methodologies

Traditional sampling methodologies, such as the purge-and-sample (or conventional purging method), low-flow or low-volume sampling, and using straddle packers and multilevel samplers, produce VOC

concentrations that may differ from VOC concentrations obtained from PDB samplers because the methodologies sometimes are influenced in different ways by aquifer hydraulic and chemical heterogeneity. This section examines potential sources of concentration differences between traditional methodologies and the PDB methodology.

The purge-and-sample approach to ground-water monitoring differs from the diffusion-sampler approach primarily because the area of the screened or open interval that contributes water to the purged sample typically is greater than for the PDB sampler and the potential for mixing of stratified layers is higher. When pumping three or more casing volumes of water prior to collecting a sample, chemical concentrations in the discharging water typically change as the well is pumped (Keely and Boateng, 1987; Cohen and Rabold, 1988; Martin-Hayden and others, 1991; Robbins and Martin-Hayden, 1991; Reilly and Gibs, 1993; Barcelona and others, 1994; Martin-Hayden, 2000), due to mixing during pumping and other factors, such as the removal of stagnant water in the casing and changing patterns of inflow and outflow under ambient and pumping conditions (Church and Granato, 1996). The induction of lateral chemical heterogeneity during pumping also may produce variations in the sampled concentrations. The amount of mixing during purging can be highly variable (Barber and Davis, 1987; Church and Granato, 1996, Reilly and LeBlanc, 1998; Martin-Hayden, 2000), and may result in concentrations that are not locally representative (Reilly and Gibs, 1993). Substantial vertical hydraulic gradients, even in shallow homogeneous aquifers, have been observed to bias sampling using conventional purging because the majority of the pumped water may come from a particular horizon not related to the contaminated zone and because the intra-well flow that intruded the aquifer may not be adequately removed during purging (Hutchins and Acree, 2000). Thus, differences may be observed between concentrations obtained from a pumped sample and from a PDB sample in a chemically stratified interval if the pumped sample represents an integration of water collected from multiple horizons and the PDB sampler represents water collected from a single horizon

Low-flow purging and sampling (Barcelona and others, 1994; Shanklin and others, 1995) disturbs the local ground water less than conventional purge-and-

sample methods. Thus, samples obtained by PDB samplers are likely to be more similar to samples obtained by using low-flow purging than to those obtained by using conventional purge-and-sample methods. Even under low-flow conditions, however, purging still can integrate water within the radius of pumping influence, potentially resulting in a deviation from VOC concentrations obtained by PDB sampling. One investigation found that in low hydraulic conductivity formations, low-flow sampling methodology caused excessive drawdown, which dewatered the screened interval, increased local ground-water velocities, and caused unwanted colloid and soil transport into the ground-water samples (Sevee and others, 2000). The authors suggest that in such cases, a more appropriate sampling methodology may be to collect a slug or passive sample from the well screen under the assumption that the water in the well screen is in equilibrium with the surrounding aquifer.

Isolating a particular contributing fracture zone with straddle packers in an uncased borehole allows depth-discrete samples to be collected from the target horizon (Hsieh and others, 1993; Kaminsky and Wylie, 1995). Strategically placed straddle packers often can minimize or eliminate the impact of vertical gradients in the sampled interval. However, even within a packed interval isolating inflowing fracture zones, deviations between VOC concentrations in water from PDB samplers and water sampled by conventional methods still may occur if the conventional method mixes chemically stratified water outside the borehole or if the packed interval straddles chemically heterogeneous zones.

The use of multilevel PDB samplers and other types of multilevel samplers (Ronen and others, 1987; Kaplan and others, 1991; Schirmer and others, 1995; Gefell and others, 1999; Jones and others, 1999) potentially can delineate some of the chemical stratification. Diffusion sampling and other sampling methodologies, however, can be influenced by vertical hydraulic gradients within the well screen or the sand pack. When vertical hydraulic gradients are present within the well, water contacting the PDB sampler may not be from a horizon adjacent to the PDB sampler. Rather, the water may represent a mixing of water from other contributing intervals within the borehole. In a screened well, even multilevel samplers with baffles to limit vertical flow in the well cannot prevent influences from

vertical flow in the gravel pack outside the well screen. Such vertical flow can result from small vertical differences in head with depth. A field test conducted by Church and Granato (1996) found that vertical head differences ranging from undetectable to 0.49 ft were sufficient to cause substantial flows (as much as 0.5 liters/minute) in the well bore.

QUALITY CONTROL AND ASSURANCE

The sources of variability and bias introduced during sample collection can affect the interpretation of the results. To reduce data variability caused during sampling, a series of quality-control samples should be utilized.

Replicate samples are important for the quality control of diffusion-sampler data. Sample replicates provide information needed to estimate the precision of concentration values determined from the combined sample-processing and analytical method and to evaluate the consistency of quantifying target VOCs. A replicate sample for water-filled diffusion samplers consists of two separate sets of VOC vials filled from the same diffusion sampler. Each set of VOC vials should be analyzed for comparison. Approximately 10 percent of the samplers should be replicated.

The length of the PDB sampler can be adjusted to accommodate the data-quality objectives for the sampling event. The length can be increased if additional volume is required for collection of replicate and matrix spike/matrix spike duplicate samples.

Trip blanks are used to determine whether exter nal VOCs are contaminating the sample due to bottle handling and/or analytical processes not associated with field processing. Trip blanks are water-filled VOA vials prepared offsite, stored and transported with the other bottles used for collecting the environmental sample, and then submitted for analysis with the environmental sample. Consideration also should be given to the collection of a predeployment PDB trip blank to determine if the PDB samplers are exposed to extraneous VOCs prior to deployment. The predeployment trip blank should be a PDB sampler that is stored and transported with the field PDB samplers from the time of sampler construction to the time of deployment in the wells. An aliquot of the predeployment blank water should be collected from the PDB sampler in a VOA vial and submitted for analysis at the time of sampler deployment.

Water used to construct the diffusion samplers should be analyzed to determine the presence of background VOCs. Although many VOCs accidentally introduced into the diffusion-sampler water probably will reequilibrate with surrounding water once the diffusion samplers are deployed, some VOCs may become trapped within the diffusion-sampler water. For example, acetone, which is a common laboratory contaminant, does not easily move through the polyethylene diffusion samplers (Paul Hare, General Electric Company, oral commun., 1999). Thus, acetone inadvertently introduced into the diffusion-sample water during sampler construction may persist in the samplers, resulting in a false positive for acetone after sampler recovery and analysis

Consideration should be given to the collection of a PDB trip blank to determine if the PDB samplers are exposed to extraneous VOCs prior to deployment. A trip blank is collected from a PDB sampler that is stored and transported with the field PDB samplers between the time of sampler construction and deployment in the well. The water for the trip blank is collected from the PDB sampler in VOA vials at the time of sampler deployment.

SUMMARY

Water-filled passive diffusion bag (PDB) samplers described in this report are suitable for obtaining a variety of VOCs in ground water at monitoring wells. The suggested application for PDB samplers is for long-term monitoring of VOCs in ground-water wells at well-characterized sites. Where the screened interval is greater than 10 ft, the potential for contaminant stratification and/or intra-borchole flow within the screened interval is greater than in screened intervals shorter than 10 ft. It is suggested that the vertical distribution of contaminants be determined in wells having 10-ft-long well screens, and that both the vertical distribution of contaminants and the potential for intraborehole flow be determined in wells having screens longer than 10 ft. A typical PDB sampler consists of a 1- to 2-ft-long low-density polyethylene lay-flat tube closed at both ends and containing deionized water. The sampler is positioned at the target horizon by attachment to a weighted line or fixed pipe.

The amount of time that the samplers should be left in the well prior to recovery depends on the time required by the PDB sampler to equilibrate with ambient water and the time required for environmental disturbances caused by sampler deployment to return to ambient conditions. The rate that water within the PDB sampler equilibrates with ambient water depends on multiple factors, including the type of compound being sampled and the water temperature. Concentrations of benzene, cis-1,2-dichloroethene, tetrachlorethene, trichloroethene, toluene, naphthalene, 1.2dibromoethane, and total xylenes within the PDB samplers equilibrated with the concentrations in an aqueous mixture of those compounds surrounding the samplers under laboratory conditions within approximately 48 hours at 21 °C. A subsequent laboratory study of mixed VOCs at 10 °C showed that tetrachloroethene and trichloroethene were equilibrated by about 52 hours, but other compounds required longer equilabration times. Chloroethane, cis-1,2-dichloroethene, trans-1,2-dichloroethene, and 1,1-dichloroethene were not equilibrated at 52 hours, but appeared to be equilibrated by the next sampling point at 93 hours. Vinyl chloride, 1,1,1-trichloroethane, 1,2-dichloroethane, and 1,1-dichloroethane were not equilibrated at 93 hours but were equilibrated by the next sampling point at 166 hours. Different equilibration times may exist for other compounds. Differences in equilibration times, if any, between single-solute or mixed-VOC solutions have not yet been thoroughly examined.

The samplers should be left in place long enough for the well water, contaminant distribution, and flow dynamics to restabilize following sampler deployment. Laboratory and field data suggest that 2 weeks of equilibration probably is adequate for many applications. Therefore, a minimum equilibration time of 2 weeks is suggested. In less permeable formations, longer equilibration times may be required. When deploying PDB samplers in waters colder than previously tested (10 °C) or for compounds without sufficient corroborating data, a side-by-side comparison with conventional methodology is advisable to justify the field equilibration time.

Following the initial equilibration period, the samplers maintain equilibrium concentrations with the ambient water until recovery. Thus, there is no specified maximum time for sampler recovery after initial equilibration PDB samplers have routinely been left in ground waters having concentrations of greater than 500 ppm of TCE for 3 months at a time with no loss of

bag integrity, and at one site, the PDB samplers were left in place in VOC-contaminated ground water for 1 year with no reported loss of sampler integrity. The effects of long-term (greater than 1 month) PDBsampler deployment on sampler and sample integrity have not yet been thoroughly tested for a broad range of compounds and concentrations. In some environments, development of a biofilm on the polyethylene may be a consequence of long-term deployment. Investigations of semipermeable membrane devices (SPMDs) have shown that the transfer of some compounds across a heavily biofouled polyethylene membrane may be reduced, but not stopped. If a heavy organic coating is observed on a PDB sampler, it is advisable to determine the integrity of the sample by comparing sampler results to a conventional sampling method concentrations before continuing to use PDB samplers for long-term deployment in that well

PDB methodology is suitable for a broad variety of VOCs, including chlorinated aliphatic compounds and petroleum hydrocarbons. The samplers, however, are not suitable for inorganic ions and have a limited applicability for non-VOCs and for some VOCs. For example, although methyl-tert-butyl ether and acetone and most semivolatile compounds are transmitted through the polyethylene bag, laboratory tests have shown that the resulting concentrations were lower than in ambient water. The samplers should not be used to sample for phthalates because of the potential for the LDPE to contribute phthalates to the water sample.

When attempting to determine whether the use of PDB samplers is appropriate at a particular well, a common approach is to do a side-by-side comparison with a conventional sampling method. This approach is strongly suggested in wells having temporal concentration variability. In a well having relatively low temporal concentration variability, comparison of the PDBsampler results to historical concentrations may provide enough information to determine whether the PDB samplers are appropriate for the well. In general, if the two approaches produce concentrations that agree within a range deemed acceptable by the local, state, and Federal regulatory agencies, then use of a PDB sampler in that well will provide VOC concentrations consistent with the historical record. If concentrations from the PDB sampler are higher than concentrations from the conventional method, then it is probable that the concentrations from the PDB sampler are an adequate representation of ambient conditions. If, however, the conventional method produces concentrations

that are substantially higher than the concentrations found by using the PDB sampler, then the PDB sampler may or may not adequately represent local ambient conditions. In this case, the difference may be due to a variety of factors, including mixing or translocation due to hydraulic and chemical heterogeneity of the aquifer within the screened or open interval of the well and the relative permeability of the well screen.

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USGS WRIR 01-4060

Standard Operating Procedure for Soil Headspace Field Screening Using an OVA/FID at Dunn Field

TO:

U.S. Army Engineering and Support Center, Huntsville

COPIES

Memphis Depot Caretaker (MDC)

U.S. Environmental Protection Agency (USEPA), Region 4

Tennessee Department of Environment and Conservation (TDEC)

FROM.

CH2M HILL

DATE:

May 5, 2000

This memorandum describes the use of the Organic Volatile Analyzer (OVA)/ Flame Ionization Detector (FID) headspace method for performing field soil screening.

Collecting Soil Samples

- 1 Calibrate the FID per the manufacture's procedures.
- 2. Place latex gloves on hands for protection and to reduce cross-contamination.
- 3. Open the 5 foot core sampler and extract the two 2.5-foot clear liners and cap each end of the liner. Label the top and bottom of each liner with the associated depths and boring ID.
- 4 Visually and physically characterize the soil core by collecting small samples from each end of the liner remembering to only remove the end caps briefly. Determine if any abrupt changes in soil lithology exists (i.e. sand to clay, gravelly sand to sandy clay).
- 5 If no change in soil lithology exists, the headspace sample should be collected (skip to #11) where the two liners connect (center point of the 5-foot interval).
 - If one or more lithological changes occur, then proceed to #6
- 6 Mark the outside of the liner with a permanent pen were the change occurs.
- 7. Label the sample bags with the appropriate sample ID.
- 8 Cut the liner approximately 4 inches above the marked soil change and separate the two sections of the liner. (The area of concern is the higher permeability soil immediately above the lower permeability layer.)
- 9 Immediately place a cap on the cut end of liner section containing the area of concern and the soil change. (This section of the liner could be sampled later for laboratory analysis.)
- 10. Use the end of the other section that was cut to collect soil for headspace readings.
- 11. Quickly fill 2 quart sized sealable plastic bags at least 1/2 full with soil using a stainless steel sampling spoon.

- 12. <u>Immediately</u> seal the bags.
- 13. * For liners that contain soil lithology changes* Label the liner that contains the area of concern with the appropriate ID.
- 14. Repeat steps #6 through #11 for each lithological change. For areas where multiple low permeability layers are concentrated, only the soil above the upper layer will be considered important.
- 15 Place the liners out of the sun and protected from the environment.
- 16. Allow the soil in the bags to reach room temperature or warmer [20°C (68°F) to 32°C (90°F)].
- 17. While the FID organic vapor analyzer is running, insert the OVA/FID probe through the side of the first bag after the temperature has equilibrated (typically after 5 minutes).
- 18. Record the highest reading on the gauge; this is the <u>unfiltered concentration</u>. If the unfiltered measurement is non-detect, do not proceed to line 9. Record the reading in the logbook as the total hydrocarbon measurement for that sample.
- 19. Attach an activated charcoal filter onto the OVA/FID
- 20. While the FID organic vapor analyzer is running, insert the OVA/FID probe with the attached charcoal filter through the side of the second bag.
- 21. Record the highest reading on the gauge; this is the filtered concentration.
- 22. Subtract the filtered reading from the unfiltered reading for the <u>total corrected hydrocarbon</u> measurement.

Attachment II. Standard Operating Procedure for Collecting Soil Samples for Volatile Organic Compounds (VOCs)

TO

U.S. Army Engineering and Support Center, Huntsville

COPIES:

Memphis Depot Caretaker (MDC)

U.S. Environmental Protection Agency (EPA), Region 4

Tennessee Department of Environment and Conservation (TDEC)

FROM.

CH2M HILL

DATE:

August 16, 2001

Standard Operating Procedure

This memorandum describes the use of pre-weighed VOC vials for collection of discrete sample aliquot to be analyzed for VOCs using EPA SW-846 Method 5035. Importantly, using this method, two vials must be prepared for each sample submitted

Collecting Soil Samples

- 1. Place nitrile gloves on hands for protection and to prevent cross-contamination.
- 2 Open the package containing the pre-cut syringe sample-collection device.
- 3. Open the vial that will be receiving the soil.
- 4 Retract the plunger of the cut-off syringe to between 5 or 6; mark on the syringe tube.
- 5. Insert the syringe into the soil.
- 6. Remove the syringe and the "slug" of soil into a pre-weighed vial. Replace the cap on the vial
- 7. Label the vial with the sample ID and date sampled.
- 8 Repeat the steps above for the second sample vial.
- Make sure that the preservative in the vial mixes with the slug of soil by shaking, if necessary.
- 10. Place vials into cooler with wet ice for shipment.

Standard Operating Procedure for Collecting Soil Samples for Volatile Organic Compounds

TO:

U.S Army Engineering and Support Center, Huntsville

COPIES.

Memphis Depot Caretaker (MDC)

US Environmental Protection Agency (USEPA), Region 4

Tennessee Department of Environment and Conservation (TDEC)

FROM:

CH2M HILL

DATE

May 5, 2000

Standard Operating Procedure

This memorandum describes the use of an EnCore sampler to collect a discrete sample aliquot to be analyzed for volatile organic compounds (VOCs). The confirmation samples will be analyzed for TCL volatile organics by SW-846 Method 8260B.

Collecting Soil Samples

- 1. Place latex gloves on hands for protection and to reduce cross-contamination.
- Open the EnCore reusable package and remove the core device and cap.
- 3. Twist the piston on the EnCore sampler, so that the piston is unlocked and can move freely.
- 4 Place the core device into the T-handle.
- 5. Open the soil-core sampler (e.g., split spoon) containing the soil core
- Using a stainless steel spoon, scrape off the initial soil touching the soil-core sampler.
- 7. Push the EnCore core device into the soil core
- 8. Twist the T-handle, and pull the encore sample free of the soil. The sampler should now be full of soil. If not, repeat this step until the encore is full of soil.
- Remove excess soil from the sides of the sampler, and place the cap onto the sampler. (Make sure both sides of the cap lock into place)
- 10. Twist the piston 90 degrees, so that it is locked
- 11. Label and reseal in the original package
- 12. Place into cooler with wet ice for shipment.

Standard Operating Procedure for QED® Bladder Pumps

PREPARED FOR:

Steve Offner/ATL

PREPARED BY:

Johannah Rogers

DATE:

March 10, 2000

Advantages for using bladder pumps from the MicroPurge® Website on Well Wizard® Bladder Pumps.

- 1. Low-flow groundwater monitoring system with rates as low as 100 mL/minute or less, does not increase turbidity, and does not alter samples.
- 2. EPA accepted for low-flow sampling.
- 3 Pneumatic bladder pumps operate with a timed on/off cycle of compressed air alternately squeezing the flexible bladder to displace water out of the pump and release it to allow the pump to refill by submergence.
- 4 The bladder prevents contact between the pump drive air and the sample.

Standard Operating Procedure

This memorandum describes techniques used for low-flow purging and intrinsic sampling of groundwater monitoring wells. Low-flow purging techniques are used to reduce purge volumes and sampling time. It also allows for the collection of more representative field parameters (for example, dissolved oxygen and redox potential).

Low-flow purging techniques have the following advantages

- Avoids lowering the water table and sampling static water in well (pulls in formation water),
- reduces sample aeration, and
- reduces groundwater turbidity (important in the collection of total metals samples).

Purging Procedure

- Measure depth to groundwater
- Measure total depth of well
- Calculate purge volume.
- Place pump intake approximately in the center of the screen interval that is submerged
 for wells screened across the water table. In fully submerged wells, place pump intake

1

approximately 1 foot below the top of screen. Rather than lowering the pump to the bottom of the well and pulling it up to the desired level, the pump should be slowly and carefully lowered to the target screen zone (measure pump tubing as it is lowered). This will prevent siltation of the groundwater.

- 5. Start the air compressor engine. If a gasoline powered compressor is used, place as far from the well as possible, in the down wind direction
- 6. Connect the appropriate hoses for the air supply
- 7. Set the length of the on/off cycle for pressurizing and venting. This will control the length of time that the pump discharges and refills the bladder. The length of the cycle is dependent on the rate of recharge of the well. It should be adjusted to prevent drawdown of the well. Consult the pump manual for recommendations on cycle times
- 8 Increase the pressure on the air compressor
- 9. Install a water level indicator above the pump to monitor drawdown during purging.
- 10. Purge wells slowly, at a rate that does not lower that water table significantly (less than 10% of the screen length). Well Wizard® Bladder Pumps can be run at rates less than 100mL/minute or less. The purging rate should be carefully controlled and can be measured using a graduated bucket. A minimum of three well volumes should be purged prior to sampling.
- 11 Consult the pump manual for detailed instructions and recommendations.

Stabilization Criteria

- 1 Measure field parameters (pH, conductivity, dissolved oxygen (DO), oxidation-reduction potential (redox), turbidity [visual or turbidimeter], and temperature) using a calibrated YSI 600XL (or equivalent) and a flow cell. Record parameters every quarter well volume. The depth to groundwater should also be recorded on the purging form to monitor the water table drawdown.
- 2. Purge monitoring wells until field parameters have stabilized to within the ranges presented below. Purging with the QED® Well Wizard® Bladder Pump should produce representative formation water without increasing turbidity or altering the parameters.
- 3 Typically, dissolved oxygen will be elevated at the start of purging (for example, 7 mg/L), and should decrease as pumping proceeds. Contaminated wells typically have a low DO (less than 1 mg/L) and a negative redox. If the DO begins to rise during purging, it is an indication that artificial aeration is occurring and the pumping rate should be reduced.
- 4 If the water table begins to drop more than 1 foot, adjust the length of the on/off cycle. If a well is purged dry, purging will be considered complete. A replacement well should be selected for intrinsic sampling adjacent to the original well in the same zone of contamination (clean upgradient, in contaminated plume, or downgradient).
- 5. Position the pump lower (approximately 2 to 3 feet) in wells that have historically low recharge rates. Slowing the pumping rate down to match the recharge rate may help avoid pumping a well dry.

Field Parameter/General Order of Stabilization:	Stabilization Criteria:		
1. pH	± 0.1		
2 Temperature	± 10%		
3 Conductivity	± 3%		
4 Redox potential	± 10 mV		
5. DO and turbidity	± 10%		

Sample Collection

- 1 Collect groundwater samples following stabilization directly out of the pump discharge.
- 2 Sample collection order is based on the approximate order of susceptibility to artificial aeration and should be consistent between all wells sampled: volatile organics (benzene, toluene, ethylbenzene, and xylenes [BTEX] and trimethyl benzene [TMB]), carbon dioxide [CO₂], total organic carbon (TOC), methane [CH₄], sulfide [SO₃], alkalinity, sulfate [SO₄], nitrate [NO₃], extractable lead [Pb], and ferrous iron (filtered). Note that nitrate has a 48 hour holding time.
- 3. Use an in-line filter to field filter dissolved metals (ferrous iron). If total metals (extractable lead) samples are turbid (silty), delay sample collection for approximately 3 to 4 hours, at which time a bailer can carefully be lowered into the uppermost portion of the water column (in wells screened across the water table) to collect the sample.

TECHNICAL MEMORANDUM

Standard Operating Procedure for Sudan IV Dye Testing

TO.

U.S. Army Engineering and Support Center, Huntsville

COPIES.

Memphis Depot Caretaker (MDC)

U.S. Environmental Protection Agency (USEPA), Region 4

Tennessee Department of Environment and Conservation (TDEC)

FROM

CH2M HILL

DATE

May 5, 2000

Standard Operating Procedure

This memorandum describes the use of Sudan IV dye as a preliminary screening technique used for detecting the presence of DNAPL in groundwater and soil samples. Sudan IV is a hydrophobic dye which turns bright red in the presence of DNAPL.

Testing Soil Samples

- 1. Collect soil samples from the soil core extracted by the sampler.
- 2. Place an aliquot of soil from the area(s) exhibiting the highest PID reading(s) into a 4 ounce glass or plastic jar or other appropriate receptacle
- Fill approximately one-half of the container with the sampled soil.
- 4. Manually disperse the soil in the jar to minimize clumping.
- 5. Fill the remaining volume of the container with distilled water
- 6. Add a very small amount (2 to 4 milligrams an amount that would rest on the edge of a toothpick) of Sudan IV dye (in powder form) to the container using extra care not to expose the dye to any parts of the body. [Sudan IV is an irritant and possible mutagen with which skin or eye contact should be avoided. Gloves should always be worn when handling the Sudan IV dye.]
- After the dye has been added, seal the container and shake the soil/distilled water/dye
 mixture for approximately 30 seconds.
- 8. Note the presence or absence of bright red staining indicative of DNAPL in the logbook <u>Is there a presence of bright red staining?</u> If yes, this indicates the presence of DNAPL in the sample.

Testing Groundwater Samples

- DO NOT purge monitoring well prior to sample collection.
- 2. Collect groundwater samples from the bottom of each monitoring well using a bottom filling, 3 foot disposable Teflon bailer.

705 398

- 3. Pour an aliquot of the liquid from the bottom of the bailer into a 4 ounce glass jar or other appropriate receptacle.
- 4. Add a very small amount (2 to 4 milligrams an amount that would rest on the edge of a toothpick) of Sudan IV dye (in powder form) to the container using extra care not to expose the dye to any parts of the body. [Sudan IV is an irritant and possible mutagen with which skin or eye contact should be avoided Gloves should always be worn when handling the Sudan IV dye.]
- 5. After the dye has been added, seal the container and shake the groundwater/dye mixture for approximately 30 seconds.
- 6. Note the presence or absence of bright red staining indicative of DNAPL in the logbook. <u>Is</u> there a presence of bright red staining? If yes, this indicates the presence of DNAPL in the sample.

Generic
Quality Assurance
Project Plan

for

Defense Distribution Depot Memphis

Prepared for

Huntsville Division Corps of Engineers Huntsville, Alabama

Prepared by

2567 Fairlane Drive Montgomery, Alabama 36116

110479.QP

Executive Summary

Introduction

In October 1992, the Defense Depot Memphis, Tennessee (DDMT), was placed on the National Priorities List (NPL) by the U.S. Environmental Protection Agency (EPA). Therefore, DDMT must fulfill requirements under the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA) and National Contingency Plan. A remedial investigation/feasibility study (RI/FS) must be prepared to determine the nature and extent of contamination, to evaluate the risk to human health and the environment, and to screen potential cleanup actions. The Generic RI/FS Work Plan was prepared to show how the investigation and study would be accomplished. This Quality Assurance Project Plan (QAPP) was prepared as a supplement to the Generic RI/FS Work Plan to describe the general sampling, laboratory, monitoring well installation, soil boring installation, and quality assurance/quality control (QA/QC) procedures that will be used during the RI/FS at DDMT.

Site Background and Location

DDMT covers 642 acres of land in Memphis, Shelby County, Tennessee, in the extreme southwestern portion of the state. The installation contains approximately 110 buildings, 26 miles of railroad track, and 28 miles of paved streets. Approximately 5.5 million square feet of storage space is open. Stored items include food, clothing, electronic equipment, petroleum products, construction materials, and industrial, medical, and general supplies.

Description of Operable Units (OUs)

DDMT is divided into four OUs for evaluation purposes. Dunn Field is designated OU-1. The Main Installation is divided into three areas: the southwestern quadrant, OU-2; the southeastern lakes and golf course area, OU-3; and the north-central area, OU-4. Substances found in OU-1 probably resulted from use of the area for landfill operations, mineral stockpiles, pistol range use, and pesticides storage. Potential contamination of OU-2 could have resulted from spills or releases from the hazardous material storage and repouring area, sandblasting and painting activities, or both. Storage of polychlorinated biphenyls (PCBs) and the use of pesticides and herbicides are potential sources of contamination for OU-3. Principal contamination in OU-4 probably resulted from a wood treatment operation and hazardous material storage.

Description of QAPP

This QAPP was prepared as a supplement to the Generic RI/FS Work Plan to provide quality assurance and quality control requirements for sampling activities, and other types of field analyses and tests that generate data as part of the activities performed during the RI/FS process at DDMT. The goal of this plan is to provide data of known quality to the project team to support the project decision-making process. The requirements of this plan apply to the primary contractor, as well as to subcontractors.

This plan addresses the following:

- QA/QC objectives for the project
- Discussion of the QC levels and applicability of each
- Specific QA/QC procedures that will be implemented to achieve these objectives
- Project team organization and responsibility

The contractor's internal QA programs will control other project aspects, such as engineering analysis and report preparation. Laboratory activities (either onsite or fixed-base analytical laboratories) will be covered by the Laboratory Comprehensive Quality Assurance Manual.

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Acronyms

ASTM American Society for Testing and Materials

bgs Below ground surface BRA Baseline risk assessment

CEHND Corps of Engineers, Huntsville Division
CEMRD Corps of Engineers Missouri River Division

CEWES Corps of Engineers Waterways Experiment Station

CFR Code of Federal Regulations
CLP Contract Laboratory Program

COC Chain-of-Custody
COE Corps of Engineers

CompQAM Comprehensive Quality Assurance Manual

CPR Cardiopulmonary resuscitation
CSL Close support laboratory
DDIS Detailed Data Inventory Sheet
DDMT Defense Depot Memphis, Tennessee

DE Disposable equipment

DOT Department of Transportation

DQE Data quality evaluation
DOO Data quality objective

DRMO Defense Reutilization and Marketing Office

E-Data Electronic data

EMIS Environmental Management Information System

EPA U.S. Environmental Protection Agency

FID Flame ionizing detection
FSP Field Sampling Plan
FTL Field team leader
GC Gas chromatograph

GC/MS Gas chromatograph/mass spectrometer

HSA Hollow stem auger
HASP Health and Safety Plan
HW Hazardous waste

ID Inside diameter

IFF Interchange File Format

MLGW Memphis Light, Gas, and Water

MR Mud rotary

MS/MSD Matrix spike/matrix spike duplicate

MW Monitoring well

NCP National Contingency Plan

NIST National Institute of Standards and Technology

NRC Nuclear Regulatory Commission
NSF National Sanitation Foundation

OSHA Occupational Safety and Health Administration

OU Operable unit

Acronyms (cont'd)

OVA/PID Organic vapor analyzer/photoionization detector

PAH Polycyclic aromatic hydrocarbon

PARCC Precision, accuracy, representativeness, completeness, and comparability

PCB Polychlorinated biphenyl PCP Pentachlorophenol

PM Project Manager

PPE Personal protective equipment

ppm Parts per million

psi Pounds per square inch
PVC Polyvinyl chloride

QA/QC Quality assurance/quality control QAPP Quality Assurance Project Plan

RCRA Resource Conservation and Recovery Act

RD Rotasonic drilling

RFA RCRA Facility Assessment

RI/FS Remedial investigation/feasibility study

RPD Relative percent difference

RTL Review team leader SDG Sample delivery group

SOP Standard operating procedure

SOW Statement of Work
SSC Site safety coordinator
STB Stratigraphic test boring
STP Sample Tracking Program
SVOC Semivolatile organic compound

TAI. Target analyte list

TCDD 2,3,7,8-Tetrachlorodibenzo-p-dioxin

TCL Target compound list

TCLP Toxicity characteristic leaching procedure

TDEC Tennessee Department of Environment and Conservation

TIC Tentatively identified compounds

VOC Volatile organic compound

WR Water rotary

1.0 Objectives of the Quality Assurance Project Plan

The purpose of this Defense Depot Memphis, Tennessee (DDMT) Generic Quality Assurance Project Plan (QAPP) is to describe the general sampling, laboratory, monitoring well installation, soil boring installation, and quality assurance/quality control (QA/QC) procedures that will be used during the Remedial Investigation/Feasibility Study (RI/FS) at DDMT. The procedures have been developed for the chemical data collection activities to provide data of sufficient quality and quantity to support the objectives of the RI/FS, and to provide careful planning of data collection and analysis activities to meet the stated data quality objectives that are consistent with the intended data uses.

The QAPP has been written in accordance with the current RI/FS guidance (ref. 21), the Data Quality Objectives for Remedial Response Activities (ref. 26), the Guidelines and Specifications for Preparing Quality Assurance Plans (ref. 27), and EPA Region IV, Environmental Compliance Branch Standard Operating Procedures and Quality Assurance Manual (ECBSOPQAM) (ref. 31) to address aspects of the field investigations to be conducted as a part of the site characterization activities that are common to all operable units (OUs) at DDMT. References used for QAPP development are provided as Appendix A.

1.1 Project Objectives

The overall objectives of the RI/FS are to determine the nature and extent of the release of hazardous substances to the underlying aquifer system as a result of past disposal activities at DDMT, to identify the sources of release, and to evaluate the effectiveness of proposed remedies. The ultimate goal is to select cost-effective and implementable remedies that mitigate threats and provide protection for public health and the environment. During the RI, the data and data collection processes will be evaluated to monitor the support of the RI/FS objectives. That is, the data must be of sufficient quality and quantity that the distribution and migration of contaminants can be determined to satisfy the objectives of the RI. The data and conclusions drawn during the RI must support the screening and in-depth analyses of the remedial alternatives to be evaluated during the FS. To accomplish these tasks, confidence in field sampling procedures; data collection, analysis, management, and validation procedures; and QA activities are vitally important. Because these items are so important to the remedial decision-making process, a carefully considered approach to detailed QA procedures is necessary for success.

To characterize the sites and potential releases, DDMT will implement an extensive field sampling effort to identify and delineate the contaminants (in the groundwater, soil, surface water, and sediments) that may have resulted from past practices at sites where hazardous or toxic wastes were managed or disposed. A laboratory that has been validated by the Corps of Engineers' Missouri River Division (CEMRD) and that is a

Program (CLP) will be selected to perform the required chemical analyses. Split samples will be routinely provided to the CEMRD to comply with Corps of Engineers (COE) quality-control requirements and to the EPA- and Tennessee Department of Environment and Conservation (TDEC)-designated laboratories to meet EPA's requirements.

1.2 Objectives of Site Investigation Activities

The primary objective of this RI is to characterize the nature and extent of contaminants in soil, surface water, sediment, and groundwater. Additional data will be collected to supplement the previous RI/FS completed in 1990 by Law Environmental Inc., to evaluate the extent of groundwater contamination in the Fluvial Aquifer and to assess the potential for contaminant migration to the Memphis Sands Aquifer. This investigation will provide additional information for the baseline risk assessment (BRA) and the selection of appropriate remedial alternatives. Other general objectives of the RI include the following:

- Understand site geology and hydrogeology sufficiently to evaluate groundwater movement and to identify potentially affected aquifers.
- Collect a sufficient number of samples from areas surrounding the site unaffected by earlier activities to adequately evaluate background concentrations of target analytes.
- Collect samples that are representative of actual site conditions.
- Provide data of known quality by using approved sampling and analytical methods.

Specific site investigation details, along with sampling and analysis objectives, are discussed in the Field Sampling Plans (FSPs) for the OU in which the site is located.

1.3 Site Characterization Activities

Field investigations will be conducted under the guidance of this QAPP, the Health and Safety Plan (HASP), and the OU-specific FSPs, as well as any addendum that may be required for these plans. Proposed sample locations are identified in the FSPs and in site maps prepared for the particular OU to be investigated. Data management, field

sampling, and field and laboratory QA/QC activities will be conducted in accordance with the procedures outlined in the QAPP. The following field activities will be conducted:

- Install monitoring wells and soil borings.
- Collect and analyze soil, groundwater, surface water, sediment samples, and the appropriate QA/QC samples.

2.0 Project Organization and Responsibilities

2.1 Project Team Organization

The project team will be organized into contractor, COE, and offsite laboratory work groups. The contractor's group will consist of a project manager, a project hydrogeologist, a project environmental engineer, a project chemist, a review team leader, a database manager, and various support staff. The COE's group will consist of a project manager, a project engineer, a project geologist, a project industrial hygienist, a project environmental engineer, and a project chemist, who will develop work plans and scopes of work, oversee field performance, and review technical documents. The contractor group at the field site will consist of the field team leader (FTL), who will be onsite for all phases of the project; the field geologists; the safety officer and sampling team; and various support technicians. The laboratory work groups include the technical staff and QA/QC personnel at the laboratories. Additional project organization information will be provided upon selection of a contractor.

2.2 Key Personnel Qualifications and Responsibilities

2.2.1 Contractor Work Group

The personnel selected for the RI/FS will have the necessary qualifications to complete this complex project. Additional information will be provided later concerning specific qualifications

In full compliance with the training requirements of Occupational Safety and Health Administration (OSHA) regulations (29 Code of Federal Regulations [CFR] 1910.120), all field personnel have received at least 40 hours of health and safety training, including first aid and cardiopulmonary resuscitation (CPR), and a minimum of 3 days actual field experience under the direct supervision of a trained experienced supervisor. The personnel positions and responsibilities listed below will be involved in the RI/FS.

Program Manager—The program manager is a senior level management person who coordinates all the project efforts for DDMT. As the direct contact between the COE and other program and project staff, the program manager will be responsible for negotiating and communicating contractual obligations, including program objectives, technical requirements, schedules, budgets, and deliverables. The program manager will coordinate all administrative and financial reporting, provide the COE with progress and financial reports, review all deliverables, and provide day-to-day coordinating with the COE.

Project manager (PM)—Responsible for overall activities for a specific project. The PM is responsible for cost and schedule control and for technical quality; in addition, he

or she will develop the work plan and monitor task order activities to ensure compliance with project objectives and scope. The PM also will communicate with the client and, as appropriate, other designated parties regarding project progress.

The PM has ultimate responsibility within CH2M HILL for producing deliverables that are technically adequate, satisfactory to the client, and cost-effective. To accomplish this, the PM assists the review team leader (RTL) in developing an internal project review schedule, provides written instructions and frequent guidance to the project team, and monitors budgets and schedules.

Review Team Leader—The RTL is generally a technical resource with experience in the various technical aspects involved in a complex project. The RTL coordinates internal QA/QC review for technical validity and adherence to both internal CH2M HILL policy and project-specific criteria. The RTL assists the PM in selecting an internal QA/QC review team and in coordinating review efforts, and works with the project team in addressing review comments and adjudicating technical disagreements.

Lead Hydrogeologist—This person is a technical specialist who is responsible for the technical aspects of the project concerning hydrogeology and who provides technical review and continuity of work between project tasks. His/her role includes selection of methodology, field procedures, and review of data analysis and reporting. He/she will be present at major meetings on decision points. The lead hydrogeologist will work closely with the lead engineer to develop and implement a field program that addresses the project objectives and provides technically sound data.

Lead Chemist—The lead chemist assists with the preparation of the project scoping documents, provides an interface between the laboratory and the project team, supervises the analytical data quality evaluation, and participates in preparing deliverables to the client. The lead chemist communicates regularly with the project team and the analytical laboratory during the field activities. The lead chemist also is responsible for monitoring project-specific laboratory activities (including checking laboratory invoices and reports) and may audit the laboratory at the PM's direction.

The lead chemist monitors so that specific QA and primary technical operations are coordinated effectively for the project. The lead chemist is responsible for the following:

- Performance and system audits of laboratory operations to evaluate compliance with the QAPP
- System audits of field operations to evaluate compliance with the QAPP
- Provision of guidance and coordination to rapidly resolve any QA/QC problems

- Independent review of QA/QC information to evaluate the quality of all deliverables or outputs from the project team
- Interaction and communication with COE QA personnel to resolve QA/QC problems specific to the project

Lead Risk Assessor—The lead risk assessor provides guidance and input into the RI/FS planning implementation stages, and directs the human health and ecological risk assessments for the project.

Remedial Design Engineer—The remedial design engineer will evaluate the data collected from the RI and direct sampling to be conducted for the FS activities. The remedial design engineer also will conduct a cost-benefit analyses and other FS activities to aid in evaluating remedial alternatives for the contaminated sites at the facility.

Lead Data Manager—Responsible for the structure, organization, format, implementation, and operation of the project database. The lead data manager supervises the data management team and provides direction to the database manager. The lead data manager, in conjunction with the PM, may decide to establish separate databases for each project task. The lead data manager is responsible for the following:

- Coordinating efforts between the project team and the database, including setting up the sample tracking program and providing instruction to field team members in its operation.
- Importing the analytical data into the project database.
- Doing a QC review of the data input into the database.
- Assisting project team members in using the database.
- Preparing the electronic deliverables to the client.

Database Manager—Works with the database on a daily basis and provides normal deliverables (for example, data summary tables) to the project team.

Field Team Leader (FTL)—Reports to the PM and will be responsible for the coordination of field efforts, provides for the availability and maintenance of sampling equipment and materials, and provides shipping and packing materials. The FTL will supervise completion of all chain-of-custody records, supervise the proper handling and shipping of samples, and be responsible for accurate completion of the field notebook. As the lead field representative, the FTL will be responsible for consistently implementing program QA/QC measures at the site and for performing field activities in accordance with approved work plans, policies, and field procedures.

Site Safety Coordinator (SSC)—The SSC oversees the administration of the project HASPs in the field. The SSC will assist in conducting site briefings and perform all final

safety checks. The SSC is responsible for stopping any investigation-related operation that threatens the health and safety of the field team or surrounding populace. Additional responsibilities are detailed in the HASP.

2.2.2 Laboratory Work Group

The selected laboratories will be responsible for screening and analysis of groundwater, soil, sediment, and surface water samples obtained during RI activities.

The chemical analysis supervisor serves as a liaison between field and laboratory operations and is responsible for the following:

- Receipt of sample custody from the field team members, verification of sample integrity, and transfer of sample fractions to the appropriate analytical departments
- Coordination of sample analyses to meet project objectives
- Preparation of analytical reports
- Review of laboratory data for compliance with method requirements
- Review of any QC deficiencies reported by the analytical department manager
- Coordination of any data changes resulting from review by the project QA supervisor or the PM
- Response to questions from the project team during the data quality evaluation process

2.3 Project Communication

One of the most critical elements in performing the RI/FS is to establish and maintain lines of communication among all project personnel. Some work groups will meet at least weekly to review the status of the project and to discuss technical and safety issues. When necessary, other meetings will be scheduled or the FTL will meet individually with field personnel or the subcontractors to resolve problems. The FTL will prepare a weekly report detailing project progress.

The FTL will be in regular telephone contact with the all work groups. When significant problems or decisions requiring additional authority occur, the FTL can immediately contact the PM or project hydrogeologist for assistance.

Daily and weekly reports, boring logs, QA reports, and other project information will be delivered by the field supervisor or other personnel on a daily basis or several times during the week.

All communications with DDMT will be channeled through the DDMT project manager, who will be informed of field activities being conducted on a daily basis.

All communications with the COE will be channeled through the Corps of Engineers, Huntsville Division (CEHND) project manager. The contractor will prepare monthly progress reports and submit telephone conversation records to the COE throughout the contract period.

3.0 Data Quality and Quality Assurance Objectives for Sampling

3.1 Introduction

This section presents the data quality objectives (DQOs) and QA objectives for the RI/FS sampling activities. DQOs are quantitative and qualitative statements that specify the quality of the data required to support decisions during the remedial response activities. They are based on the end uses of the data to be collected. The basis on which these objectives were established are discussed in the following sections. The criteria for evaluating data quality, precision, accuracy, representativeness, comparability, and completeness are presented in this section, along with the mechanisms that will be used to determine if they are met.

3.2 Establishing Data Quality Objectives

Objectives for data quality reflect the expected uses of the data, the expected levels of contamination, and the available analytical and sampling resources.

3.2.1 Data Uses

The primary uses of the data to be gathered during the DDMT RI sampling activities are as follows:

- Contaminant Characterization—Data will be used to describe the nature and extent of contaminants in the soil and groundwater at the site.
- Health and Safety—Air monitoring within the RI/FS work zones will be used to establish the level of protection needed for workers during the RI activities.
- Risk Assessment—Data will be used to evaluate the threat posed by the site to public health and the environment via the soil, groundwater, surface water, and air pathways.
- Evaluation of Alternatives Soil chemistry and physical data will be collected and used to evaluate the feasibility of various remedial technologies.
- Engineering Design of Alternatives—Data such as preliminary volume estimates for contaminated soil and groundwater will be used for engineering design purposes and to determine the cost and performance of various remedial technologies.

3.2.2 Data Quality Levels

Data must be of sufficient quality to support the decision-making process. A tiered approach to sampling and analysis (including screening) will be used so that the field team can adjust the sampling effort to accommodate site-specific conditions. The tiered approach will be accomplished by screening a large number of samples for potential contamination using Level 2 data quality; then a selected number of samples will be submitted to an analytical laboratory for confirmation. Screening data will be used to provide sufficient sampling to evaluate the potential presence of target compounds at each site and to accomplish quantitation.

Four categories of data will be collected as part of this field effort, with each category having a different level of supporting QA/QC documentation. The four categories, or levels, correspond to QC levels 1, 2, 3, and 4. Level 1 includes field monitoring activities such as pH, temperature, conductivity, and total organic vapor monitoring. Level 2 screening activities and Level 3 analysis provide confirmation by an analytical laboratory. Level 4 analysis provides legally defensible data, if needed. For each QC level, the potential measures and methods to be used, as well as the applicable data package deliverables, are outlined below. For each site, the use and applicability for each of the available measures and methods will be evaluated and appropriate measures and methods selected. For example, the pH and conductivity of groundwater samples from all the screening sites will be measured; however, only soil samples from selected sites will be tested for VOCs.

3.2.2.1 Level 1-Field Surveys

Level 1 encompasses field monitoring activities and does not require formal data package deliverables. Level 1 activities are focused on easily measured bulk characteristics of a sample such as total organic vapors, or pH, temperature, and conductivity. Level 1 activities also include screening samples using immunoassay field methods for classes of compounds such as polycyclic aromatic hydrocarbons (PAHs) or polychlorinated biphenyl (PCBs) in soils.

CH2M HILL typically uses the data generated from field monitoring to make decisions about the execution of the investigation, such as approximating the relative degree and extent of contamination to assist the investigation activities, or providing a general sample screening before analysis by the analytical laboratory.

Immunoassay screening provides a yes/no approach to screening: either the target compound(s) is present at, or above, the reporting limit or it is not. These tests will be used to identify potential sources of contamination and may be used to estimate approximate areas for vertical and horizontal extent of contamination. Immunoassay screening kits use an antibody that is developed to have a high degree of sensitivity to the target compounds. This antibody's high specificity is coupled with a sensitive

colorimeteric reaction that provides a visual result. Immunoassay screening tests consist of four steps:

- Sample Extraction—An aliquot of soil is weighed and extracted with methanol.
- Dilution of Sample and Standard—The sample extract is diluted to the required detection level.
- Immunoassay—The sample and enzyme conjugate are introduced into antibody tubes and allowed to stand; then the tubes are washed, coloring agent is added, and the color is allowed to develop
- Measurement and Interpretation—The color of the sample is measured
 using the spectrophotometer and the sample results are compared to the
 standard results. This comparison provides an accurate semi-quantitative
 measurement of the specific contaminant of interest.

Immunoassay kits that will be used in the field for Level 1 screening include PCBs, PAHs, total petroleum fuel contamination, pentachlorophenol (PCP), and dioxins (2,3,7,8-Tetrachlorodibenzo-p-dioxin [TCDD]). Each of the immunoassay kits is described briefly below:

• PCBs—Recognizes all commercial Aroclors; the more highly chlorinated and most common (1260, 1254, and 1248) are detected at lower concentrations, as summarized in Table 3-1.

Detection Limits	le 3-1 for Aroclors in Soil emphis, Tennessee
Aroclor	mg/kg in soil
1260	0.4
1254	0.4
1248	1.0
1242	2.0
1232	4.0
1016	4.0

• Total Petroleum Fuel Contamination—This immunoassay responds to a selected subset of the chemical components in fuels, primarily aromatic and aliphatic compounds with fewer than 15 carbons. Because this test

responds to "petroleum products," it cannot be used to distinguish individual types or sources of fuel. Reporting limits for various fuels using this screening test are summarized in Table 3-2.

Table 3-2 Reporting Limits for Various Fuels Using the Total Petroleum Fuel Contamination Screening Test Defense Depot Memphis, Tennessee		
Fuel	Reporting limit in mg/kg	
Gasoline	10	
Diesel fuel, #2	15	
Jet A fuel	15	
Jet fucl, JP-4	15	
Kerosene	15	
Fuel oil, #2	15	

- PAHs—This test is used to screen for 3- and 4-ring PAHs, which are indicative of petroleum contamination. The overall detection limit is 1 mg/kg.
- PCP-This test recognizes pentachlorophenol only and has a reporting limit of 0.5 mg/kg.
- Dioxin—This test is used to detect the presence of 2,3,7,8-TCDD only and has a reporting limit of 10 picograms/kg. The extraction for this screening test is more complex than the simple methanol extraction used for the other analyses; therefore, samples for dioxin screening will be sent to the analytical laboratory for extraction and screening.

Monitoring results, as well as pertinent data concerning the sampling event, are documented in a bound field book. Level 1 documentation will consist of the following:

- Instrument identification
- Calibration information (standards used and results)
- Date and time of calibration and sample measurement
- Sample results

The logbooks will be reviewed by the FTL daily for completeness and correctness. No additional documentation or data quality evaluation is required.

3.2.2.2 Level 2-Screening Data

Level 2 screening data will be used by the project team to make informed decisions in the field concerning implementation and execution of the work plan, as well as to evaluate whether a release has occurred and to estimate the extent of contamination. Level 2 data differ from Level 1 data in that Level 1 is used to measure "bulk" characteristics of a sample, while Level 2 analyses are used to estimate the concentrations of selected individual compounds.

Level 2 data quality will be used on this project to collect cost-effective (lower cost than Level 3) quality data for use in decision making and in the risk assessment. The level 2 data quality will be evaluated as outlined in Section 8 and the sample results will be confirmed using Level 3 data.

EPA-approved methods will be used to analyze Level 2 samples. Level 2 data quality samples will be analyzed using the same analytical techniques as Level 3 data. The difference between Level 2 and Level 3 will be the frequency and target acceptance windows for laboratory QA/QC samples. The same QA/QC samples will be analyzed for Level 2 as Level 3; however, the QA/QC samples may be analyzed less frequently with broader acceptance limits than with Level 3. For example, for VOCs or SVOCs by GC/MS, for Level 2 an instrument tune check sample will be analyzed once every 24 hours rather than once every 12 hours as required for Level C. A comparison of the Level 2 and Level 3 QA/QC requirements is provided as Appendix B.

Formal data package deliverables are not required for this level of data quality; however, all instrument calibration and sample analysis activities must be documented and this information retained by the laboratory. Data package deliverables may require summaries of laboratory performance information (such as calibration), but the laboratory must maintain all the corresponding documentation for at least 7 years. Data package deliverables will include instrument calibration, sample, method blank results, and matrix spike results. Example data packages will be included in the subcontractor documentation.

Confirmation is critical for samples that are determined by field screening to contain concentrations near the action levels. Approximately 10 percent of the samples will be submitted to an analytical laboratory for additional Level 3 confirmatory testing.

3.2.2.3 Level 3-Laboratory Analyses

The purpose of Level 3 data is to provide the basis for evaluating Level 2 data and for making decisions for further action, if needed, at each of the areas of investigation and to broaden the characterization of contaminants. The TCL has been designed to fully evaluate the potential for contamination from past site activities and to support a preliminary risk evaluation. Only EPA-approved methods from SW-846, Test Methods for Evaluating Solid Waste or EPA CLP methods will be used to analyze samples for

Levels 3 or 4. Level 3 data package deliverables include all the CLP-type QC summary forms, but none of the unreduced experimental data, (summarized in Table 7-1). Therefore, during the data quality evaluation process, it is possible to evaluate the effect of the overall analytical process on the usability of the data; however, it is not possible to recreate the details of the analytical process or sample calculations.

TCLs and reporting limits for Levels 2 and 3 data quality are included in Section 7.

Many of the OU-specific FSPs refer to Level 3 analyses as "TAL/TCL." This is a common usage way of referring to the CLP SOWs lists for organic and inorganic compounds. For this project, "TCL/TAL" refers to VOCs, SVOCs, pesticides, PCBs, metals, and cyanide, but does not refer to dioxins. For TCL/TAL analyses, the CLP target compound lists and reporting limits will be used.

3.2.2.4 Level 4-Laboratory Analyses

Level 4 analytical methods are the same as Level 3; the difference between the levels is in the data package deliverables. Level 3 deliverables include only the QC summary information (typically provided on the CLP QC summary forms or functional equivalents). Level 4 deliverables include the summary forms and all the unreduced, experimental data. Therefore, it is possible for Level 4 data to completely recreate the entire analytical process and recalculate all of the calibration and sample results. For Level 3, this information is summarized on the data sheets and used to evaluate laboratory performance and potential matrix interferences.

There is a potential for Level 4 data to be required in the future at this facility. Samples analyzed using Level 4 QC are analyzed using the same analytical methods as Level 3 samples, but different data package deliverables are provided, as discussed in this section. Confirmatory samples will be analyzed using Level 3 QC, and no Level 4 is proposed at this time. However, if in the future Level 4 information becomes necessary, this information will be requested from the analytical laboratory.

4.0 Field Sampling Procedures

4.1 General Sampling Requirements

The following general sampling requirements will be maintained:

- Prior notification of facility to obtain entry permits for personnel.
- Field sampling teams will consist of a minimum of two individuals. One
 person will collect the sample as the other monitors adherence to sampling
 procedures, records any difficulty encountered, and documents other
 information pertinent to the investigation.
- To the extent feasible during sampling episodes, sampling activities in each medium will be conducted so that the sampling order will be from the area of least contamination to the area of most contamination.
- The preferred order of sample collection will be specified in the OUspecific FSP.
- Sample collection for chemical analysis will be performed with either disposable sampling devices or decontaminated, stainless steel or Teflon[®] devices. When composite samples are required, the sample will be homogenized in stainless steel bowls. All sampling equipment will be decontaminated in accordance with the procedures outlined later in this plan.
- Samples collected for VOC analysis will not be homogenized.
- Precleaned sample containers will be provided by the analytical laboratory
 except for the stainless steel sleeves used for soil sampling, which will be
 decontaminated onsite. All sample container records will be maintained by
 the analytical laboratory and will be available upon request.
- A sample that is representative of the matrix being sampled will be collected.
- Sample integrity will be maintained from the time of sample collection to receipt by the laboratory.

All field notes will be recorded in indelible ink on standard forms in bound notebooks. A daily field log will be completed by the FTL. This log will be signed and dated daily. Significant events occurring during the day will be recorded and reported to the PM. Daily communication is essential to evaluate whether timely corrective actions are

necessary. The field notebook(s) must provide a place for the field team members to sign and date the entries. The FTL must review all field notes.

4.2 Sample Blanks and Field Duplicates

The number of environmental and field QC samples to be collected are discussed in the OU-specific FSP. The three types of sample blanks—travel (trip) blanks, equipment (rinsate) blanks, and field blanks—along with field duplicates and split samples, are discussed below.

4.2.1 Trip Blanks

Trip blanks are to be analyzed for VOCs only, and consist of sample bottles filled in the laboratory with American Society for Testing and Materials (ASTM) Type II water; the sample bottles are then sent to the sampling location with sampling kits. The specified number of trip blanks are returned from the sampling location with every shipment of groundwater samples and analyzed for VOCs. One of these trip blanks will accompany split VOC samples to the COE QA laboratory.

4.2.2 Equipment Blanks

Rinsate blanks for the groundwater samples are processed by rinsing decontaminated sampling equipment with ASTM Type II water obtained from the laboratory. The rinse water is collected in sample bottles, preserved, and handled in the same manner as the samples. Split equipment blank samples of the rinsate will be sent to the COE QA laboratory. Equipment blanks will be collected once a day for the equipment used during sampling procedures.

4.2.3 Field Blanks

Field blanks are samples of source water used for decontamination and are used to monitor the potential for contamination from the source water. Field blanks will be collected once a week from each water source.

4.2.4 Field Duplicates

Field duplicate samples are collected to measure the precision of the sampling process. The FTL will choose at least 10 percent of the total number of sample locations previously known to contain moderate contamination, and will collect duplicate samples from these locations. The source information will be recorded in the field notes, but not on the chain-of-custody (COC) form prepared by the field team at the time of sample collection. The identity of the duplicates will not be given to the analysts. The source information will be forwarded to the QA reviewer to aid in the review and validation of

the data. The source of the field duplicate for the QA samples will be clearly identified on the COC form sent to the QA laboratory.

4.2.5 Split Samples

Split samples are used to calculate the precision of the sampling and analytical processes by providing a measure of comparability between laboratories. Split samples will be submitted to the contractor's laboratory as QC samples and to the COE and EPA/TDEC Laboratories as QA samples. Split samples will be collected from 5 percent of the samples collected at DDMT for the purpose of a quality control check by the Corps of Engineers' laboratory in Missouri. Also, TDEC reserves the right to collect split samples and to analyze these samples by the State of Tennessee laboratory. The contact person at the COE laboratory will be notified at least 2 weeks in advance of the sampling event at (402) 444-4304. The samples will be sent to the following address:

COE Laboratory
Missouri River Division
420 South 18th Street
Omaha, Nebraska 68102

4.2.6 Matrix Spike/Matrix Spike Duplicate (MS/MSD)

MS/MSD samples will be collected and shipped to the laboratory for spike analyses. Five percent of the samples collected will be accompanied by spike samples. However, if a spike sample has not been collected in a 14-day time period, a spike sample will be collected and sent for analyses.

4.2.7 Other Sample Blanks

Samples of the bentonite, sand, and mud used in the drilling process will be collected and retained for future analysis, if necessary.

4.3 Field Documentation

Bound field log books will be maintained by the FTL and other team members to provide a daily record of significant events, observations, and measurements during sampling events. All entries will be signed and dated. All information pertinent to sampling will be recorded in bound log books. Entries in the log book must include at least the following:

- Name and title of author, date and time of entry, and weather/ environmental conditions during field activity
- Location of sampling activity

- Name and title of field crew
- Name and title of any site visitors
- Sample media (for example, groundwater)
- Sample collection method
- Number and volume of sample(s) taken
- Date and time of collection
- Sample identification number(s)
- Sample distribution (for example, laboratory)
- Water level measurement data
- Field observations
- Any field measurements made, such as pH, temperature, and conductivity
- All sample documents such as:
 - Bottle lot numbers
 - Dates and method of sample shipments
 - COC forms
- Sample handling (preservation)

All original data recorded in field log books, sample labels, and COC forms will be written with waterproof, black, indelible ink. None of these accountable, serialized documents are to be destroyed or thrown away, even if one is illegible or contains inaccuracies requiring document replacement. If an error is made on an accountable document assigned to one individual, that individual should make all corrections simply by crossing a line through the error, initialing and dating the correction, and entering the correct information. The erroneous information should not be obliterated. Any subsequent error discovered on an accountable document should be corrected by the person who made the entry. All subsequent corrections will be initialed and dated.

4.4 Sample Numbering and Containers

The FTL is responsible for proper sampling, labeling of samples, preservation, and shipment of samples to the laboratory to meet required holding times. Table 4-1

Table 4-1
Required Sample Containers, Preservation, and Holding Times
Defense Depot Memphis, Tennessee

Analyses	Sample Matrix*	Container†	Quantity	Preservative**	Holding Time
Volatile Organic Compounds (SW8240)	W	40-mL VOA vials††	3	Cool 4°C, HCl, pH <2	14 days
	S	4-oz Glass	1	Cool 4°C	14 days
Semivolatile Organic Compounds	w	1-L amber glass	2	Cool 4°C	7/40 days***
Pentachiorophenoi (8151)	S	1-L amber glass	2	Cool 4°C	7/40 days
BNAs (8270/3520)	S	4-oz Glass	1	Cool 4°C	40 days
PAHs (8310/3520)	w	1-L amber glass	2	Cool 4°C	7/40 days***
Pesticides/PCBs (8080/3520)	w	1-L amber glass	2	Cool 4°C	7/40 days***
	s	4-oz Glass	1	Cool 4°C	40 days
Organopesticides (8150/3520)	w	1-L amber glass	2	Cool 4°C	7/40 days***
Thiodyglycol (U109)	w	40-mL vials††	2	Cool 4°C	40 days
(LL09)	s	8-oz Glass	1	Cool 4°C	7/40 days***
Metals (Total) (6010, 7000)	w	1-L polyethylene	1	Cool 4°C, HNO ₃ , pH <2	6 months
	s	8-oz Glass	1	Cool 4°C	6 months
Metals (Dissolved) (6010, 7000)	w	1-L polyethylene	1	Cool 4°C, HNO ₃ , pH <2	6 months
Mercury (7470)	W	1-L polyethylene	1	Cool 4°C, HNO ₃ , pH <2	28 days
	s	8-oz Glass	1	Cool 4°C	28 days
Chromium VI (7196)	w	1-L polyethylene	1	Cool 4°C, HNO ₃ , pH <2	24 hours
	S	4-oz Glass	1	Cool 4°C	24 hours
Total Dissolved Solids (160.1)	w	1-L polyethylene	1	Cool 4°C	7 days

^{*}Sample matrix: S = Surface soil, subsurface soil, sediment;

Source: RI Report, 1990

W = Groundwater, surface water

[†]Glass containers will be sealed with Teflon®-lined screw caps

^{**}All samples will be stored promptly at 4°C in insulated chest.

^{††}VOC vials will be sealed with Teflon®-septa secured screw caps.

^{***}Extraction: 7 days for water, 40 days for analysis.

identifies the proper containers, preservation techniques, and maximum holding times according to EPA SW-846.

4.5 Sampling Numbering System

A sample numbering system will be used to identify each sample collected during the field investigation and for all blanks. The numbering system will provide a tracking procedure to allow retrieval of information about a particular location and to monitor that each sample is uniquely numbered. The FTL will maintain a list of sample numbers.

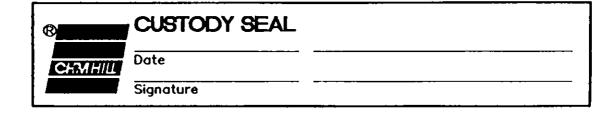
4.6 Sample Chain-of-Custody

Sample custody and documentation procedures described in this section will be followed throughout all sample collection at DDMT. Components of sample custody procedures include the use of field log books, sample labels, custody seals, and COC forms. Examples of these are present in Figures 4-1 and 4-2. Each person involved with sample handling will be trained in COC procedures before the implementation of the field program. The COC form will accompany the sample during shipment from the field to the laboratory. If samples are split and sent to different laboratories, a copy of the COC form will accompany each split sample.

The information provided on the COC form will include the following:

- The project name
- The sampling station number or sample number
- Date and time of collection
- Grab or sample designation
- A brief description of the type of sample and sampling location
- Signature of individuals involved in the sample transfer
- The time and date they receive the sample
- Sample matrix
- The analytical methods required

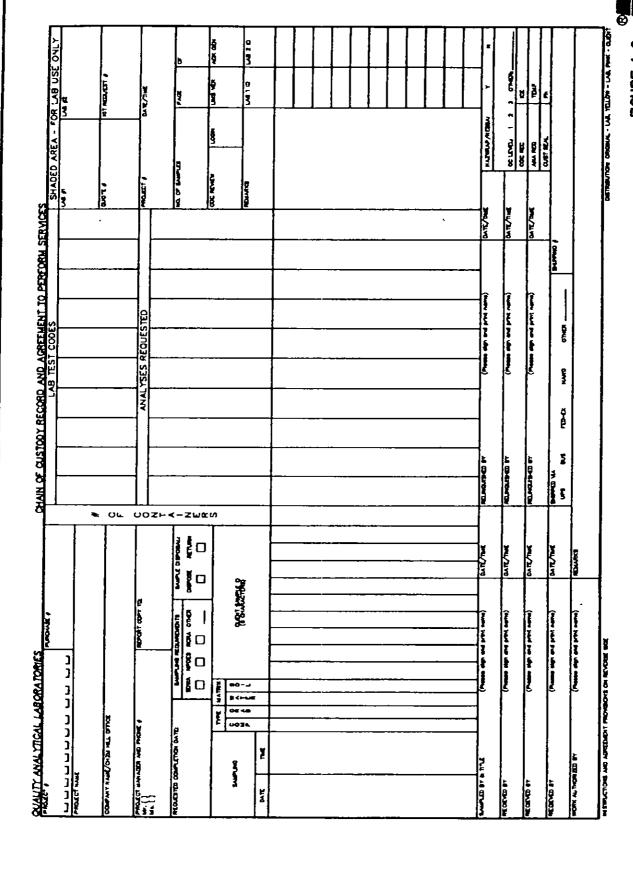
COC records initiated in the field will be placed in a plastic cover and taped to the inside of the shipping containers used for sample transport from the field to the laboratory. This record will be used to document sample custody transfer from the field sampler to the laboratory.



#	PH. (205) 271-1444 Montgomery Laboratory 2567 Fairlane Drive Montgomery, Alabama 3616
ė	CLIENT
⋩	SAMPLE NO
ΑŢΟ	LOCATION
LABORATORY I.D. #	ANALYSIS
	PRESERVATIVE
	DATEBY

FIGURE 4-1
EXAMPLE CUSTODY SEAL AND SAMPLE CONTAINER LABEL
Defense Depot Memphis, Tennessee





EXAMPLE CHAIN OF CUSTODY RECORD Defense Depot Memphis, Tennessee

CHMHILL

MQP-0005 DWG 02-21-95

4.6.1 Sample Custody

A sample is under custody under the following conditions:

- It is in your actual possession; or
- It is in your view, after being in your physical possession; or
- It was in your physical possession and then you locked it up to prevent tampering; or
- It is in a designated and identified secure area.

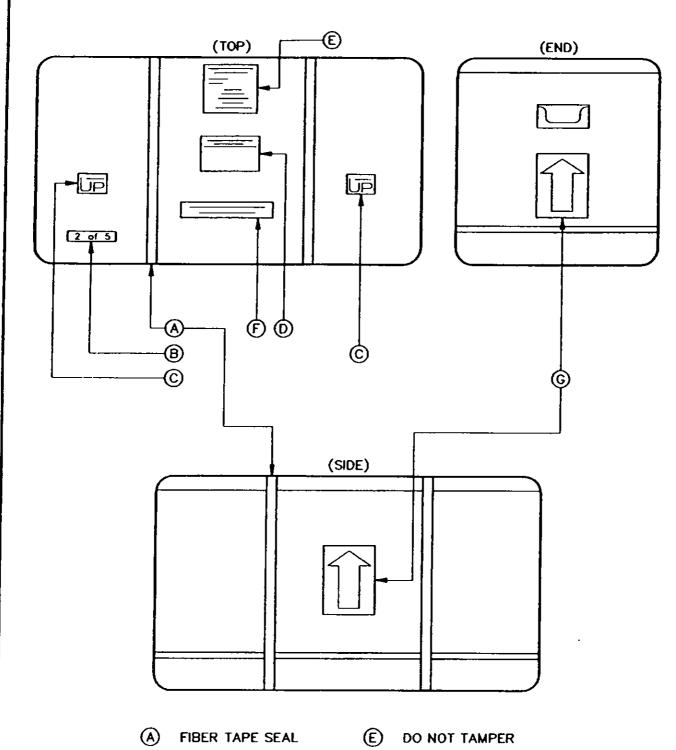
4.6.2 Sample Custody in the Field

The following procedures will be used to document, establish, and maintain custody of field samples:

- Sample labels will be completed for each sample, with waterproof ink, making sure that the labels are legible and affixed firmly on the sample container (see Figure 4-1).
- All sample-related information will be recorded in the project log book.
- The field sampler will retain custody of the samples until they are transferred or properly dispatched.
- During the course of and at the end of the field work, the field supervisor determines whether these procedures have been followed, and whether additional samples are required.

4.7 Sample Shipment

Samples will be delivered to the designated laboratory. During sampling and sample shipment work, the FTL (or a designee) will contact the appropriate laboratory daily to inform it of shipments. Hard plastic ice chests or coolers with similar durability will be used for shipping samples. The coolers must be able to withstand a 4-foot drop onto solid concrete in the position most likely to cause damage. Styrofoam or bubble wrap will be used as packing material to protect the samples from breakage during shipment. All water VOC vials will be shipped in the same cooler. After packing is complete, the cooler will then be taped shut with COC seals affixed across top and bottom joints. Each container will be clearly marked with "THIS END UP" arrows on all four sides and a sticker containing the originator's address. Figure 4-3 provides a schematic for proper labeling of the cooler.



- B CHEST NUMBER
- C THIS SIDE UP
- (D) ADDRESS LABEL
- (F) ENVIRONMENTAL LAB SAMPLES
- **(G)** UP ARROW

FIGURE 4-3
PROPER LABELING OF AN ICE CHEST
FOR LOW LEVEL SAMPLES
Defense Depot Memphis, Tennessee



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The following procedures will be used when transferring the samples for shipment:

- Samples are accompanied by a COC form. When transferring the possession of samples, the individuals relinquishing and receiving will sign, date, and note the time on the record. This record documents transfer of custody of samples from the field sampler to another person, or to the laboratory. Overnight carriers will be treated as a single entity and a single signature will be required when the samples are delivered to the laboratory.
- Samples will be properly packaged for a shipment and dispatched to the appropriate laboratory for analysis with a separate signed COC form enclosed in each sample box or cooler.
- Whenever samples are split with a government agency, a separate COC form will be prepared for those samples and marked to indicate with whom the samples are being split.
- All packages will be accompanied by a COC form showing identification of the contents. The original record will accompany the shipment, and a copy will be retained by the FTL.

4.8 Laboratory Sample Custody

The FTL will notify the laboratory of upcoming field sampling activities and the subsequent transfer of samples to the laboratory. This notification will include information concerning the number and type of samples to be shipped, as well as the expected date of arrival.

The following procedures will be used by the laboratory sample custodian in maintaining the COC once the samples have arrived at the laboratory:

- The laboratory will designate a sample custodian who is responsible for maintaining custody of the samples and for maintaining all associated records documenting that custody.
- Upon receipt of the samples, the custodian will check the original COC and request-for-analysis documents and compare them with the labeled contents of each sample container for corrections and traceability. The sample custodian signs the COC and records the date and time received. The sample custodian also will assign a unique laboratory sample number to each sample.

- Care is exercised to annotate any labeling or descriptive errors. In the
 event of discrepancies in the documentation, the laboratory will
 immediately contact the FTL as part of the corrective action process. A
 qualitative assessment of each sample container is performed to note any
 anomalies, such as broken or leaking bottles. This assessment is recorded
 as part of the incoming COC procedure.
- If all data and samples are correct, and there has been no tampering with the custody seals, the "received by laboratory" box is signed and dated.
- The samples are stored in a secured area and at a temperature of approximately 4°C, if necessary, until analyses are to begin.
- Samples are accompanied by a COC form. When transferring the possession of samples, the individuals relinquishing and receiving will sign, date, and note the time on the record. This record documents transfer of custody of samples from the field sampler to another person, or to the laboratory.
- A laboratory COC form accompanies the sample or sample fraction through final analysis for control.
- Copies of the COC and request-for-analysis forms will accompany the laboratory report and will become a permanent part of the project records.

4.9 Disposal of Derived Wastes

In the following sections, the disposal of derived wastes is discussed.

4.9.1 Purged/Development Water and Decontaminating Fluids

Development and purged water will be collected, stored, and analyzed (if required). The discharge will be conducted in accordance with the DDMT industrial discharge permit application (currently being applied for). The processed water will be collected in a storage tank for disposal to the City of Memphis sanitary sewer system (consistent with the permit). Solids will be allowed to settle out of the water before being transferred to the treatment system.

4.9.2 Storage, Analysis, Treatment, and Disposal of Investigation-derived Wastes

All monitoring well and soil boring cuttings will be collected and placed in DOTapproved drums. A label will be affixed to each drum clearly indicating the boring number and depth interval from which the cuttings originated. The site geologist will maintain a log detailing the disposition of cuttings from each hole. The drums will be stored in the permitted Resource Conservation and Recovery Act (RCRA) storage area pending the results of the chemical analysis (toxicity characteristic leaching procedure [TCLP]), which will determine the disposition of the contents (if they are determined to be hazardous or nonhazardous by the toxicity characteristic).

4.9.2.1 Soil Waste

Analytical sample results from the investigation will be reviewed to evaluate whether any of the soil waste might exceed TCLP criteria. Upon completion of the data evaluation, a letter report will be submitted to DDMT detailing the drums that contain cuttings that are nonhazardous and may be disposed of onsite as fill. The sample from each drum will be collected using a stainless steel scoop and will be obtained immediately below the surface material in each drum. No attempt will be made to obtain depth-integrated samples from within the drums because of the homogenization expected during filling of the drums. Analysis of these samples will be at DQO analytical Level 3. Upon completion of laboratory analysis, a report will be submitted to DDMT detailing those drums containing cuttings that the should be considered hazardous waste (HW). The report will identify options for treatment and disposal of the HW in accordance with applicable federal and State of Tennessee regulations. The contents of the drums will be identified with a composite representative analytical sample. Of particular concern are cuttings with metals (primarily arsenic, chromium, and lead) contamination. The RI Report (ref. 7) reported widespread occurrence of metals concentrations in both surface and subsurface soils. A number of these samples were obtained from areas with no known source of metals contamination.

Soil and cuttings from the decontamination basin will be collected in drums. The site geologist will record the well number(s) from which decontamination sediments were added to the drum. Labeling and handling of the drums from decontamination will follow the same procedures as the drums of drill cuttings.

4.9.2.2 Classification and Disposal of Soil Waste

If the analysis of a soil sample indicates that organic compounds or metals exceed either federal or state TCLP limits (whichever is more stringent), then the drum(s) associated with that sample will be considered HW and will be disposed in accordance with federal and state requirements through the Defense Reutilization and Marketing Office (DRMO) at DDMT. Drums containing cuttings that were recommended to be considered nonhazardous will be disposed only upon specific written instructions from DDMT.

4.9.2.3 Personal Protective Equipment and Disposable Equipment Waste

All disposable personal protective equipment (PPE) waste (gloves, coveralls, decontamination supplies, protective coverings, respirator canisters, booties, and splash suits) and disposable equipment (DE) waste (plastic ground and equipment covers,

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Teflon[®] tubing, conduit pipe, and aluminum foil) used during the study will be collected and double bagged. PPE and DE wastes are generally classified as nonhazardous wastes (ref. 31) and will be disposed in dumpsters at DDMT. This procedure is in accordance with Ref. 31.

5.0 Field Procedures

5.1 Groundwater

Groundwater sampling efforts will be conducted to identify and evaluate contaminants in the groundwater beneath and around DDMT. A summary of the quantity of samples to be collected and the parameters to be tested during chemical analysis is provided in the OU-specific FSP. Table 4-1 provides minimum laboratory QC sample requirements, including container type, container quantities, preservatives, holding times, SW-846 Methods, and extraction and preparation methods for each parameter.

5.1.1 Groundwater Sample Locations and Rationale

Groundwater samples will be collected for chemical analysis from both existing and newly constructed monitoring wells at DDMT. Collection and analysis of groundwater samples are planned for selected Memphis Light, Gas, and Water (MLGW) monitoring wells in the Allen Well Field. These samples will be collected if groundwater analysis from any of the optional wells (along Elvis Presley Boulevard) show that the contamination has migrated from Dunn Field to the wells on Elvis Presley Boulevard. In the event that recent groundwater data are not available from MLGW, efforts will be coordinated with MGLW to obtain the necessary approval to collect and chemically analyze groundwater samples from the Allen Well Field monitoring wells. Groundwater samples from the wells will be analyzed for several reasons: to characterize sites and to evaluate the nature of releases from disposal sites at DDMT; to evaluate the vertical and horizontal extent of a potential contaminant plume in the Fluvial Aquifer; to evaluate whether contaminants in the Fluvial Aquifer pose a threat to the Memphis Sand Aquifer; and to obtain background water quality data (offsite and upgradient wells) for comparative study. The specific rationale for collecting groundwater samples from each location will be provided in the OU-specific FSP. Additional samples to be analyzed will include equipment blanks, field duplicates, and samples of water from the wells. Split field duplicates and split equipment blanks will routinely be sent to the CEMRD.

5.1.2 Groundwater Sampling Procedures

Before groundwater sample collection, static water levels in the monitoring wells will be measured to calculate groundwater purge volumes. Water level measurements collected for this purpose will be obtained within 24 hours of purging the monitoring well.

Groundwater levels used to construct a groundwater potentiometric surface map will be collected within a 24-hour time frame, provided that barometric conditions remain essentially the same. This will be determined by using a barometer during water level measurements. The intent of this requirement is to obtain water levels during a short time frame during which no significant barometric variations occurred (all readings within 0.25-inch mercury), and not to obtain water levels within a 24-hour period when

significant barometric variations did occur (readings greater than 0.25-inch mercury). All water levels will be measured using a decontaminated, electronic water level indicator with an accuracy of plus or minus 0.1 foot. Monitoring well sampling will generally proceed from the potentially least contaminated well to the most contaminated well, according to existing data.

To prevent contamination of sampling equipment by surface soils when the wells are being purged or sampled, a plastic ground cloth will be placed beneath all sampling equipment. Purging will be accomplished through the use a decontaminated stainless steel submersible pump or Teflon® bailer. The discharged water will be monitored for pH, temperature, and specific conductivity. Purging will continue until three to five well volumes have been removed and the pH, temperature, and conductivity are stabilized (three successive measurements are within 5 percent of one another).

The amount of purged fluid will be measured by filling graduated buckets or by using a stopwatch and noting the flow rate of the pump versus elapsed times. All water purged from the wells will be permitted for discharge to the city sewer. Wells will be sampled immediately after purging, if possible, but no later than 6 hours after purging. Wells that recharge slowly will be purged dry and allowed to recharge to at least 80 percent of initial well volume before sampling. If excessive time (greater than 10 hours) is required for the slow recharging wells to recharge to 80 percent, it will be documented by the FTL in the field log. To monitor that data is consistent, all wells will be sampled within a 14-day time frame.

Clean disposable vinyl gloves will be used to handle all samples and equipment used for purging and sample collection. Each well will be sampled with a Teflon[®] bailer decontaminated according to procedures described previously. Precleaned bailers will be wrapped in aluminum foil for transportation to DDMT. A clean, braided nylon cord will be used to lower each bailer into the well and will be discarded after each use. Care will be taken to prevent contact between the bailer and line and the ground.

Samples will be collected in accordance with the guidelines furnished in the *Practical Guide for Ground Water Sampling* (ref. 1) and the *EPA Region IV ECBSOPQAM* (ref. 31). In accordance with EPA's Environmental Services Division guidelines, care will be taken to avoid aeration of the sample. The sample will be poured in a slow, steady stream from the bailer to the prepared sample containers. The process will be repeated as necessary to fill each container to the required volume. Field measurements of pH, specific conductance, and temperature will be conducted and recorded using instruments that have been calibrated daily and decontaminated before each use. Temperature will be measured immediately upon pouring the sample from the bailer into a glass beaker.

Samples to be analyzed for VOCs will be collected first, to minimize the effects of volatilization caused by disturbance of the water surface in the well. VOC sample containers will be filled completely to the top of the container, leaving no air space above the liquid. Before transport to the laboratory for analysis, samples will be preserved in

accordance with the guidelines in Table 4-1. Trip blanks will be included with each container holding samples to be analyzed for VOCs. Groundwater samples also will be collected by EPA and state regulators on a regular basis throughout the project.

5.2 Soil

5.2.1 Surface Soil

Surface soil samples will be collected and analyzed to identify and to delineate contaminants in the surface soils at sites and at some offsite locations (for background sampling). A summary of the quantity of samples to be collected and the parameters to be tested during chemical analysis is provided in the OU-specific FSP. Container type, container quantities, preservatives, holding times, SW-846 Methods, and extraction and preparation methods for each parameter are provided in Table 4-1. This section of the QAPP identifies the general requirements and purposes for collection of surface samples, including the field QA/QC methods.

5.2.2 Surface Soil Sampling Procedures

Surface soil samples will be collected using a clean stainless-steel hand auger or scoop to retrieve soil from zero to 12 inches below ground surface (bgs). Any VOC samples will be placed in the appropriate jars immediately upon collection. The remaining sample will be thoroughly mixed in a stainless-steel mixing bowl before being transferred to the appropriate sample containers. Surface cover (grass and weeds) and debris (such as broken glass and rocks) will be removed from the sample prior to placing in sample containers.

5.2.3 Subsurface Soils

Subsurface soil samples from soil borings will be collected for chemical analyses from both soil and monitoring well borings installed for this study. Samples will generally be selected on the basis of historical data results, field screening during sampling, or both. The overall purpose of this sampling effort will be to characterize the subsurface conditions by providing soil samples for chemical analysis to determine the nature and extent of releases of hazardous substances to the environment from waste disposal sites on DDMT, as well as the vertical and horizontal extent of such contamination in the subsurface soils; to evaluate soil lithology and subsurface stratigraphy; and to help characterize the potential hydraulic interconnection between the Fluvial Aquifer and the Memphis Sand Aquifer on the Main Installation. Soil samples also will be collected for geotechnical lab analyses. Locations and justifications for sample collection, including background samples and offsite locations, are provided in the OU-specific FSPs. Additional samples to be analyzed include equipment blanks and field duplicates (to fulfill QA/QC requirements) and samples from soil cuttings to determine disposal requirements. Split field duplicates and equipment blanks will routinely be sent to the CEMRD

laboratory. Trip blanks will be included with each container holding samples to be analyzed for VOCs.

5.2.4 Subsurface Soil Sampling Procedures

Three types of subsurface soil samples will be collected—vertical (shallow) soil borings, vertical (deep) soil borings. The specific number of samples for chemical analysis and depths of collection are discussed in the OU-specific FSPs. However, in general, one soil sample will be collected from the first 12 inches for all borings, from an intermediate depth based on field screening, and from the saturated zone of some vertical (deep) borings for geotechnical analyses. Soil samples will collected on the basis of visual or organic vapor analyzer/photoionization detector (OVA/PID) field screening. Soil samples will be stored in airtight containers and shipped daily to the laboratory for analysis. Geotechnical sample collection and analyses are discussed in Section 5.4. The general analyses include grain size, moisture content, and Atterberg limits. Grain size analysis will be performed on the aquifer material. Atterbergs will be performed on the fine silty to clay material. If the confining layer at the base of the Fluvial Aquifer is penetrated, Atterberg limits will be performed on the retrieved sample to evaluate the condition and character of the clay. The final decision to collect a sample from a certain zone will be at the discretion of the field geologist. This decision will be documented in the field log.

5.3 Surface Water and Sediment Samples

Surface water samples will be collected and analyzed to determine whether storm waters are contributing to the degradation of the Golf Course Pond and Lake Danielson and to determine if sites at DDMT are affecting the quality of storm water runoff waters leaving the installation. Specific location criteria and analysis will be identified in the appropriate OU FSP. Sediment samples will be collected from the same location as surface water samples to the extent possible. Collecting sediment and surface water samples from the same location will be easily accomplished at Lake Danielson and at the Golf Course Pond. However, it may not be possible for some of the storm water drainage channels. The samples will be taken from various locations around DDMT and will be used to further define sites previously identified in the RI Report (ref. 7) and the RFA (ref. 25) and to help characterize any possible sources for contaminants found in Lake Danielson, in the Golf Course Pond, and in storm water drainage channels.

5.3.1 Surface Water Sampling Procedures

After a rainstorm with at least 0.2 inches of precipitation, when quantities of surface water/runoff are sufficient for collection, samples will be collected for chemical analysis. Sampling locations are identified in the OU-specific FSPs, which are considered representative of surface water runoff from the installation. These samples will be used to determine whether storm waters are contributing to the degradation of the lakes and runoff waters leaving the installation. Samples may be collected from storm drainage

ditches will be a single grab sample taken at mid-depth from the center of the channel. Samples collected from Lake Danielson and from the Golf Course Pond. If so, they will be collected from the estimated deepest point of the lake or pond and, with the exception of the volatile sample, will consist of single vertical composite (depth integrated) samples. The vertical composite samples will be taken using a decontaminated stainless steel Kemmerer sampler or bailer. The physical water quality parameters of specific conductivity, temperature, pH, and dissolved oxygen will be measured at each sampling point. Specific conductivity, temperature, dissolved oxygen, and pH will be measured with an electronic meter. The first draw of sample will placed into the VOC containers immediately if a bailer or Kemmerer sampler is being used. An aliquot will be placed in each container from each subsequent draw until the bottles are filled.

Samples will be collected from the surface directly into the container where the column of water is less than 1 foot deep and when no preservatives are required in the sampling bottle. Samples requiring preservatives will be collected in a spare bottle that has been rinsed twice in the water to be sampled. The sample collected will then be transferred to the appropriate container. Sediment samples will be collected at the location of all surface water samples unless the sample is obtained from a concrete-lined drainage ditch with no accumulated sediment. If sediment samples are also to be collected, the surface water samples will be collected first. Care will be taken to prevent disturbance of the sediments in the stream, lake, or pond.

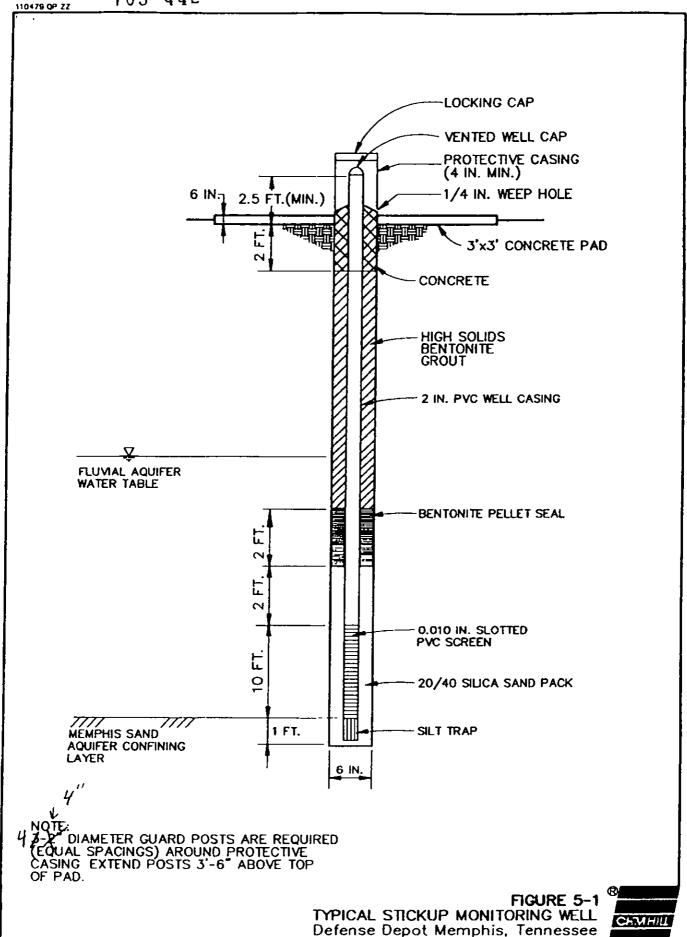
5.3.2 Sediment Sampling Procedures

Samples of sediment from the drainage ditches will be collected using a stainless steel scoop. The samples will be collected when there is no flow in the ditch or when the flow allows wading to the sample location. Field judgment will be exercised when collecting sediment samples. The depth of sampling will be limited to zero to 12 inches for surface sediments. Smaller intervals may be used to limit sampling to sediments rather than native soil. The sampling interval will be documented in the field logbook. If there is flow in the stream, the sample location will be approached from downstream of the point facing into the current. All non-purgeable organic samples will be thoroughly mixed in a stainless steel mixing bowl before being transferred to the appropriate sample container. Sediment samples that are to be analyzed for VOCs will be immediately placed in the appropriate sample container and filled completely. No head space will remain in the sample container.

5.4 Soil Boring and Monitoring Well Drilling Procedures

5.4.1 Permitting and Design of Monitoring Wells

The design and construction of monitoring wells will follow (as closely as practical) the design criteria presented in the Handbook of Suggested Practices for the Design and Installation of Groundwater Monitoring Wells (ref. 37) and EPA Region IV ECBSOPQAM



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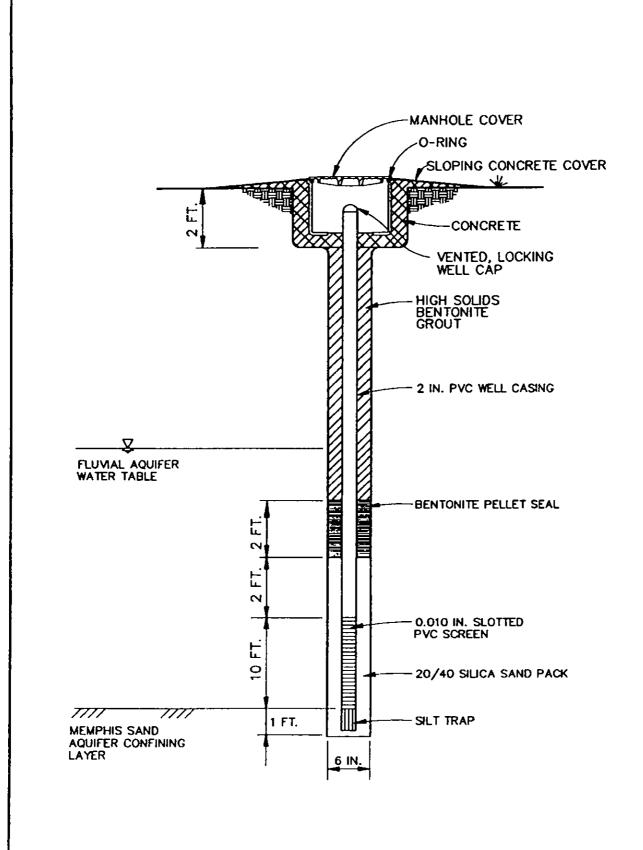


FIGURE 5-2
TYPICAL FLUSHMOUNT MONITORING WELL
Defense Depot Memphis, Tennessee



(ref. 31). Diagrams of typical well construction details are shown in Figures 5-1 and 5-2. Drilling and field personnel will have all applicable state and local certification required for drilling. DDMT will be responsible for obtaining the required entry permits for offsite locations. Additionally, Figures 5-3 and 5-4 show the construction details of the proposed Memphis Sand Aquifer Monitoring Well (Section 4.6 of the OU-4 FSP).

5.4.2 Installation of Monitoring Wells and Soil Borings

The procedures described below will be followed for monitoring well installation and soil borings.

5.4.2.1 General Requirements

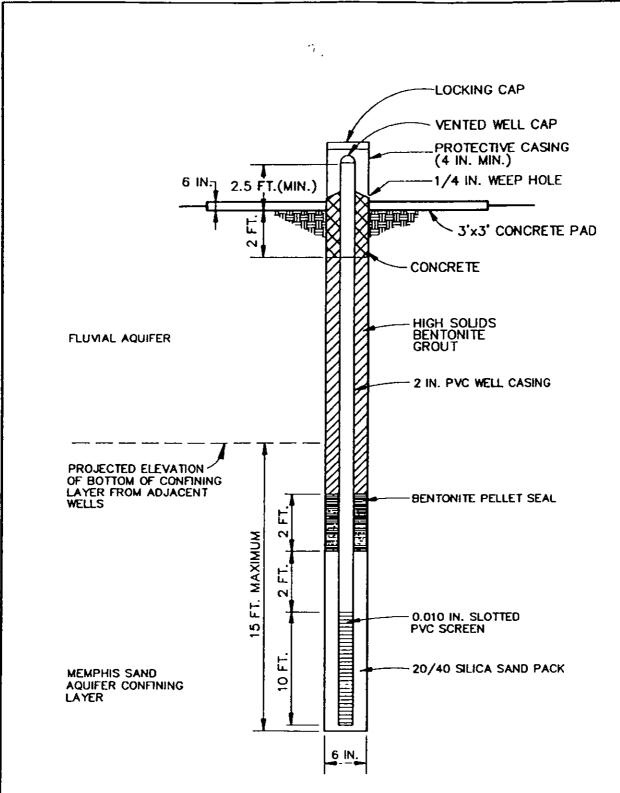
The drilling contractor will provide all drilling equipment, materials, and personnel required to install the monitoring wells and soil borings. A qualified geologist or geotechnical engineer will be onsite for all drilling, installation, development, and testing activities.

5.4.2.2 Protection of Water-yielding Zones

Water will be used during drilling only when absolutely necessary for successful installation of the well. During the drilling of wells at DDMT for the RI/FS, a zone of flowing sand was encountered in some boreholes. This zone made removal of the auger from the hole difficult, especially when it was left in overnight. In such an instance, water or an additive may be necessary to keep the hole open. If water is required during drilling or well installation, only non-chlorinated potable water will be used. If an additive is required, only pure bentonite will be used. Any proposed use of water or bentonite will be cleared through the CEHND Contracting Officer before use. Grease or oil on drill rod joints will not be permitted; neither will dispersing agents such as phosphates or acids. Toxic and contaminating substances will be prohibited during any part of the drilling, well installation, or well development activities. No attempt will be made to chemically disinfect the well.

All drilling activities and methods will be performed to prohibit the introduction of contaminants from one zone to another, particularly from the Fluvial Aquifer to the Memphis Sand Aquifer. Monitoring well borings intended to penetrate the Memphis Sand Aquifer will be completed with an isolation casing that will be pressure-grouted to approximately 3 ft into the confining layer. The grout will be allowed to set for a minimum of 24 hours before advancing the borehole and installing a monitoring well.

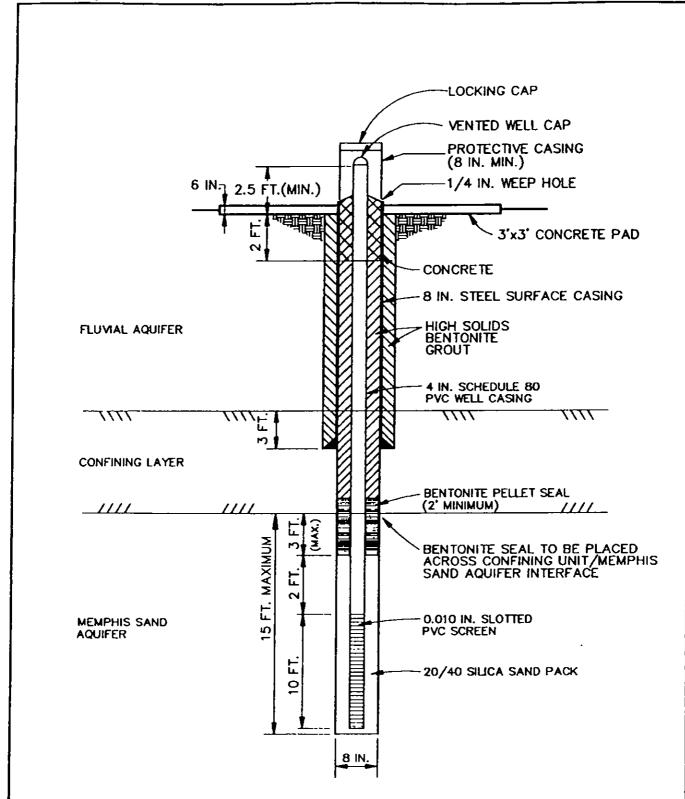
When material is removed from the confining unit for confirmation or laboratory testing from a soil boring, the base of the borehole will be backfilled using tremie pipe to pump pure bentonite containing at least 20 percent solids to the top of the confining unit.



NOTE:
3-2" DIAMETER GUARD POSTS ARE REQUIRED
(EQUAL SPACINGS) AROUND PROTECTIVE
CASING. EXTEND POSTS 3'-6" ABOVE TOP
OF PAD. SEE FIGURE 5-2 FOR FLUSHMOUNT
INSTALLATION.

FIGURE 5-3
MEMPHIS SAND AQUIFER MONITORING WELL
WITHOUT CONFINING UNIT
Defense Depot Memphis, Tennessee





NOTE:
3-2" DIAMETER GUARD POSTS ARE REQUIRED
(EQUAL SPACINGS) AROUND PROTECTIVE
CASING. EXTEND POSTS 3'-6" ABOVE TOP
OF PAD. SEE FIGURE 5-2 FOR FLUSHMOUNT
INSTALLATION.

FIGURE 5-4
MEMPHIS SAND AQUIFER MONITORING WELL
WITH CONFINING UNIT
Defense Depot Memphis, Tennessee



5.4.2.3 Drilling Techniques

Drilling techniques will be followed as described below.

Soil Borings. The DDMT soil borings and monitoring wells will be installed using hollow stem auger (HSA), mud rotary (MR), water rotary (WR), rotosonic, or another EPA-approved alternative drilling technique.

It is acknowledged that the HSA technique is preferable for installation of the monitoring wells and will be used whenever possible. As stated previously, a zone of flowing sand has been encountered during previous drilling operations at DDMT. If the auger becomes ineffective in the sands, a center plug will be used. If the center plug is ineffective, WR will be used. MR will be used only as a last resort. The drill rigs will install a minimum 7-inch-diameter borehole to facilitate installation of 2-inch inside diameter (ID) casing and screens for the Fluvial Aquifer monitoring wells. If soil borings and monitoring wells are to be installed in the Memphis Sand Aquifer, a larger diameter boring will be drilled for installation of the isolation casing. The drill rig will have the capability to collect split-spoon samples according to ASTM procedures. At a minimum, the rig will be equipped with a cathead-operated, 140-pound hammer with a 30-inch draw.

Hollow Stem Auger Technique. When a boring is advanced using HSA, the following protocol will be followed to install the well casing and screen in the shallow wells:

- Install the 2-inch screen and riser through the HSAs with enough riser pipe to extend the well casing about 2 ft above the ground surface.
- Install an artificial sand pack through the annular opening, using a tremie pipe.
 Water in small amounts may be used to prevent bridging of the sand in the annulus.
- Remove hollow stem augers in increments as the annulus space fills with sand.
- Continue installing sand pack until it reaches at least 2 ft above the top of the well screen.
- Install a minimum 2-foot pure bentonite seal of at least 20 percent solids using a tremie pipe.
- Remove HSAs from boring.
- Grout boring annulus to within 2 ft of ground surface using a tremie pipe and high solids pure bentonite grout. Install steel security cap and a 3-foot by 3foot by 6-inch concrete pad with protective posts if the well is in a high-traffic

area. The grout will be allowed to set a minimum of 48 hours before developing the well.

Water Rotary Technique. When a boring is advanced using WR, the following protocol will be followed to install the well casing and screen the shallow wells:

- After termination of boring, all drilling rods will be removed.
- Install the 2-inch screen and riser, with enough riser pipe to extend about 2 ft above the ground surface. Centralizers may be necessary to center the pipe in the borehole.
- Install the sand pack with a tremie pipe from the bottom of the boring until at least 2 ft above the well screen.
- Install a minimum 2-foot pure bentonite seal with at least 20 percent solids.
- Grout boring annulus to within 2 ft of the ground surface using a tremie pipe and high solids, pure bentonite grout. Install steel security cap and a 3-foot by 3-foot by 6-inch concrete pad with protective posts if the well is in a high-traffic area. The grout will be allowed to set a minimum of 48 hours before developing the well.

Mud Rotary Technique. When a boring is advanced using MR, the protocol described below will be followed to install the well casing and screen in the shallow wells:

- After termination of boring, all drilling rods will be removed.
- Install the 2-inch screen and riser, with enough riser pipe to extend about 2 ft above the ground surface. Centralizers may be necessary to center the pipe in the borehole.
- Remove the mud cake from the boring well by pumping potable water through the well riser and screen.
- Install the sand pack with a tremie pipe from the bottom of the boring until at least 2 ft above the top of the well screen.
- Install minimum 2-foot bentonite seal.
- Grout boring annulus to within 2 ft of ground surface using a tremie pipe and high solids pure bentonite grout. Install steel security cap and a 3-foot by 3-foot by 6-inch concrete pad with protective posts. The grout will be allowed to set a minimum of 48 hours before developing the well.

Rotasonic Drilling (RD) Technique. When a boring is advanced using RD, the following protocol will be followed to install the well casing, screen, and cover for the shallow wells:

- At the termination depth of the boring, the inner drill pipe and core barrel containing the soil sample (typically up to 10 ft in length) are removed.
- Install the 2-inch monitoring well casing and screen through the outer drill pipe (usually 6- or 8-inch ID) using enough casing (riser) that the well extends about 2 feet above the ground surface.
- Install an artificial sand pack through the annular opening using a 1- or 1.5-inch tremie line. The drill pipe and well casing can be vibrated to minimize the potential for bridging of the sand in the annulus. Water in small amounts may also be used to minimize the potential for bridging.
- Remove the outer drill pipe in increments and allow the annular space to fill
 with sand. Repeat this process until the sand extends at least 2 feet above the
 top of the well screen.
- Install a minimum 2-foot bentonite slurry seal containing at least 20 percent solids into the annular space using a tremie pipe. Granular bentonite (pellets or chips) may be slowly poured into the annular space as an alternative to the bentonite slurry. If granular bentonite is used, the drill pipe and well casing can be vibrated to minimize the potential for bridging. Potable water should be used to hydrate the pellets or chips if the bentonite interval occurs above the water table. A minimum of 4 hours should be allowed for the bentonite to hydrate before grouting the remaining annular space.
- Grout annulus to within 2 feet of ground surface using a tremie pipe to pump a neat cement-bentonite sealant in the annular space. During the placement of the grout above the bentonite seal, the outer drill casing is incrementally removed, allowing this material to completely fill the annular space.
- Install a locking steel security cover within a 3-foot by 3-foot by 6-inch concrete pad. A minimum of three high-visibility steel protective posts will be installed around the concrete pad if the well is in a high-traffic area. The grout within the annular space of each monitoring well will be allowed to cure a minimum of 48 hours before beginning well development.

5.4.2.4 Borehole Abandonment Procedures

Upon completion of each borehole, or if for any reason a well must be abandoned during drilling, the abandonment will follow the procedure as outlined in Section E.8.1 of EPA's ECBSOPOAM (ref. 31).

5.4.2.5 Well Design

Well Riser and Screen. The OU-specific FSP will dictate the requirements for each specific proposed monitoring well. In general, the risers and screens used in well construction will be made of polyvinyl chloride (PVC) (meeting National Sanitation Foundation [NSF] Standard 14). PVC is preferred to stainless steel where possible because all of the existing monitoring wells at DDMT have PVC screens and risers. To have comparable results, wells that will be installed should be constructed with similar materials.

Additionally, previous analytical results from existing monitoring wells at DDMT indicate that contamination is not affecting well materials. There has been no indication of degradation of the well materials resulting in well failure or leaching of organics from the well materials. Thus, the sample and data quality will not be adversely affected by using PVC.

Continued use of PVC for well construction materials will provide water samples that will be consistent with samples from the existing monitoring wells without sacrificing data quality. This approach is consistent with technical information provided in Ref. 33, an EPA report concerning the selection well materials and contaminants, and Ref. 34, a COE report documenting surface changes in well casing pipes exposed to high concentrations of organic compounds. However, if DNAPL concentrations are detected during drilling operations or if contaminants are present in concentrations that degrade PVC well casing materials (ref. 41), then stainless steel will be used as the well construction material in the area of DNAPL concentration.

Riser. Wells installed in the Fluvial Aquifer will be constructed of new threaded, flush joint, PVC pipe with a nominal 2-inch diameter. Well risers will conform to the requirements of ASTM-D 1785 Schedule 40 pipe and NSF Standard 14 PVC, and will be clearly identified as such. Any Memphis Sand Aquifer wells will consist of new threaded, flush joint, Schedule 80 PVC pipe with a nominal 4-inch diameter and will conform to NSF Standard 14.

Screen. The well screens will be a minimum of 10 ft long and will be constructed of ink- and printing-free PVC material similar to the well riser. The screens will be non-contaminating, factory-constructed, continuous wrap or mill-slot design, with a slot size of 0.010 inch to minimize the volume of silt and sand entering the well. This slot size is compatible with the results of the sieve analysis of existing wells shown in Appendix C of the RI Report (ref. 8). The mean grain size for the samples from the Fluvial Aquifer ranged from 0.0075 to 0.11 inches, with most samples in the range of 0.012 to 0.032 inches. Most of the wells had a coefficient of uniformity less than 3 and a curvature of less than 2. The screens in the existing wells are also of the same slot size. The wells have functioned satisfactorily. A 20/40 filter pack will be used in the well installations. This screen and filter pack combination will minimize the sediment entering the well, while allowing adequate flow for rapid purging and sampling of the monitor wells. To

confirm the compatibility between the screen and the aquifer material, sieve analysis will be performed on at least one representative sample of the aquifer in which the screen is placed. The sieve analysis will be conducted in accordance with ASTM-C 117 and C 136. The results will be submitted in the field boring logs.

Screen Location. Wells will be constructed so that base of the screen is near the top of the confining unit between the Fluvial and Memphis Sand aquifers. The proposed screen length is 10 feet. The placement of well screens near the base of the Fluvial Aquifer is consistent with the nature of the contaminants of concern. Floating constituents have not been encountered and are not expected during this project. The potential contaminants of concern include solvents such as 1,1,2,2-Tetrachloroethane; 1,1,2-Trichloroethane; 1,1-Dichloroethene; carbon tetrachloride; and trichloroethene, as well as metals such as arsenic, barium, lead, chromium, and nickel. None of these substances occur or are expected to occur as a floating product or dense layers within the aquifer.

Joining Screen and Riser. Screen and riser sections will be joined by threaded, flush-joint couplings to form watertight unions that retain 100 percent of the strength of the screen. Solvent glue will not be used at any time in construction of the wells. The bottom of the deepest screen or casing section will be sealed with a threaded cap or plug of inert, non-corroding material similar in composition to the screen.

Well Plumbness and Alignment. All risers and screens will be set plumb and true to line. The monitoring well screen and riser pipe will be held in the center of the hole by the augers during the installation of the annular materials. Centralizers will be used where necessary to calculate plumbness and alignment of the wells (generally for wells that exceed 80 ft in depth). It can be assumed that centralizers will be used for wells in the Memphis Sand Aquifer. Centralizers will not be attached to the well screen. The lowest centralizer attachment will be a minimum of 10 ft above the top of the well screen.

Filter Pack. Silica sand will be used as the filter pack material. Only clean, inert silica sand of 20/40 or similar gradation will be used to construct a uniform and continuous filter pack. This filter pack is slightly finer than would be typically used in material with the reported grain size distribution of the Fluvial Aquifer. However, this difference will not alter the well efficiency and will provide an effective connection with the aquifer. The pack will be designed to prevent migration of fines into the screen. The existing wells are constructed of similar-sized material. The filter pack will be placed by tremie pipe from the base of the boring to approximately 2 ft above the well screen. If the boring penetrates the confining layer, bentonite will be used to backfill the portion of the confining layer penetrated by the auger.

Bentonite Seal and Grout. A minimum 2-foot bentonite pellet seal will be placed into the annular space between the riser and the boring wall at the top of the filter pack. The bentonite will be tremied in place to prevent "bridging." A bentonite grout mixture, consisting of a coarse-grained, high solids bentonite grout of at least 20 percent solids pure bentonite (Baroid Benseal, American Colloid, Volclay, or equal), will be placed

from the top of the bentonite seal to within 2 feet of ground surface. The grout will contain a minimum of 20 percent solids and be mixed in the field with clear water in accordance with manufacturer's specifications. The upper 2 feet of the annulus will be filled with cement grout, as shown in Figures 5-1 and 5-2.

Soil Sampling for Geotechnical Analysis. During drilling, soil samples will be collected and geotechnical analysis will be performed as outlined below:

- Soil samples will be taken continuously for the first 10 ft, and then at 5-foot intervals thereafter.
- Sampling will be done with a split-spoon sampler (ASTM-D 1586-67) or thin wall sampler (ASTM-D 1587-74) using standard sampling techniques.
- Samples will be stored in labeled, air-tight plastic or glass containers until such time as they are needed for testing or the contract is complete.
- All soil samples will be visually classified by the Unified Soil Classification System. The field classification will be verified by laboratory analyses consisting of the following:
 - Shelby tube samples will be collected from specific wells and borings identified in the OU-specific FSPs. These samples will be collected and tested using Standard Triaxial Permeability methods developed by the COE (Engineering Manual 1110-2-1906, 1986) (ref. 39) to determine if the confining unit is capable of allowing contaminants to migrate to the lower aquifer:
 - a. Grain-size distribution (ASTM-D 421 and 424)
 - b. Atterberg limits (ASTM-D 423 and 424)
 - c. Moisture content (ASTM-D 2216)
 - d. Triaxial permeability (EM 1110-2-1906, 1986)
 - Specific depths for samples to be tested will be determined by the field geologist after reviewing the boring logs.

Protection of Well and Surface Completion. Precautions will be taken to prevent tampering with monitoring wells or the entrance of foreign material into the well. Upon the completion of each well, a vented cap will be installed to prevent material from entering the well. A protective steel casing will be placed around the well riser. The steel casing will be equipped with a cap and lock and will be between 24 inches and 36 inches above ground level. It will be taller than the enclosed well. Depending on the location (offsite versus onsite), wells may be set in a protective casing much closer to the ground (flush-mounted) to reduce the attraction for vandalism. At a minimum, a 3-foot-square, 4-inch-thick concrete pad will be constructed around the protective casing at

ground level and sloped away from the well. The portion of the pad around the well will be set a minimum of 3 inches in the ground. Three, 2-inch or larger diameter steel posts will be equally spaced around the protective casing and embedded in the concrete pad. There will be no openings in the protective casing wall below its top. The top of the well riser, as opposed to the well casings, will be notched on the north side, which will be the point where the elevation is established. The elevation will be to the closest 0.01 foot. All outside casing will be permanently identified with the well number. A survey marker will be permanently placed in each pad. Each survey marker will be stamped with the identifying number according to the directions of the survey section in this QAPP. Protective casings and steel posts will be primed and painted with two coats of traffic yellow paint.

Temporary Capping. Any well that is to be temporarily removed from service, or left incomplete because of delay in construction, will be capped with a watertight cap and equipped with a vandal-proof cover.

5.4.2.6 Field Logs

The field geologist or geotechnical engineer will maintain suitable field logs detailing drilling and well construction activities. One copy of each field log, including the required color slides, will be submitted to the Contracting Officer not longer than 10 calendar days after each well is completed. Information provided in the logs will include the following, as a minimum:

- Reference point for all depth measurements
- Depth of each change of stratum
- Thickness of each stratum
- Identification of the material of which each stratum is composed according to the Unified Soil Classification System, or standard nomenclature, as necessary
- Depth interval from which each formation sample was taken, and condition of sample (such as wet or dry)
- Depth at which hole diameter (bit sizes) change
- Depth at which groundwater is first encountered
- Depth to the static water level
- Total depth of completed well
- Depth or location of loss of drilling fluids (if used)

- Location of any fractures, joints, faults, cavities, or weathered zones
- Depth and thickness of grouting or sealing
- Nominal hole diameters
- Amount of cement used for grouting or sealing
- Depth and type of well casing
- Description (to include length, location, diameter, slot sizes, material, and manufacturer) of well screen(s)
- Any sealing-off of water-bearing strata
- Static water level upon completion of the well and after well development
- Drilling date or dates
- Construction details of monitoring well
- Well development notes

Final Logs. Photocopies of the original field logs will be included in an Appendix of the final report. Additionally, the field logs will be edited (for spelling and grammar) and drafted for inclusion into the final report.

5.4.2.7 Well Development

After each well has been constructed, but no sooner than 48 hours after grouting is completed, the well will be developed by pumping or surging, without the use of acids, dispersing agents, or explosives. Development will continue for a minimum of 4 hours or until groundwater removed from the well is clear and free of sand and drilling fluids, and parameters (such as pH, temperature, and conductivity) are stabilized to less than 5 percent fluctuation between three successive readings. Other than formation water from the particular well, no other liquid will be introduced into the well. After final development of the well, approximately 1 liter of water will be collected (from the well) in a clear glass jar and photographed in front of a standard color chart with 35-mm color slide film. The jar will be shaken immediately before being photographed to display any suspended solids. The photograph will have enough close-up lighting to show the clarity or turbidity of the water. The slides will be submitted as part of the well log.

5.4.2.8 In-Situ Permeabilities

The hydraulic conductivity of the water-bearing zone in which each monitoring well is screened will be estimated using a rising head pneumatic slug test method. This slug test method will allow testing to be performed quickly, and nearly instantaneous removal of the pneumatic slug will eliminate much of the noise in the very-early-time data that is often present in manual slug test methods in transmissive aquifers.

5.4.2.9 Decontamination Procedures

A stringent decontamination and inspection program will be followed to prevent the introduction of any contaminants into the subsurface during drilling. A decontamination area for the cleaning of drilling equipment will be set up away from the drill site. After cleaning and decontaminating, all drilling equipment and sampling tools will remain off the ground on metal racks, metal sawhorses, or plastic sheeting until ready for use.

Drill Rig and Tools. All the drilling rigs and drilling equipment will be steam cleaned in the designated cleaning/decontamination area before entering the drill site. In addition, all downhole drilling, sampling, and associated equipment will be cleaned and decontaminated by the following procedure:

- Steam clean using a steam cleaner capable of generating a pressure of at least 2,500 pounds per square inch (psi) and producing a steam of at least 20°F. All equipment that is hollow or that has holes to transmit water or drilling fluids will be cleaned inside and outside.
- Rinse with potable tap water.
- Rinse with de-ionized water from a stainless steel container.
- Rinse with pesticide grade isopropanol from a stainless steel container.
- Air dry.
- Wrap with aluminum foil, if appropriate, to prevent contamination if equipment is going to be stored or transported.

All cleaning and decontamination will be conducted in a designated area lined with heavy-duty plastic. A catch basin will be used or constructed to contain all runoff until it can be placed into containers. The cleaning of drilling equipment (drill pipe, auger, and tools) will be conducted above the plastic sheeting on saw horses or other appropriate means.

All of the drilling equipment, including the drill rig, will be inspected before entering the site to monitor whether there are fluids leaking and whether all gaskets and seals are

intact. No oil or grease will be used to lubricate drill stem threads or any other drilling equipment being used over the borehole or in the borehole without prior approval.

Soil and Sediment Sampling Equipment Decontamination. All the soil and sediment sampling equipment not associated with the drill rig and drilling will be decontaminated by personnel wearing disposable latex gloves or vinyl gloves and using the following procedure:

- Wash with tap water and laboratory grade, non-phosphate detergent, using a brush if necessary to remove particulate matter and surface films.
- Rinse with tap water.
- Rinse with de-ionized water.
- Rinse twice with pesticide grade isopropanol.
- Rinse with organic-free water (not deionized or distilled water).
- Air dry.
- Wrap with aluminum foil, if appropriate, to prevent contamination if equipment is going to be stored or transported.
- Water used in decontamination operations will be disposed of as is purge water.

Surface Water Sampling Equipment Decontamination. All of the surface water sampling equipment will be decontaminated by personnel wearing disposable latex gloves or vinyl gloves and using the following procedure:

- Wash with tap water and laboratory grade, non-phosphate detergent, using a brush if necessary to remove particulate matter and surface films.
- Rinse with tap water.
- Rinse with de-ionized water.
- Rinse twice with pesticide grade isopropanol.
- Rinse with organic-free water (not deionized or distilled water).
- Air dry.
- Wrap with aluminum foil, if appropriate, to prevent contamination if equipment is going to be stored or transported.

• Water used in decontamination operations will be disposed of as is purge water.

Groundwater Sampling Equipment Decontamination. With the following exceptions, all groundwater sampling will be conducted with disposable sampling equipment (such as disposable bailers and disposable rope) that requires no decontamination.

Elevation tapes will be decontaminated using the following procedure:

- Wash with tap water and laboratory grade, non-phosphate detergent, using a brush if necessary to remove particulate matter and surface films.
- Rinse with tap water.
- Rinse with de-ionized water.
- Air dry.
- Wrap with aluminum foil or seal in a plastic bag.

Submersible pumps and hoses used to purge groundwater wells will be decontaminated using the following procedures:

- Flush the hose using laboratory grade, non-phosphate detergent, followed by scrubbing the exterior of the hose with a brush.
- Rinse the exterior of the hose with tap water followed by pumping tap water through the hose.
- Rinse the exterior of the hose and pump with de-ionized water.
- Place equipment in a polyethylene bag to prevent contamination.

5.5 Geophysical Survey and Logging

5.5.1 Natural Gamma Logs

Although MW-36 and MW-37 are double cased, there is a concern that they may represent a pathway for migration of potentially contaminated water. Either a dual density (gamma-gamma) or an acoustic velocity log will be conducted in the two wells currently screened in the Memphis Sand Aquifer (MW-36 and MW-37) to measure the density of the grout, to determine the location of the filter pack relative to the confining unit (the filter pack will have a lower density than the bentonite seal), and to determine if the grout is effectively sealing the upper aquifer from the lower aquifer.

Gamma-gamma and acoustic velocity are the only geophysical methods available to determine the soundness of the grout inside a small borehole with a 2-inch-diameter well casing. Because of the accuracy and the lack of a nuclear source, the acoustical method is the preferred method. However, because the probe used in the acoustical method has a diameter of 1 1/16 of an inch, the well casing must be perfectly round and free of any interior abnormalities (such as scaling or ridges). If interior abnormalities are encountered, the gamma-gamma method will have to be employed.

Geophysical logging service companies must maintain licenses from the Nuclear Regulatory Commission (NRC) to operate and transport a nuclear source. Part of their license requirements includes preparing a company health and safety plan. This plan includes safe handling training for their employees, quarterly testing of their equipment, and training regarding safe shipment of the sources. Part of the employee training includes provisions that do not allow untrained personnel to operate or be near a source when it is onsite. When implementing the health and safety plan, the area where the source is used is roped off and untrained personnel are not allowed within that exclusion zone. The service company's health and safety plan will be followed when that company is onsite, as described in Section 10 of DDMT's HASP.

In addition to the precautions that service companies take to maintain their license, they are subject to an audit from the NRC (or from the agreement state that implements the NRC rules) while they are onsite.

Natural gamma logging will be performed on six existing wells to help identify the depth to the Jackson/Claiborne confining unit. Because the existing monitoring wells are constructed with 2-inch-diameter PVC, natural gamma logging is the only applicable logging method. Other viable alternatives require a larger diameter casing. These logs will be prepared by lowering a natural gamma radiation detector into the well or borehole and recording the amount of naturally occurring gamma radiation present as a function of depth. Clay minerals commonly contain the isotope potassium-40, which is typically the source of gamma radiation. Natural gamma logs will be used in determining the proportion of clay present and the depth to formation interfaces.

The six existing wells to be logged are the two wells into the Memphis Sand Aquifer (MW-36 and 37) and four Fluvial Aquifer wells (MW-19, 34, 38, and 39) in the north-central area of DDMT in the vicinity of the depression into the confining unit (see the Generic RI/FS WP, ref. 38), for a discussion of this depression). The two Memphis Sand wells will provide a clear profile of the natural gamma characteristics of the confining unit. The four Fluvial Aquifer wells may provide added information on clay formations in the vicinity of the confining unit. New wells will be logged on a case-by-case basis. The logging of the well will be conducted by qualified personnel. All the necessary equipment, personnel, and safety procedures will be provided by the selected contractor. A copy of the log, along with a letter report indicating the findings, will be submitted as an appendix to the RI report.

5.5.2 Electromagnetic and Magnetic Surveys

Electromagnetic and magnetic surveys were performed in Dunn Field in the vicinity of known burial sites. The survey was performed in June 1993 by the Corps of Engineers Waterways Experiment Station (CEWES). The purpose was to confirm locations of buried pits and trenches that might be burial sites of hazardous and toxic waste that could be contributing to groundwater contamination in Dunn Field. The results of the investigation are being analyzed and will be included as an appendix to the RI/FS report. Magnetometers will be used before drilling to clear drill sites of any buried metal and utilities.

5.6 Surveying

5.6.1 Control Monuments

Control monuments, monitoring wells, and soil and stratigraphic borings will be surveyed for their locations and elevations by a State of Tennessee certified land surveyor. Permanent survey markers will be installed at each control monument and monitoring well. Documentation, tabulation, and mapping of the final coordinates and elevations will be submitted in the RI Report appendixes.

Three permanent control monuments with a 3½-inch-diameter domed, brass, bronze, or aluminum alloy cap will be set in accessible locations within or immediately adjacent to the project area. These monuments will be set no closer than 500 ft to each other. Coordinates (1:10,000) and elevations (1:5,000) to Third Order accuracies or better will be established to the closest 0.01 foot for each monument. The coordinates will be referenced to the State Plane Coordinate System, and the elevations will be referenced to the 1929 North American Vertical Datum. Each survey marker and monument will be stamped with the following data by using steel dies that are a minimum of 1/8 inch tall: COE, Huntsville, Alabama Identification Number Month and Year Established.

5.6.2 Location Surveys

Coordinates and elevations will be established for each of the following items: all new monitoring wells, stratigraphic test borings, and the corners of the geophysical survey area. The coordinates will be to the closest 1.0 foot and referenced to the State Plane Coordinate System. The elevation will be determined for both the top of the well casing (at the water-level measuring point) and the top of the survey marker. All elevations will be referenced to the North American Vertical Datum of 1929. A 3½-inch-diameter domed brass, bronze, or aluminum alloy cap will be permanently set in the concrete pad surrounding each well. The marker will be stamped as indicated above. In addition to the coordinates, the elevations to the closest 0.01 foot will be provided for the survey marker and top of casing for the pump test well, the piezometers, and all new monitoring wells.

5.6.3 Documentation

A tabulated list of the coordinates and elevations for the corners of the geophysical survey, stratigraphic test borings, monitoring wells, and control monuments will be prepared and submitted. The tabulation will consist of the designated name or number of the corner, boring, well, or monument; the X and Y coordinates; and all of the required elevations. Elevations will be determined for both the top of casing and the top of the survey monument at each monitoring well. This information will be used to generate a map plotted at a scale of 1 inch = 300 ft or larger showing the location, identification, coordinates, and elevations of the geophysical survey, soil borings, wells, and monuments. The tabulated list of coordinates and the map will be submitted, along with all field books and computation sheets, no later than when the Draft RI Report for this project is submitted.

6.0 Calibration Procedures

6.1 Field Instruments

Field instruments will be calibrated daily before beginning sampling activities. Standards used to calibrate the field survey instruments will be traceable to NIST Standards. The method and frequency of calibration for the instruments used for each field activity are described in this section.

6.1.1 HNu Calibration

The meter will be calibrated according to manufacturer's instructions. The manufacturer will be contacted regarding recommendations for the most appropriate calibration procedure to be used for the contaminants of interest. General instructions are included in the HASP. On a daily basis, the meter will be calibrated to isobutylene. The HNu will be zeroed to background levels each hour and at each new location. Calibration records will be kept in the field log book by field personnel.

6.1.2 Organic Vapor Analyzer Calibration

The primary calibration of the OVA is performed at the factory to 100 parts per million (ppm) methane gas. Secondary calibration will be performed according to manufacturer's specifications at the beginning of each sampling activity. Those specifications are included in the HASP. In addition, the manufacturer will be contacted regarding recommendations for the most appropriate calibration procedure to be used for the contaminants of interest. The meter will be zeroed to background levels on a daily basis by field personnel.

6.1.3 Soil Boring Drilling

While drilling either borings or wells, an OVA or an HNu will be used to screen the soil samples and to monitor the ambient air. The calibration procedures outlined in Section 6.1.1 will be followed during the soil boring activities.

6.1.4 Groundwater Sampling

Several instruments will be used during the collection of groundwater samples. Initial monitoring of the ambient air for volatile organic vapors around the wellhead will be performed using an HNu meter. The meter will be calibrated to isobutylene each day and will be zeroed to ambient air at each well location before opening the well. During well evacuation, pH and specific conductance will be measured. The meters will be calibrated in the field before use at each well, following manufacturer's specifications. The calibration procedures are described below and will be carried out by field personnel.

6.1.5 pH Meter Calibration

The pH meters will be calibrated against two sets of standard pH solutions, either 4.0 standard units (SU) and 7.0 SU or 7.0 SU and 10.0 SU, depending on whether previous pH measurements have been less than or greater than 7.0 SU, respectively. Both the Cole-Parmer and Beckman meters automatically recognize pH standards and adjust the span and offset readings accordingly. Both pH meters also measure and display temperatures and automatically compensate pH readings accordingly. At the end of calibration, the meter readings will be adjusted and the probe will be rinsed thoroughly with distilled water.

6.1.6 Specific Conductivity Meter Calibration

The specific conductivity meters will be standardized by immersing the decontaminated conductivity probe into a standard solution of conductivity buffer. The conductivity of the standard solution will be within the same order of magnitude as the water sample. The meter reading will be manually adjusted to the buffer solution value. The Markson conductivity meter is automatically temperature-compensated to 20°C, while the Hanna meter requires manual adjustment of a temperature compensation knob. After calibrating, the probe will be triple rinsed with distilled water.

The pH and conductivity meters will be decontaminated before use at each well. The probes will be rinsed three times with distilled water before storage each day. The meters will be checked for battery charge and physical damage each day. The meters, pH standard solutions, and conductivity buffers will be stored in a cool, dry environment. Standard solutions will be discarded on their expiration dates.

6.2 Laboratory Equipment

The contracted laboratory will provide the project chemist and QA supervisor with a copy of the appropriate Comprehensive Quality Assurance Manual (CompQAM) for review and approval. The Laboratory CompQAM will outline in detail procedures for instrument calibration control.

Section 7.0 Analytical Procedures

Samples will be analyzed using EPA-approved methods. Before the field effort begins, the analytical laboratory will provide the lead chemist with a copy of its CompQAM for review and approval.

7.1 Data Packages

Level 1 and 2 data package deliverables were detailed in Section 3.2.2. Level 3 data package deliverables are summarized in Table 7-1. Level 4 deliverables are the same as Level 3 with the addition of all the unreduced experimental data.

7.2 Reporting Limits

Method target compound lists and reporting limits are summarized in Table 7-2. Because of the use of similar analytical techniques for Levels 2 and 3, the target reporting limits presented in Table 7-2 are applicable for both data quality levels.

7.3 Special Analyses

The reporting limits are based on the Contract Laboratory Program Contract Required Detection Limits, which are equal to PQLs for this project.

Ten VOC compounds, three SVOC compounds, and one pesticide have MCLs lower than the standard reporting limits for the analytical methods chosen, as summarized in Table 7-3. Groundwater samples from areas not affected by site activities will initially be analyzed using the normal VOC and SVOC methods (CLP). However, sample locations that meet both of the following criteria may be resampled and reanalyzed using the low-level method presented below:

- None of the method target compounds can be present in concentrations greater than 25 μ g/L (upper linear calibration range for the CLP).
- At least one of the target compounds was detected above its MCL but below the method reporting limit.

Also, for compounds where the CLP reporting limits do not meet the MCL or other preliminary remediation goal, the intent is to reanalyze the sample using a method with lower detection limits, if feasible. The decision to reanalyze samples using lower detection limits will be made on a case-by-case basis.

Table 7-1 Level 3 Data Package Deliverables Defense Depot Memphis, Tennessee Page 1 of 2				
GI D				
CLP Form	Purpose			
Organic Compounds by GC/MS				
1	Data summary form			
2	Surrogate spike recovery			
3	MS/MSD recovery			
4	Method blank summary			
5	Instrument performance check summary			
6	Initial calibration data			
7	Continuing calibration check			
8	Internal standard area and retention time summary			
Organic Co	mpounds by GC (Pesticides, PCBs, Herbicides)			
1	Data summary form			
2	Surrogate spike recovery			
3	MS/MSD recovery			
4	Method blank summary			
6D	Initial calibration retention time summary			
7E	Continuing calibration summary			
8C	Analytical sequence—evaluation of retention time shift for the internal standard			
10	Compound identification summary			
Inorganic C	ompounds			
1	Data summary form			
2	Initial and continuing calibration verification			
3	Blanks			
4	ICP Interference check samples			

Table 7-1 Level 3 Data Package Deliverables Defense Depot Memphis, Tennessee			
	Page 2 of 2		
CLP Form	Purpose		
5A	Spike sample recovery		
5B	Post-spike sample recovery		
6	Duplicates		
7	Laboratory control sample		
8	Method of standard addition results		
9	ICP serial dilution results		
10	Instrument detection limit		
11A & B	ICP inter-element correction factors (annually)		
12	ICP linear ranges (quarterly)		
13	Preparation logs		
14	Analysis run logs		

Table 7-2 Target Compound Lists and Reporting Limits Defense Depot Memphis, Tennessee

		Page 1 of 7
Target Compound	Water (μg/L)	Soil (µg/kg)
Volatile Organic Compounds		
Chloromethane	10	10
Bromomethane	10	10
Vinyl chloride	10	10
Chloroethane	10	10
Methylene chloride	10	10
Acetone	10	10
Carbon disulfide	10	10
1,1-Dichloroethene	10	10
1,1-Dichloroethane	10	10
1,2-Dichloroethene (total)	10	10
Chloroform	10	10
1,2-Dichloroethane	10	10
2-Butanone	10	10
1,1,1-Trichloroethane	10	10
Carbon tetrachloride	10	10
Bromodichloromethane	10	10
1,2-Dichloropropane	10	10
cis-1,3-Dichloropropene	10	10
Trichloroethene	10	10
Dibromochloromethane	10	10
1,1,2-Trichloroethene	10	10
Benzene	10	10
trans-1,3-Dichloropropene	10	10
Bromoform	10	10
2-Hexanone	10	10
4-Methyl-2-pentanone	10	10

Table 7-2 Target Compound Lists and Reporting Limits Defense Depot Memphis, Tennessee				
		Page 2 of 7		
Target Compound	Water (µg/L)	Soil (µg/kg)		
Tetrachloroethene	10	10		
1,1,2,2-Tetrachloroethane	10	10		
Toluene	10	10		
Chlorobenzene	10	10		
Ethyl benzene	10	10		
Styrene	10	10		
Xylenes (total)	10	10		
Semivolatile Organic Compounds				
Phenol	10	330		
bis(2-Chloroethyl)ether	10	330		
2-Chlorophenol	10	330		
1,3-Dichlorobenzene	10	330		
1,4-Dichlorobenzene	10	330		
1,2-Dichlorobenzene	10	330		
2-Methylphenol	10	330		
2,2'-oxybis(1-Chloropropane)	10	330		
4-Methylphenol	10	330		
N-Nitroso-di-n-propylamine	10	330		
Hexachloroethane	10	330		
Nitrobenzene	10	330		
Isophorone	10	330		
2-Nitrophenol	10	330		
2,4-Dimethylphenol	10	330		
bis(2-Chloroethyoxy)methane	10	330		
2,4-Dichlorophenol	10	330		
1,2,4-Trichlorobenzene	10	330		

Table 7-2 Target Compound Lists and Reporting Limits Defense Depot Memphis, Tennessee

		Page 3 of 7
Target Compound	Water (μg/L)	Soil (µg/kg)
Naphthalene	10	330
4-Chloroaniline	10	330
Hexachlorobutadiene	10	330
4-Chloro-3-methylphenol	10	330
2-Methylnaphthalene	10	330
Hexachlorocyclopentadiene	10	330
2,4,6-Trichlorophenol	10	330
2,4,5-Trichlorophenol	25	830
2-Chloronaphthalene	10	330
2-Nitroaniline	25	830
Dimethylphthalate	10	330
Acenaphthylene	10	330
2,6-Dinitrotoluene	10	330
3-Nitroaniline	25	830
Acenaphthene	10	330
2,4-Dinitrophenol	25	830
4-Nitrophenol	25	830
Dibenzofuran	10	330
2,4-Dinitrotoluene	10	330
Diethylphthalate	10	330
4-Chlorophenyl-phenylether	10	330
Fluorene	10	330
4-Nitroaniline	25	830
4,6-dinitro-2-methylphenol	25	830
N-Nitrosodiphenylamine	10	330
4-Bromophenyl-phenylether	10	330
Hexachlorobenzene	10	330

Table 7-2 Target Compound Lists and Reporting Limits Defense Depot Memphis, Tennessee							
Page 4 of 7							
Target Compound	Water (µg/L)	Soil (µg/kg)					
Pentachlorophenol	5	165					
Phenanthrene	10	330					
Anthracene	10	330					
Carbazole	10	330					
Di-п-butylphthalate	10	330					
Fluoranthene	10	330					
Pyrene	10	330					
Butylbenzylphthalate	10	330					
3,3'-dichlorobenzidine	10	330					
Benzo(a)anthracene	10	330					
Chrysene	10	330					
bis(2-Ethylhexyl)phthalate	10	330					
Di-n-octylphthalate	10	330					
Benzo(b)fluoranthene	10	330					
Benzo(k)fluoranthene	10	330					
Benzo(a)pyrene	10	330					
Indeno(1,2,3-cd)pyrene	10	330					
Dibenz(a,h)anthracene	10	330					
Benzo(g,h,i)perylene	10	330					
Thiodyglycol	12.1	4200					
2,4-Dinitrotoluene	10	330					
Pesticides and PCBs	Pesticides and PCBs						
alpha-BHC	0.050	1.7					
beta-BHC	0.050	1.7					
delta-BHC	0.050	1.7					

Table 7-2 Target Compound Lists and Reporting Limits Defense Depot Memphis, Tennessee

	Page 5 of 7					
Target Compound	npound Water (µg/L) Soil (
gamma-BHC (Lindane)	0.050	1.7				
Heptachlor	0.050	1.7				
Aldrin	0.050	1.7				
Heptachlor epoxide	0.050	1.7				
Endosulfan I	0.050	1.7				
Dieldrin	0.10	3.3				
4,4'-DDE	0.10	3.3				
Endrin	0.10	3.3				
Endosulfan II	0.10	3.3				
4,4'-DDD	0.10	3.3				
Endosulfan sulfate	0.10	3.3				
4,4'-DDT	0.10	3.3				
Methoxychlor	0.50	3.3				
Endrin ketone	0.10					
Endrin aldehyde	0.10	3.3				
Toxaphene	5.0	170				
Aroclor-1016	1.0	33				
Aroclor-1221	2.0	67				
Aroclor-1232	1.0	33				
Aroclor-1242	1.0	33				
Aroclor-1248	1.0	33				
Aroclor-1254	1.0	33				
Aroclor-1260	1.0	33				
alpha-Chlordane	0.05	1.7				
gamma-Chlordane	0.05	1.7				

Table 7-2 Target Compound Lists and Reporting Limits Defense Depot Memphis, Tennessee						
	·	Page 6 of 7				
Target Compound	Water (μg/L)	Soil (µg/kg)				
Herbicides						
2,4-D	2.5	50				
Silvex (2,4,5-TP)	0.5	10				
2,4,5-T	0.5	10				
Dinoseb	0.5	10				
Dioxins and Furans						
Tetrachlorodibenzodioxins	0.005	0.005				
Pentachlorodibenzodioxins	0.005	0.005				
Hexachlorodibenzodioxins	0.005	0.005				
Tetrachlorodibenzofurans	0.005	0.005				
Pentachlorodibenzofurans	0.005	0.005				
Hexachlorodibenzofurans	0.005	0.005				
Metals						
Aluminum – ICP	200	40,000				
Antimony-ICP	60	12				
Arsenic-GFAA	10	2				
Barium – ICP	200	40,000				
Beryllium-ICP	5	1				
Cadmium-ICP	5	1				
Calcium – ICP	5,000	1,000,000				
Chromium-ICP	10	2				
Cobalt - ICP	50	10,000				
Copper-ICP	25	5				
Iron-ICP	100	20,000				
Lead-GFAA	3	0.6				
Magnesium – ICP	5,000	1,000,000				
Manganese – ICP	15	3,000				

Table 7-2 Target Compound Lists and Reporting Limits Defense Depot Memphis, Tennessee Page 7 of 7					
Target Compound	Water (μg/L)	Soil (µg/kg)			
Mercury-CVAA	0.2	0.1			
Nickel-ICP	40	8			
Potassium – ICP	5,000	1,000,000			
Selenium-GFAA	5	1			
Silver-ICP	10	2			
Sodium – ICP	5,000	1,000,000			
Thallium-GFAA	10	2			
Vanadium – ICP	5,000	1,000,000			
Zinc-ICP	20	4			

Table 7-3
Comparison of Organic Compounds with MCLs and Method Reporting Limits
Defense Depot Memphis, Tennessee

Target Compound	Analysis	MCL (μg/L)	Normal CLP Method Reporting Limit (µg/L)	Special Method Reporting Limit (µg/L)
Vinyl chloride	VOC	2	10	12
Methylene chloride	VOC	5	10	22
1,1-Dichloroethene	VOC	7	10	12
1,2-Dichloroethane	VOC	5	10	12
Carbon tetrachloride	VOC	5	10	12
1,2-Dichloropropane	VOC	5	10	1*
Trichloroethene	VOC	5	10	1*
1,1,2-Trichloroethene	VOC	5	10	1*
Benzene	VOC	5	10	12
Tetrachloroethane	VOC	5	10	12
Hexachlorobenzene	SVOC	1	10	0.2 ^b
Pentachlorophenol	SVOC	1	50	0.5°
bis (2-ethylhexyl)phthalate	SVOC	6	10	5
Aldrin	Pesticide	_	0.05	0.02 ^b

^{*}Low Level Contract Laboratory Program

^bMethod 8080

^{&#}x27;Method 8151

8.0 Data Quality Evaluation

8.1 Level 1-Field Survey Data

Field instruments used by CH2M HILL to collect temperature, pH, and conductivity are direct reading, thus making field calculations and subsequent data reduction unnecessary. All field data will be recorded in the site log books by appropriate trained field personnel. Field data will include the following:

- Instrument identification
- Calibration information (standards used and results)
- Date and time of calibration and sample measurement
- Sample results
- Supporting information (for example, temperature for pH reading)

If QC samples are used as part of the overall immunoassay tests, the results of these analyses also will be included in the field log. The FTL will provide a summary of the immunoassay results to the project chemist as well as to the FTL for review.

All data will be reviewed the FTL, who is responsible for the collection and verification of all field data while in the field. Data initially will be accepted or rejected by the FTL before leaving the sampling site. Extreme readings (readings that appear significantly different from other readings at the same site) will be accepted only after the instrument has been checked for malfunction and the readings verified by retesting. In addition, extreme or spurious readings will be recorded in the field log book, along with the rationale for accepting or rejecting the data.

Field documentation, sample data, instrument calibrations, and QC data will be reviewed by the PM (or a designee) before being included in the project files. QC checks will be reviewed by the project chemist, as well.

8.2 Level 2-Field Screening Data

The field screening laboratory will be required to provide a limited data package that includes instrument calibration, results for field samples, method blanks, and QC samples. This data package will be defined in detail in the subcontracting documents.

The project chemist will review the QC supporting information on a weekly basis and will provide a summary report to the PM at the end of the field effort. Areas of review will include the following:

- Instrument Calibration Correct frequency for initial and continuing calibration, initial calibration linear range, and continuing calibration within the method target acceptance limits
- Sample Results Results within the linear calibration range
- Laboratory Method Blanks—Potential for field sampling or laboratory contamination
- QC Sample Results—Replicate sample precision and spiked sample recovery (where applicable)
- Matrix Spike Results Will be used to evaluate the effect of the sample matrix on the overall analytical results, as well as to provide an estimate for analytical accuracy and precision.

In addition to the methods outlined above, samples will be submitted to the fixed-base analytical laboratory for Level 2 screening. The laboratory will use the same analytical approach as outlined in the EPA-approved method; however, for Level 2 the frequency of QC will be decreased and no supporting QA/QC documentation will be included in the data package deliverables. There will not be any changes in the method target compound lists and reporting limits. For example, samples will still be analyzed for the same list of VOCs; however, for Level 2 samples, fewer MS/MSD samples will be analyzed and only sample results and method blank results will be submitted for the data package deliverables.

8.3 Level 3-Laboratory Analyses

Data quality evaluation will be performed by the CH2M HILL project chemists. The data quality evaluation process is used to assess the effect of the overall analytical process on the usability of the data. The two major categories of data evaluation are laboratory performance and matrix interferences. Evaluation of laboratory performance is a check for compliance with the method requirements and is a straight-forward examination; either the laboratory did, or did not, analyze the samples within the limits of the analytical method. Evaluation of the matrix interferences is more subtle and involves examination of several results including surrogate spike recoveries, matrix spike recoveries, and duplicate sample results.

Level 3 data package deliverables are summarized in Table 7-1 and will be detailed in the laboratory subcontractor documents. Before the analytical results were released by the

laboratory, both the sample and QC data were carefully reviewed to verify sample identity, instrument calibration, detection limits, dilution factors, numerical computations, accuracy of transcriptions, and chemical interpretations. Additionally, the QC data were reduced and spike recoveries were included in control charts, and the resulting data were reviewed to ascertain whether they were within the laboratory defined limits for accuracy and precision. Any non-conforming data were discussed in the data package cover letter and case narrative. The laboratory will retain all the analytical and QC documentation associated with each data package. Such retained documentation need not be hard (paper) copy, but can be available on other storage media such as magnetic tape. However, the laboratory must be able to produce a hard copy of all the retained information upon request.

The data package will be reviewed by the project chemists using the process outlined in the EPA guidance document, Functional Guidelines for Evaluating Data Quality (EPA, 1991) (ref. 40). This overall process is used regardless of whether the samples were analyzed using CLP methods or not. The data review and validation process is independent of the laboratory's checks. It focuses on the usability of the data to support the project data interpretation and decision-making process. Areas of review include data package completeness, holding time compliance, initial and continuing calibration, spiked sample results, method blank results, and duplicate sample results. A data review worksheet will be completed for each data package. Acceptance criteria for each area of review are specified in the analytical method. For example, acceptance criteria for initial and continuing calibration are specified in each analytical method; any non-conformances will be noted on the data review worksheets and the effect of the non-conformance on the overall usability of the data will be evaluated as part of the overall data quality evaluation.

Samples that do not meet the acceptance limit criteria will be indicated with a qualifying flag, which is a one or two-letter abbreviation that indicates a problem with the data. Flags used in the text may include the following:

- U Undetected. Analyte was analyzed for but not detected above the detection limit.
- I Estimated. The analyte was present, but the reported value may not be accurate or precise.
- <u>UI</u> Reporting limit estimated. The analyte was not detected above the method detection limit, but the actual detection limit may be estimated.
- Rejected. The data were rejected because the corresponding QC data were not within the method-specified limits.

It is important to note that laboratory qualifying flags are included on the data summary forms (Form I) which are submitted to the project by the laboratory. However, during

the data review and validation process, the laboratory qualifying flags are evaluated and replaced with validation flags.

Once each of the data packages has been reviewed, and the data review worksheets completed, then the entire data set will be evaluated for overall trends in data quality and usability. Information summarized as part of the data quality evaluation may include chemical compound frequencies of detection, dilution factors that might affect data usability, and patterns of target compound distribution. The data set will also be evaluated to identify potential data limitation or uncertainties in the laboratory. Additional areas of review are discussed below.

8.3.1 Field and Laboratory Blank Contamination

Review includes the appearance and concentration of target compounds in field and laboratory blanks as well as of environmental samples. Common field sampling and laboratory contaminants detected in blank include acetone, methylene chloride, and phthalates. Acetone and methylene chloride are used to extract samples in the laboratory and hence are common laboratory contaminants. Phthalates are used as plasticizers, the most common of which is bis(2-ethylhexyl)phthalate, and are often introduced during sample handling.

According to the EPA Functional Guidelines, concentrations of these common contaminants detected in samples at less than 10 times the maximum concentration in the blanks can be attributed to field sampling and laboratory contamination rather than to environmental contamination from site activities. As a note, concentrations of common contaminants such as acetone, methylene chloride, and phthalates detected in both the sample and the corresponding blanks use the 10X rule. Concentrations of less common contaminants are multiplied by five rather than 10, as required by the EPA Functional Guidelines.

8.3.2 Surrogate Spike Recoveries

Surrogate spike recoveries are compounds for each of the organic analytical methods. For gas chromatograph/mass spectrometer (GC/MS) analyses, surrogate spike compounds are the structural homologs of target compounds, often with deuterium substituted for hydrogen, and are therefore are expected to behave in a similar manner during analysis. For GC analyses, surrogate spike compounds, are structurally similar (but not identical) to target compounds and again, should behave in a similar manner during analysis. Surrogate spike recoveries are used to monitor both laboratory performance and matrix interferences. Surrogate spike recoveries from field and laboratory blanks are used to evaluate laboratory performance because these blanks represent an ideal sample matrix. Surrogate spike recoveries for field samples are used to evaluate the potential for matrix interferences. When surrogate spike recoveries for field samples fall outside the method target acceptance windows, the samples are re-analyzed. If the surrogate spike recovery

is still outside the acceptance window for the re-analyzed sample, then the sample results are qualified as affected by matrix interferences.

8.3.3 Matrix Spike Recoveries

For this QC measure, three aliquots of a single sample are analyzed—one native and two spiked with the same concentration of matrix spike compounds. Unlike the surrogate spike compounds, matrix spike compounds are found on the method target compound list. Spike recovery is used to evaluate potential matrix interferences as well as accuracy. The duplicate spike results are compared to evaluate precision.

8.3.4 Duplicate Sample Results

Typically, one duplicate field sample will be collected for every 10 field samples. Both the native and duplicate samples are analyzed for the same parameters. Target compounds that are detected in both the native and duplicate samples can be compared and precision for the sample results calculated.

8.4 Level 4-Laboratory Analyses

Data quality evaluation of Level 4 data will be executed using the same process descirbed for Level 3 data; however, calculations for calibration, spike recovery, and sample results will be recreated using the raw data. These example calculations will be included with the data review worksheets.

8.5 Reconciliation with Data Quality Objectives

The final activity of the data quality evaluation is an assessment of whether the data meets the DQOs. The goal of this assessment is to demonstrate that a sufficient number of representative samples were collected and the resulting analytical data can be used to support the project decision-making process. The following precision, accuracy, representativeness, completeness, and comparability (PARCC) measures are used:

- Precision—is the agreement between duplicate results and can be estimated by comparing duplicate matrix spike recoveries and field duplicate sample results.
- Accuracy—is a measure of the agreement between an experimental
 determination and the true value of the parameter being measured. For
 organic analyses, each of the samples is spiked with a surrogate spike
 compound and for inorganic analyses, each sample was spiked with a
 known reference material before digestion. Each of these approaches
 provides a measure of the matrix effects on the analytical accuracy.

Accuracy can be estimated from the analytical data and cannot be measured directly.

- Representativeness—is a qualitative measure of the degree to which sample data accurately and precisely represent a characteristic environmental condition. Representativeness is a subjective parameter and is used to evaluate the efficacy of the sampling plan design. Representativeness is demonstrated by providing full descriptions of the sampling techniques and the rationale used for selecting sampling locations in the project scoping documents.
- Completeness—is defined as the percentage of measurements that are judged to be valid compared to the total number of measurements made. Typically, a goal of 95 percent usable data is desired.
- Comparability—is another qualitative measure designed to express the confidence with which one data set may be compared to another. The following factors affect comparability: sample collection and handling techniques, sample matrix type, and analytical method. Comparability is limited by the other PARCC parameters because data sets can be compared with confidence only when precision and accuracy are known. Data from one phase of an investigation to another can be compared when the same EPA-approved methods are used and data package deliverables are similar.

9.0 Performance and System Audits

Performance and systems will be audited to verify documentation and implementation of the project work plan, to identify any nonconformances, and to verify correction of identified deficiencies.

9.1 Assessments and Response Actions

Assessment activities may include surveillance, inspections, peer review, management system review, readiness review, technical systems audit, performance evaluation, and data quality assessment. The CH2M HILL project chemist or PM will be responsible for initiating audits, for selecting the audit team, and for overseeing audit implementation.

The project chemist or PM will evaluate the need for a performance audit independently, or by recommendation of the PM or the client. Performance audits are used to quantitatively assess the accuracy of analytical data through the use of performance evaluation and blind check samples. Laboratory performance will be audited by the PM, project chemist, or a designee.

The FTL is responsible for supervising and checking that samples are collected and handled in accordance with the approved project plans and that documentation of work is adequate and complete. The PM is responsible for seeing that project performance satisfies the QA/QC objectives. Reports and technical correspondence will be peer reviewed by an assigned qualified individual, otherwise external to the project, before being finalized.

9.2 Field Team Performance and System Audits

The FTL or a designated representative will conduct weekly informal audits of the field activities. The weekly audit for completeness will include the following items:

- Sample labels
- COC records
- Field notebooks
- Sampling operations
- Document control

The first three items above will be checked for completeness. Sampling operations will be reviewed to determine if they are performed as stated in the project-specific work plan, or as directed by the FTL. The informal document control audit will consist of checking each document for completeness, including such items as signatures, dates, and project numbers.

A systems audit of field operations may be required by the project-specific work plan and will be used to review the total data generation process, which includes onsite review of the field operational system, physical facilities for sampling, and equipment calibrations. A performance audit may be conducted by the PM and the FTL during the first week of sampling if it is deemed necessary by the PM, FTL, project chemist, or client. The audit may focus on verifying that proper procedures are followed so that subsequent sample data will be valid. Before the audit, a checklist will be prepared by the PM and the FTL, and will serve as a guide for the performance audit. The audit may verify the following:

- Collection of samples follows the available written procedures.
- COC procedures are followed for traceability of sample origin.
- Appropriate QC checks are being made in the field and documented in the field log book.
- Specified equipment is available, calibrated, and in proper working order.
- Sampling crews are adequately trained.
- Record-keeping procedures are being followed and appropriate documentation is maintained.
- Corrective action procedures are followed.

An audit report summarizing the results and corrections will be prepared and filed in the project files.

9.3 Laboratory Performance and Systems Audits

The analytical laboratory will conduct both internal and external QC checks. External QC checks include participation in EPA's certification and performance evaluation programs. The results of quarterly performance evaluation samples will be made available to the PM on request. Internal QC checks (duplicates, blanks, and spiked samples) will be performed in accordance with the approved methods.

Laboratory systems will be audited annually and as required by specific projects. Contracted laboratories are required to submit a laboratory QAPP and relevant SOPs before the field effort begins. If, during data evaluation and data use, any problems are noted, specific corrective actions will be implemented on a case-by-case basis. An additional systems audit may be requested by the CH2M HILL project chemist or PM, if warranted.

Depending on the project objectives, the laboratory may be required to perform the following:

- Monthly project review of 10 percent of all projects done by the QA department
- Audits performed by the laboratory QA manager at a frequency greater than specified in the lab CompQAM
- Special audits by the project chemist or corporate management when a problem is suspected

10.0 Preventive Maintenance

10.1 Field Instruments

All equipment used by CH2M HILL will be maintained in accordance with the manufacturer's instructions. Preventive maintenance activities for field equipment are listed in Table 10-1. Routine maintenance and all equipment repairs will be documented in the site log book. Whenever a piece of equipment fails to operate properly, the instrument either will be repaired in-house (if possible) or will be sent out for repairs and another instrument equivalent to the original substituted (if possible).

Table 10-1 Field Equipment Preventive Maintenance Defense Depot Memphis, Tennessee					
Instrument	Activity	Frequency			
pH meter	Battery replacement or electrode cleaning	As needed (indicated by LCD display) or as specified in instrument manual			
Conductivity Meter	Battery replacement or probe cleaning	As needed (indicated by LCD display) or as specified in instrument manual			

10.2 Analytical Laboratory Instruments

Preventive maintenance for laboratory instruments is discussed in detail in the laboratory CompQAM.

11.0 Calculation of Data Quality Indicators

11.1 Quality Control Measures

The QC measures described below are incorporated into Levels 2, 3, and 4 analytical methods.

Method Blanks—A method blank is a sample of analyte-free water that is treated as a sample in that it undergoes the same analytical process as the corresponding field samples. Method blanks are used to monitor laboratory performance and contamination introduced during the analytical procedure. Typically, one method blank is required per 10 or 20 samples (depending on the analytical method) or one per batch, whichever is more frequent.

Matrix Spikes—For inorganic analyses, a single sample is split and one portion is spiked with a known amount of reference material. For organic analyses, three aliquots of a single sample are analyzed—one native and two spiked with matrix spike compounds. Unlike the surrogate spike compounds, matrix spike compounds are found on the method TCL. Spike recovery is used to evaluate potential matrix interferences as well as accuracy. The duplicate spike results are compared to evaluate precision. The matrix spike compounds and method target acceptance ranges are summarized for each analytical method. Typically, one matrix spike (inorganic) or matrix spike/matrix spike duplicate (MS/MSD) sample (organic) is analyzed for every 20 samples of the same matrix.

Surrogate Spikes Recoveries—This QC measure is applicable only to organic analyses. Surrogate compounds are the structural homologs of target compounds, often with deuterium substituted for hydrogen, and are therefore expected to behave in a similar manner during the analysis. Surrogate spike recoveries were used to monitor both laboratory performance and matrix interferences. Surrogate spike recoveries from field and laboratory blanks were used to evaluate laboratory performance because the field blanks represent an "ideal" sample matrix. Surrogate spike recoveries for field samples were used to evaluate the potential for matrix interferences. For field samples, when the surrogate spike recoveries fall outside the method target acceptance windows, the samples are re-analyzed. If the surrogate spike is still outside the acceptance window for the re-analysis, then the sample results are qualified as affected by matrix interferences.

11.2 Formulas for Calculating Accuracy, Precision, and Completeness

Precision is a measure of the agreement or repeatability of a set of replicate results obtained from duplicate analyses made under the same conditions. Precision will be estimated from analytical data and cannot be measured directly. The precision of a

duplicate determination can be expressed as the relative percent difference (RPD), as calculated from the equation:

$$RPD\ IX_1 - X_2I/(X_1 + X_2)X200$$

where X₁ and X₂ are the duplicate values.

Accuracy is a measure of the agreement between an experimental determination and the true value of the parameter being measured. Accuracy is estimated through the use of known reference materials or matrix spikes. Accuracy is calculated from analytical data and is not measured directly. Spiking of reference materials into an actual sample matrix is the preferred technique because it provides a measure of the matrix effects on the analytical accuracy. Accuracy, defined as percent recovery (P), is calculated by the following equation:

$$P = (SSR - SR) / SA] \times 100$$

where SSR is the spiked sample result, SR is the sample result (native), and SA is the spike added.

Completeness is defined as the percentage of measurements judged to be valid compared to the total number of measurements made. Completeness is calculated using the formula:

12.0 Corrective Actions

12.1 Field Activities Corrective Actions

The PM is responsible for initiating corrective actions. Corrective action steps include problem identification, investigation responsibility assignment, investigation, action to eliminate the problem, increased monitoring of the effectiveness of the corrective action, and verification that the problem has been eliminated.

Documentation of the problem is important to the overall management of the study. A corrective action request form for problems associated with sample collection is completed by the person discovering the QA problem. This form identifies the problem, establishes possible causes, and designates the person responsible for action. The responsible person will be either the project manager or the FTL.

The correction action request form (Figure 12-1) includes a description of the corrective action planned and has space for follow-up. The PM verifies that the initial action has been taken and appears to be effective and, at an appropriate later date, checks to see if the problem has been resolved fully. The PM receives a copy of all corrective action request forms and enters them into the corrective action log. This permanent record aids the PM in follow-up and assists in resolving the QA problems.

Examples of corrective action include, but are not limit to, correcting COC forms, analysis reruns (if holding time criteria permit), recalibration with fresh standards, replacement of sources of blank contamination, or additional training in sampling and analysis. Additional approaches may include the following:

- Resampling and re-analyzing.
- Evaluating and amending sampling and analytical procedures.
- Accepting the data and acknowledging the level of uncertainty or inaccuracy by flagging the validated data and providing an explanation for the qualification.

12.2 Laboratory Activities Corrective Actions

The laboratory department supervisors review the data generated to verify that all QC samples have been run as specified in the protocol. Laboratory personnel are alerted that corrective actions may be necessary under the following conditions:

 QC data are outside the warning or acceptable windows for precision and accuracy established for laboratory samples.

Originator:	Date:
Person responsible for replying:	
Description of problem and when identified:	
Sequence of Corrective Action (CA): (Note, if submit this form directly to the project manager	no responsible person is identified,
State date, person, and action planned:	
	· · · · · · · · · · · · · · · · · · ·
CA initially approved by:	
Follow-up date:	
Final CA approval by:	Date:
Information copies to:	
Responsible Person:	
Field Team Leader:	
Project Manager:	

FIGURE 12-1
CORRECTIVE ACTION REQUEST FORM
Defense Depot Memphis, Tennessee



- Blanks contain contaminants at concentrations above the levels specified in the laboratory QAPP for any target compound.
- Undesirable trends are detected in matrix spike recoveries or RPD between matrix spike duplicates.
- There are unusual changes in detection limits.
- Deficiencies are detected by the laboratory QA director during internal or external audits, or from the results of performance evaluation samples.

If nonconformances appear in analytical methodologies, QC sample results are identified by the bench analyst, and corrective actions are implemented immediately. Corrective action procedures are handled initially at the bench level by the analyst, who reviews the preparation or extraction procedure for possible errors; and checks the instrument calibration, spike and calibration mixes, instrument sensitivity, and so forth. The analyst immediately notifies his/her supervisor of the problem that is identified and the investigation being made. If the problem persists or cannot be identified, the matter must be referred to the laboratory supervisor and QA/QC officer for further investigation. Once resolved, full documentation of the corrective action procedure must be filed with the laboratory supervisor, and the QA/QC officer must be provided with a corrective action memorandum for inclusion into the project file if data are affected.

Corrective actions may include, but are not limited to, the following:

- Re-analyzing suspect samples
- Resampling and analyzing new samples
- Evaluating and amending sampling and analytical procedures
- Accepting data with an acknowledged level of uncertainty
- Recalibrating analytical instruments
- Qualifying or rejecting the data

After the implementation of the required corrective action measures, data that is deemed unacceptable may not be accepted by the PM, and follow-up corrective actions may be explored. Details of laboratory corrective actions are provided in the laboratory CompQAM.

13.0 Quality Assurance Reports

The purpose of QA reports is to document implementation of the QAPP. These reports include periodic assessments of measurement data accuracy, precision, and completeness; the results of performance audits; the results of system audits; and identification of significant QA problems and recommended solutions.

The analytical laboratory will be responsible for submitting monthly progress reports to the client as requested.

The final QA report will be attached as an appendix to the project report and may include the following:

- Data quality assessment in terms of PARCC, and the method detection limits
- The degree to which DQOs were met
- Limitations of the measurement data; usability of the data
- Applicability of the data to site conditions
- Laboratory QC activities, including a summary of planned versus actual laboratory QC activities, explanations for deviations, and an evaluation of data quality for each analysis for each media
- Field QC activities, including a summary of planned versus actual field QC activities, explanations for deviations, and an evaluation of the data quality of field QC samples/activities and estimated effect on sample data
- Data presentation and evaluation, including an assessment of sampling and analysis techniques, data quality for each analysis and each media, and data usability

A final report will be submitted to the client after comments from the client and any regulatory agencies have been incorporated.

14.0 Sample and Database Management

14.1 General Information

The project database will be EDMS-A (environmental data management system in Access) and an environmental management information system (EMIS) deliverable will be submitted to the client. EMIS is similar to Interchange File Format (IFF) typically used by EPA, and the two formats are compared in Table 14-1. The few fields in IFF that do not correspond to an EMIS field include data that are not normally collected or are represented in EMIS in another field (LTHAN in Table 14-1 is represented in the flag qualifiers in EMIS).

The data management team consists of the PM, database manager, and data manager. The team will be responsible for the execution of the Data Management Plan. All documentation relating to the development and execution of the Data Management Plan will be kept in the project data management file, which will be stored in a central location accessible to all members of the data management team. The data manager will be responsible for maintenance of the data management file.

The data management file will consist of the following sections:

- Internal correspondence
- External correspondence
- Field correspondence
- Data management meeting notes
- Work plan information
- Project instructions
- Status reports
- E-Data documentation from lab
- Import description and exception reports
- Front-end QC description and exception reports
- Intermediate QC description and exception reports
- Back-End QC description and exception reports
- E-Data resubmittal requests
- Internal deliverable review comments
- External deliverable review comments
- Standard procedures

All electronic files associated with the project data management task will be kept on the network file server. Examples of these files are memos, plans, instructions, spreadsheets with station data, and the database itself. Backups of this data will be made according to that office's daily, system-wide backup routine.

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Parameters Defense Depot Memphis, Tennessee

Table 14-1

like lab and proj qualifiers SAMPLE_PREP - EXTRACT_METH SAMPLE_PREP - ANALYSIS_DATE SAMPLE_DATA - COLLECT_DATE SAMPLE_PREP - EXTRACT_DATE ANAL_RES - CONCENTRATION SAMPLE_PREP.LABSAMP_ID SAMPLE DATA - SAMPLE NO ANAL RES - VALCOMP - VVL ANAL RES - PARAM LABEL SAMPLE PREP - RECEIVED ANAL_RES - DATA_QUAL ANAL RES - ANAL METH SAMPLE_DATA - MATRIX ANAL_RES - UNIT_MEAS ANAL RES . LAB QUAL (1-16 SiteID) (17-21 Solid Wat Vigt ID) (22 Program Status Indicator - VVL) SAMP_LOC - LOC_ID SAMP_LOC - SITE_ID SAMPLE_PREP - SDG 500 ANAL_RES - DILUTE None None Repilcate number. Identifies results as which number replicate Extraction method used (SV, Pesticide/PCB etc.) Sample matrix (SOIL, WATER, AIR, OTHER) (ND) for non detects or blank for detects Analytical method used to find VALUE Name and organization of reviewer [XXXXXXX XXXX] Analytical result of chemical Unique field sample ID Project qualifier - VVL Unique lab sample ID Lab qualifier - VVL Parameter identifier Date recieved at lab Batch identifier Extraction date Collection date Dilution factor Analysis date Units [xxxxxxxxx] NYMMDD MAMMOD (AMMAY) [ATM:MDD] [XXXX] [A22] [A15] [A 15] [A12] [73] 3 ₹ [9Y] (¥0 **Ş** 3 3 ₹ PAKAMETER KEY LOCATION KEY REVIEWQUALIF CASE NUMBER WHO REVIEW SAMPLE KEY LABQUALIF PARAMID REPLNUM AMETHOD EMETHOD PILUTION MATRIX VALUE NYL) ADATE CDATE UNITS RDATE EDATE

mgm95-DDMT-WP2/028.xls

Table 14-1
Parameters
Defense Depot Memphis, Tennessee

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ANAL RES DETECT LIM		400	Noile	None		SAMPLE PREP - LAB ID		ANAL RES COMMENTS	
			DETECT 11MIT IXXXXXXX XXXXIIMethod detection limit	Signal Party Constitution of the Constitution	XXXXXXX XXXX Practical quantitication timit for the specifical minity;		Name of 1sb performing analysis		Additional information
A WHEL	[XXXXXXXXXX] Lab reporting limit		XXXX XXXXXXX			١	[\40]		(A80)
	REPLIMIT		DETECT 1 IMIT		POL		1 4 9		Comment

14.2 Hard Copy Data Management

Management of hard copy data packages is the responsibility of the data manager. As data packages are received, the data manager will enter the sample delivery group (SDG) number and date received in the database, and pass the data package to the data quality evaluation manager.

A cursory review of each hard copy data package will be performed by the data quality evaluation manager. Under the direction of the data quality evaluation manager, the data received will be compared to the COC to confirm that hard copies of all expected results are received. The SDG number for each analysis requested (for example, volatiles, semivolatiles, total metals, filtered metals, and dioxins) will be recorded in the Detailed Data Inventory Sheet (DDIS). Data packages will be prepared for data quality evaluation and filed in a central data storage area.

After all data packages are received, the DDIS will be reviewed for completeness by the data quality evaluation (DQE) team as part of the data quality evaluation process. The finalized DDIS will be included as part of the data quality evaluation technical memorandum delivered to the client.

14.3 Field Data Management

A sample tracking program (STP) will be used to manage data collected by the field team. STP is a subsystem of the EMIS implementation of the Microsoft Access-based Environmental Data Management System (EDMS/A-EMIS), developed to manage the flow of information from the field sampling team to the laboratory and to internal/external clients. STP is used for entry of field-originating information (such as station locations, lithologic descriptions, well completion information, sample collection dates/times, analyses requested, and field measurements), and to produce sample bottle labels, COC forms, electronic files containing COC information, and daily and weekly sampling summary reports.

STP will be updated by the database manager to include codes for EMIS-specific data reporting requirements (such as site location type, sample matrix, and analytical method) in accordance with the November 1994 EMIS Data Dictionary. Queries will be developed to aid the field team in calculating sample collection statistics and in verifying stations sampled and analyses requested against the work plan. All software modifications and support will be the responsibility of the database manager.

Before field mobilization, all STP modifications will be reviewed. All November 1994 EMIS Data Dictionary codes applicable to the project will be verified by data entry personnel. A data inventory table of all analytical methods to be requested and the corresponding analytes to be received from the laboratory will be verified by the data

manager and sent to the laboratory for verification. All sampling location information (such as well identification and site identification) will be verified against historically used location information by the data manager. If historical names are not available, location information will be provided by the client's data manager. A table of location information and the corresponding analyses to be requested will be sent to the client's data manager for independent verification.

Testing of STP modifications will consist of running STP through the normal daily routine performed in the field using an example data set that will be representative of planned field sampling activities. A daily sample summary report will be printed. Sample labels will be generated for all planned analytical combinations. Sample collection times will be entered and a COC will be printed. An electronic file containing COC information will be generated and sent via modem to the analytical laboratory for import into its data management system. Finally, an example weekly summary report will be produced and compared against the example data set.

The data manager will coordinate the implementation of STP during the field investigation during the mobilization period. Implementation will include the setup of all necessary computer hardware and software, setup of electronic communication systems, installation of the database, and STP usage training for the two-person sample management team. After the initial training, the data manager will provide support to the sample management team, as needed, for the duration of the field sampling event.

During the field sampling event, all station location, lithologic description, well completion, groundwater level, and sampling-related data will be entered by one field sample management team member and checked by the other team member against the original data forms (for example, purging forms, sampling forms, soil boring logs, and well completion logs) using the manual data entry verification procedure described below.

One of the sample management team members will be designated as the field data manager and will assume responsibility for setting up samples, generating labels, logging samples and generating COCs, generating electronic files containing COC information and transferring them via modem to the analytical laboratory, and entry of field-related information. The field data manager is also responsible for verifying that samples with QA Levels 3 and 4 collected on the same day will be shipped to the laboratory on separate COCs. The other sample management team member will be responsible for setting up sample coolers in the morning for the sampling teams to take out, checking in coolers after sample collection throughout the day, confirming that the sample preservation is adequate, shipping the sample coolers from the field to the laboratory, and verifying field-related information entered into the database against the hard copy. QA Level 2 (screening) samples and analyses will not be tracked by STP or reported in EMIS format.

The FTL will notify the data manager or database manager of any unusual occurrences relating to field sampling that affect the field or laboratory data that are to be processed by the data management team. Examples of unusual occurrences are assigned samples

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that were not collected, omission of field-generated data from the database, or breaking of sample bottles during transport to or processing at the laboratory. This information will be documented as appropriate in the database and the data management file under "Field Correspondence."

After log-in of the SDG from the field, the laboratory will acknowledge receipt of the samples by faxing the following items to both the field data manager and the DQE team:

- COC
- Exception Report—noting any problems with the sample shipment
- Sample Receipt Summary Report—containing data entered into the laboratory's database for each sample (including SDG, sample identification, location identification, analysis requested, data collected, and date received by laboratory)

The field data manager will use this information to verify all field-related information (sample identification, location identification, analysis requested, and date collected) at the laboratory, using the manual data entry verification procedure described in this section. The date received by the laboratory and the SDG number assigned by the laboratory to each sample will be entered into STP by the field sample management team from the Detailed Laboratory Summary Report.

The field data manager will generate a weekly sample status report. This report will be delivered to the FTL for review and delivery to the client. The field data manager will fax a copy of the finalized weekly sample status report to the data manager, who will add it to the data management file under "Status Reports."

Data from STP will be transmitted via modem or disk from the field team to the data manager on a weekly basis. The time and method of transmittal will be coordinated by the field data manager and the data manager. The data manager will check the STP data for correctness, completeness, and consistency. The data manager will alert the FTL of any errors or omissions contained in the STP data.

STP data will be contained in the STP file EDMSDATA.MDB and will be "imported" into the data management team copy of EDMS/A-EMIS by renaming the existing file in the appropriate EDMS subdirectory to EDMSDATA.MXX (where XX is the two-digit number of the field effort's week) and copying the new EDMSDATA.MDB file into that same directory. The goal is to have one EDMSDATA.MDB file for every week of the field effort, each containing data up to that week, with the most current file using the .MDB extension.

14.4 Management of Laboratory Electronic Data Deliverables

Electronic data (E-Data) deliverables will be sent as compressed (PKZIP 2.04) files to the data manager. A copy of the E-Mail cover letter, which includes a list of the file(s) transmitted and the date and time of transmittal, will be printed and stored in the data management file under "E-Data Documentation from Lab."

E-Data will be imported into EDMS/A-EMIS, using an EMIS-specific import program. The import program reads the data into EDMS/A-EMIS and performs a series of QC and data validation checks, based on the requirements specified in the November 1994 EMIS Data Dictionary. The checks and the rules they are based on are documented in the data management file under "Import Description and Exception Reports."

If the import program encounters any exceptions to the QC checks described above, the exception will be listed in the Import Exceptions Report. The Import Exceptions Report will contain the information necessary to identify the import file and line, and an explanation of the exception. Exceptions serious enough to jeopardize the integrity of the database will be reported as "ERRORS," and the offending line will not be imported. Less critical exceptions will be reported as "WARNINGS," and the offending line will be imported.

The data manager will evaluate each item in the Import Exceptions Report and determine what action, if any, needs to be taken. If the appropriate action is a manual data change to the laboratory-provided E-Data files by the data management team, the change will be verified and the laboratory will be notified of the change via E-Mail. If the appropriate action is to request a resubmission of the electronic data from the laboratory, the resubmission will be requested.

Once the appropriate action to be taken is completed, the action taken for each item in the Import Exceptions Report will be noted, initialed, and dated. Once all items listed on the Import Exceptions Report are resolved, the report will be added to the data management file under "Import Exceptions Reports."

During the data management process, manual changes may be made to the EDMS/A-EMIS database that create discrepancies with data stored in files at the laboratory. The data manager will notify the laboratory of the discrepancies so that laboratory records can be updated.

14.5 Front-end Data Content Verification

After the import of laboratory electronic data into the EDMS/A-EMIS database and resolution of all Import Exceptions, a series of queries will be performed to verify the content of and relationships between data. Content queries will confirm that all specific data codes used are correct as defined by the November 1994 EMIS Data Dictionary. Relationship queries will verify that relationships between certain data elements are correct and logical. For example, queries will verify that for a single sample, the Collection Date is an earlier date than the Analysis Date. The front end QC queries will be reviewed and modified as needed to check for valid values specific to this project.

If a database record does not satisfy the conditions specified by the query, the exception will be listed in the Front-End Exceptions Report. The Front-End Exceptions Report will contain the name of the query, the information necessary to identify the database record, and an explanation of the exception. The data manager will evaluate each item in the Front-End Exceptions Report and determine what action, if any, needs to be taken. If the appropriate action is a manual data change, it will be verified. If the appropriate action is to request a resubmission of the electronic data from the laboratory, the resubmission will be requested. If the action taken affects information received from the laboratory in its deliverables, the laboratory will be notified of the changes made via E-Mail.

Some items in the Front-End Exceptions Report may be acceptable. For example, the Front-End Exceptions Report may identify a matrix spike that is reported with a Sample Location ID of "FIELDQC." The Location ID of "FIELDQC" is only appropriate for equipment blanks, field blanks, and trip blanks; matrix spikes normally are not taken from blanks. Evaluation of the database record reveals that the matrix spike was taken by the laboratory to satisfy its own internal QC procedures, and that the parent sample from which the matrix spike was taken was an equipment blank. Therefore, the Sample Location of "FIELDQC" is acceptable.

Once the appropriate action to be taken is completed, the query will be re-run to confirm that the exception has been corrected, and the item in the Front-End Exceptions Report will be initialed and dated. If the item is acceptable, it will be noted as such and explained as necessary on the Front-End Exceptions Report, initialed, and dated. Once all items listed on the Front-End Exceptions Report are resolved, the report will be added to the data management file under "Front-End QC Descriptions and Exceptions Reports."

14.6 Data Quality Evaluation Flag Entry

The data manager is responsible for the entry of the data quality evaluation flags into the database after the completion of data quality evaluation by the DQE team. The DQE team will notify the data manager when the data quality evaluation is completed. Using data entry forms in EDMS/A-EMIS, laboratory qualifiers and/or concentration values changed on the Form I by the DQE team will be entered into the database in the

validation flag and/or concentration fields. If the laboratory qualifier and/or concentration values were not changed by the DQE team, no entry will be made in the validation flag and/or concentration fields. After the completion of data entry, the data manager will update the validation flag field as appropriate with data from the laboratory qualifier field for validation flag values that were not changed during the data quality evaluation process. This update will occur for all non-surrogate parameters associated with normal environmental samples, field duplicates, dilutions, or re-extractions. This update will not occur for surrogate parameters or for parameters associated with equipment blanks, trip blanks, field blanks, matrix spike/spike duplicates, inorganic laboratory replicates, or laboratory blanks.

After completion of the process described above, Replicate Form Is will be generated from the database and printed. The Replicate Form Is will be verified against the original validated (marked-up) Form Is using the manual data entry verification procedure. If errors are discovered, the error will be corrected in the database, and a new Replicate Form Is will be generated, printed, and verified against the original marked-up Form I. This process is repeated until no errors remain. When the verification process is completed, the Replicate Form Is will be filed with the original validated (marked-up) Form Is according to SDG number. An entry will be made in the history data table to document that the data quality evaluation flag field values have been entered and verified.

14.7 Intermediate Data Completeness Verification

After entry of the data quality evaluation flags, a series of queries will be performed to verify the content of, correctness of, and relationships between the data. This intermediate data completeness verification will consist of the complete set of front-end data content validation queries (with results evaluated and documented), and additional intermediate queries that will further evaluate the database. The intermediate QC queries will be reviewed and modified as needed to meet the requirements of this project.

Content and relationship queries involving the data quality evaluation flag field will be evaluated. For example, queries will be performed confirming that all the data quality evaluation flags are valid and that all analytical result records with a QA level other than "N" have non-null values in the data quality evaluation flag field. In addition, queries will be performed confirming that the one-to-many relationships between Sample Data, Sample Preparation Data, and Analytical Results are intact and correct. Queries will confirm that all Analytical Results records have associated Sample Preparation Data records, and that all Sample Preparation Data records have associated Sample Data records. Conversely, queries will confirm that no Sample Data records exist without associated Sample Preparation Data records, and that no Sample Preparation Data records exist without associated Analytical Results records.

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If a database record does not satisfy the conditions specified by the query, the exception will be listed in the Intermediate QC Exceptions Report. The Intermediate QC Exceptions Report will contain the name of the query, the information necessary to identify the database record, and an explanation of the exception. The data manager will evaluate each item in the Intermediate QC Exceptions Report and determine what action, if any, needs to be taken. If the appropriate action is a manual data change, it will be verified. If the appropriate action is to request a resubmission of the electronic data from the laboratory, the resubmission will be requested.

Once the appropriate action to be taken is completed, the query will be re-run to confirm that the exception has been corrected, and the item in the Intermediate QC Exceptions Report will be initialed and dated. If the item is acceptable, it will be noted as such and explained as necessary on the Intermediate Exceptions Report, initialed, and dated. Once all items listed on the Intermediate Exceptions Report are resolved, the report will be added to the data management file under "Intermediate QC Descriptions and Exceptions Reports." If the action taken affects data provided by the laboratory in its electronic deliverables, the laboratory will be notified via E-Mail of the changes made.

14.8 Generation of EMIS-like Access Tables

Two weeks before each deliverable deadline (draft/final), and provided that the necessary data are complete, the database manager will generate the EMIS-like Access tables. These tables follow the exact field name, count, type, length, and order of the EMIS tables deliverables. For the project, seven tables will be generated: SAMP_LOC, WELL_COMP, LITH_DES, SAMPLE_DATA, WATER_LEVEL, SAMPLE_PREP, and ANAL_RES. These tables are the source and final repository of the data for the draft and final deliverables.

The database manager will establish the structure of the tables manually in EDMS/A-EMIS, according to the EMIS November 1994 Data Dictionary specifications. The tables will be populated by running queries that pull the appropriate data from various EDMS/A-EMIS tables and place them in the corresponding fields in the EMIS-like Access tables. In addition to bringing in the data, the queries also format the data as necessary (for example, date as DD-MMM-YY, number of digits beyond the decimal point, and so forth).

Following the generation of the EMIS-like Access tables, a series of queries will be performed to verify the content of, correctness of, and relationships between the data. These queries, known as the back-end data content verification queries, will consist of appropriate front-end and intermediate data verification queries modified to analyze the EMIS template tables and their respective field names. The back-end QC queries will be reviewed and modified, if needed, to check for valid values specific to this project.

If a database record does not satisfy the conditions specified by a query, the discrepancy will be listed in the Back-End QC Exceptions Report. The Back-End QC Exceptions Report will contain the name of the query, the information necessary to identify the database record, and an explanation of the exception. The data manager will evaluate each item in the Back-End QC Exceptions Report and determine what action, if any, needs to be taken. If the appropriate action is a manual data change, it will be verified. If the appropriate action is to request a resubmission of the electronic data from the laboratory, the resubmission will be requested.

Once the appropriate action to be taken is completed, the query will be re-run to confirm that the exception has been corrected, and the item in the Back-End QC Exceptions Report will be initialed and dated. If the item is acceptable, it will be noted as such and explained as necessary on the Back-End QC Exceptions Report, initialed, and dated. Once all items listed on the Back-End QC Exceptions Report are resolved, the report will be added to the data management file under "Back-End QC Descriptions and Exceptions Reports."

Depending on the action taken to resolve items in the Back-End QC Exceptions Report, the EMIS-like Access tables may have to be regenerated and the process described above repeated. When all issues are resolved, generation of draft/final deliverables will proceed.

14.9 Generation of Deliverables

After completion of the EMIS-like Access table generation, the EMIS deliverables will be generated by the data manager. The source for these deliverables will be the EMIS-like tables in EDMS/A-EMIS. Microsoft Excel (v.5.0) will be the primary tool used to manipulate and format the data contained in the EMIS-like tables. Using Excel macros, data will be extracted directly from the EMIS-like tables in EDMS/A-EMIS. The data will then be inserted into Excel worksheets modeled after the EMIS Lotus 123 (v.2.2) templates provided by the client's data manager. The filled Excel worksheets are then saved as Lotus 123 spreadsheets. Once completed and reviewed, these Lotus 123 spreadsheets serve as the final deliverables.

The EMIS Lotus 123 templates have three purposes. First, the templates specify the column (field) order in which the data is to be organized. Second, they specify the field type for each field. Third, they help the client's data manager view the data.

Hard copies of the SAMP_LOC, WELL_COMP and LITH_DESC EMIS files will be generated and given to the site geologist for review using guidelines that will include a checklist of project-specific, acceptable entries and the November 1994 EMIS Data Dictionary. The site geologist will fill out a Review Comments Form that will be returned to the data manager along with the marked-up hard copy.

Hard copies of the WATER_LEVEL and SAMPLE_DATA EMIS files will be generated and given to the FTL for review using guidelines that will include a checklist of project-specific, acceptable entries from the November 1994 EMIS Data Dictionary. The FTL will fill out a Review Comments Form that will be returned to the data manager along with the marked-up hard copy.

The draft submission of SAMPLE_DATA to the client will include normal environmental and field duplicate samples only. The final submission of SAMPLE_DATA will contain all sample types.

Hard copies of at least three sets of SAMPLE PREP and ANAL RES records for each SAMPLE PREP fraction (volatiles, semivolatiles, pesticides, and so forth) will be generated and given to a representative of the DQE team for review using guidelines that will include a checklist of project-specific acceptable entries (previously agreed upon with the client data manager) and the November 1994 EMIS Data Dictionary. The reviewer will fill out a Review Comments Form that will be returned to the data manager along with the marked-up hard copy.

An electronic backup of the database will be made and stored as the current working version. After backup, the DQE team reviewer will be given access to the original electronic EDMS/A-EMIS database for electronic review of the EMIS template tables. The data management team will provide queries incorporating appropriate joins between the key fields of the EMIS template tables. Queries will be performed by the DQE reviewer using the guidelines described above. Comments will be noted on a Review Comments Form and returned to the data manager.

The data management team will determine what action, if any, is necessary to address the Review Comments for each EMIS deliverable. Actions taken will be noted on the Review Comments Form, initialed, and dated. The Review Comments Form and marked-up hard copies will be added to the data management file under "Internal Deliverable Review Comments." Depending on the nature of the comments and their resolution, the EMIS template tables may have to be regenerated and reviewed again.

If subsequent reviews are necessary, the data manager will return the marked-up hard copy, the Review Comments Form, and the corrected hard copy to the reviewer. The review process will continue until all exceptions identified in Review Comments Forms are resolved and verified.

After resolution of all internal review comments, the draft EMIS tables (Lotus 123 v.2.2 templates) will be placed on one or more 3.5-inch high density disk(s) (formatted using MS-DOS) with the files in a self-extracting compressed format (PKZIP 2.04). Each disk will be labeled with the following information:

- Name of Facility: DDMT
- Contractor Name:

- A. Executable File Name:
- EMIS File Name(s): EMIS_SL, EMIS_WC, EMIS_LD, EMIS_SD, EMIS WL, EMIS SP, EMIS AR1, EMIS_AR2...etc.
- Date of Submission:

A transmittal letter will accompany each data submission and will specify Contractor name, Contract number, Subcontractor point of contact, and a list of the files submitted. Additional explanation regarding the procedure for uncompression of the files will also be indicated. Unless directed otherwise, disk(s) containing draft and final EMIS files will be transmitted by the data manager via overnight delivery to the client's data manager.

The client's data manager should notify the PM immediately if any problems are encountered loading the draft EMIS electronic data deliverable into EMIS. This will allow the data management team to take any corrective actions needed and to include a corrected file(s) in the final EMIS electronic data deliverable.

The client's data manager will provide the PM with a hard copy of review comments. The data management team will determine what action, if any, is necessary to address the comments. Actions taken will be noted and explained to the extent necessary on the hard copy Comment Response Form, initialed, and dated. The client's data manager's Review Comments Form will be added to the data management file under "External Deliverable Review Comments." Depending on the nature of the comments and their resolution, the EMIS template tables may have to be regenerated and checked again.

After resolution of the client's data manager's comments, the final EMIS deliverables will be packaged and transmitted as described above for the draft deliverable. Copies of the final deliverables sent to the client will be archived by the data manager.

14.10 Postmortem

Any manual changes made to the electronic data by the client's data manager after the transmission of the final electronic deliverable will be documented as appropriate in the database and in the data management file to ensure that the data contained in the EDMS/A-EMIS database is identical to that in the client's database.

An archive of all the data on both file servers will be made to tape in a standard format (QIC-80, 8mm, etc) and stored with other project documentation, according to existing guidelines. The data will then be kept on both network file servers for 6 months. At the end of that period, a second archive will be made as described above and stored. At that time, unless the data is being actively used or modified, it will be removed from both network file servers.

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If any subsequent changes need to be made to the data, it will be restored from the latest tape, modified, archived as indicated above, and removed from the network file servers. Unless problems occur with data restoration, the primary source for non-database and database files will be the archives. All laboratory deliverables (either hard copy or electronic) will be retained by the laboratory for a period of 7 years.

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DDMT ACRONYMS

Acronym	Meaning/Explanation	
י2-C	LMG designation for non-CLP Pesticide standard mixture of single component pesticides and surrogat	
	components)	
BFB	Bromofluorobenzene	
CCB	Continuing Calibration Blank	
CCC	Calibration Check Compounds	
CCV	Continuing Calibration Verification	
CDA	Comma Delimited ASCII	
CLP	USEPA Contract Laboratory Program	
COC	Chain of Custody	
CRDL	Contract Required Detection Limit - defined in CLP SOW for Inorganics	
CRQL	Contract Required Quantitation Limit - defined in CLP SOW for Organics	
CVAA	Cold-Vapor Atomic Absorption	
% D	Percent Difference	
DEM	Degradation Evaluation Mixture (LMG designation for 8080 work), measures Endrin and 4,4'-DDT	
	degradation)	
DFTPP	Decafluorotriphenylphosphine	
EDL	Estimated Detection Limit	
EMIS	Environmental Management Information System	
GC	Gas Chromatography	
GC/MS	Gas Chromatography/Mass Spectrometry	
GFAA	Graphite Furnace Atomic Absoption	
ICB	Initial Calibration Blank	
ICP	Inductively Coupled Plasma	
ICSA/ICSAB	Interference Check Samples (ICP)	
ICV	Initial Calibration Venification	
CV	Initial Calibration Verfication	
IDI.	Instrument Detection Limit	
IEC	Inter-Element Correction Factor (ICP)	
INDA	Pesticide single component mixture A - compounds and concentration defined in CLP SOW	
	The 3 levels are named INDAL, INDAM, and INDAH (as specified in SOW)	
INDB	Pesticide single component mixture B - compounds and concentration defined in CLP SOW	
	The 3 levels are named INDBL, INDBM, and INDBH (as specified in SOW)	
IR .	Infrared Spectrophotometer	
IS	Internal standard	
LCS	Laboratory Control Sample	
LCSD	Laboratory Control Sample Duplicate	
LIMS	Laboratory Information Management System	
LMG	QAL Montgomery Lab	
MDL	Method Detection Limit	
MS/MSD	Matrix Spike and Matrix Spike Duplicate	
MSA	Method of Standard Addition	
PCB	Polychlorinated biphenyl	
PCB LOC	PCB Locator = mixture of aroctors 1221, 1248, and 1260 - which contain most PCB congener peaks. This	
	standard is used to provide all necessary peaks to identify aroclors in samples	
PEM	Performance Evaluation Mixture - compounds, concentrations, and criteria (degradation and RF) defined in	
	CLP SOW	
PIBLK	Pesticide/PCB instrument blank - CLP nomenclature	
% R	Percent Recovery	
RESC	Resolution Check Mixture - compounds, concentration, and criteria defined in CLP SOW	
F	Response Factor	
<u>:</u>	Lab Reporting Limit	

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DDMT ACRONYMS

Acronym	Meaning/Explanation
RPD	Relative Percent Difference
RRF	Relative Response Factor
RRT	Relative Retention Time
RSD	Relative Standard Deviation
RT	Retention Time
RT window	Retention Time window
SOP	Standard Operating Procedures
sow	CLP Statement of Work We are currently following OLM01.9 for Organics and ILM02.1 for Inorganics
TAL	Target Analyte List - as defined in Inorganic CLP SOW
TCL	Target Compound List - as defined in Organic CLP SOW
TEF	Toxicity Equivalent Factor
TIC	Tentatively Identified Compound

PROJECT: MEMPHIS DEFENSE DEPOT GENERAL CHEMISTRY

	LEVEL 2	LEVEL 3
NO PROCEDURAL CHANGES IN SAMPLE PREPARATION		
Instrument Calibration	1/day	l/day
Method Blank	I/batch of 20 or less Target Analyte < Reporting Limit (RL)	1/batch of 20 or less Target Analyte < Reporting Limit (RL)
Initial Calibration/ICV	I/day EPA Methods 90-100% CLP-Cyanide 85-115%	1/day EPA Methods 90-110% CLP-Cyanide. 85-115%
Continuing Calibration	Same as above	Same as above
MS/DUP	Recovery 80%-120% RPD <20%	Recovery 80%-120% RPD <20% TSS DUP Only
LCS	1/batch Recoveries Cyanide 85-115% Roveries EPA Methods 90-110%	1/batch Recoveries Cyanide 85-115% Recoveries EPA Methods 90-110%
Reporting Levels	Water Soil CN 10 0μg/L 10 mg/Kg TSS 4 0 mg/L -NA- F 0 10 mg/L 10 mg/kg I 2 0 mg/L 20 mg/Kg Br 2 0 mg/I 20 mg/Kg I(IC) 0 1 mg/L 1 mg/Kg Br (IC) 0 1 mg/L 1 mg/Kg	Water Soil CN CRDL 10 ug/L 1 0 mg/kg TSS 4.0 mg/L -NA- F 0.10 mg/L 1.0 mg/kg I 20 mg/L 20 mg/Kg Br 2 0 mg/L 20 mg/Kg I (IC) 0 1 mg/L 1 mg/Kg Br(IC) 0 1 mg/L 1 mg/Kg
Dilutions	If Linear Range is Exceeded	If Linear Range is Exceeded
Report	LIMS Report	CLP Report
Review	Peer or Supervisor	Peer or Supervisor
Price		

pH (EPA 150 1)
Cyanide (CLP-SOW)
Total Suspended Solids (EPA 160 2)
Fluoride (EPA 340 2)
Iodide (EPA 345 1), Titrametric (Phospholine Iodide)
Iodine (EPA 300 0), Ion Chromatography (IC)
Bromide (EPA 300 1), Titrametric
Bromide (EPA 300 0), Ion Chromatography (IC)

PROJECT: MEMPHIS DEFENSE DEPOT CATIONS

CATIONS				
	LEVEL 2	LEVEL 3		
NO	NO CHANGE IN SAMPLE PREPARATION			
Instrument Tune	ICP Scan No GFAA Hg - by CVAA	CLP/SOW Criteria CLP ICP + GFAA+CVAA		
Instrument Blank	Target Analytes < 5xCRDL	Target < CRDL		
Method Blank	1-20/Target Analytes < 5xCRDL	1:20 CLP Criteria		
Initial and Continuing Calibration	CCV/CCB 1.20 CCV 70 - 130% recoveries Calibration ICP Blank + 1 standard Hg Blank + 3 standards	Calibration: CLP Criteria CLP ICV % Recovery 90-110% ICP, GFAA 80-120% Hg 85-115% CN CRA/CRI @ 1/run 2/run ICP		
Interference Check	ICSA Beginning I ICSAB End 1 70-130%	ICSA/ICSAB 80-120% 1 set/ICP rua		
MS/DUP	Post Spike 1 20 MS/DUP 1 20 or as requested	1 MS 1:20 1 DUP 1:20 GFAA Post Spikes 85-115% (every sample)		
LCS	1 20, Soil - EPA Criteria (0287) Recovery 70-130% H ₂ O	1:20; Soil - EPA Criteria (0287) % Recovery 80-120% H ₂ 0		
Reporting Levels	As 100 ICP & Hg Pb 50 Same as CRDL Se 60 Ti 60 (See Attachment)	CLP Criteria		
Dilutions	Any sample response 10% above Linear Range	CLP Criteria		
Report	LIMS Form I	CLP Cntena		
Review	Analyst 100% Technical Review 10%	CLP Criteria		
Price				

OC Pesticides and PCBs by GC/ECD			
Quality Control	DOQ Level 2 Criteria (Screen)	DOQ Level 3 Criteria (CLP SOW OLM01.9)	
istriment blanks	As needed Targets < 5 \ RL	At CLP SOW specified frequency Targets < 1/2 CRQL	
Method blanks	Targets < 5 \ CRQL	Targets < CRQL	
MS/MSD	Frequency = 1 set / 20 samples Use lab generated limits as advisory Recovery outside of limits will be investigated for possible explanation	Frequency = 1 set / 20 samples Use CLP limits - CLP does not require corrective action.	
Surrogate spikes	Use lab generated limits as advisory Recovery outside of limits will be investigated for possible explanation	Use CLP limits - CLP does not require corrective action	
LCS (a blank spike is prepped with every MS/MSD for internal QC & control charting)	No criteria	Not required by CLP SOW	
lutial calibration	DEM - Endrin and 4,4'-DDT degradation must each be ≤30% 3 point of single-component pesticides (22-C mix) should produce correlation coefficient ≥ 0.95 or 25%RSD (linearity check) PCB LOC at RL (to be used for identification) Toxaphene/Chlordane at RL	Standard CLP requirements RESC - check resolution PEM - check degradation (Endrin and 4,4'-DDT each ≤ 20%, combined ≤ 30%) All multi-component targets at CRQL (single pt) 3 levels of single-component pesticides to demonstrate instrument linearity (INDA/INDB)	
Continuing calibration	Mid-level 22-C - should be ≤25%D from initial Then recalibrate with this as single point Frequency = after every 20 samples (approximately every 12 hours)	CLP specified standards and frequency PIBLK/PEM and PIBLK/INDAM/INDBM alternating to bracket 12 hour blocks RF < 25% from initial and degradation criteria same as initial	
	Mid-level multi-component standard of any hit in a sample - should be run within 48 hours of sample. This single point will be used to calculate	Multi-component targets found in any samples will be run within 72 hours of sample (for identification). Calc. from initial single point	
Retention time windows	No defined RT windows Analyst will compare RT and/or RRT to nearby applicable standards when targets are tentatively identified	CLP specified RT windows	
Internal standards	Internal standard quantitation will be used. No quantitative criteria for IS response.	As specified in CLP SOW, only external standard quantitation will be used	
Cleanup (Sulfur removal with Hg for all Pesticides/PCBs)	Pest and Pest/PCB will go through CLP approved lots of florisi! PCBs will be partitioned against sulfuric acid (which is a very effective cleanup)	Cleanups will be performed as specified in CLP SOW with CLP enterna. Florisil for all samples and GPC for all soils.	
Second-column confirmation	Second column confirmation will be done as needed and will have same criteria as primary But as long as criteria is met on one column, analysis will continue	As required by SOW - dual column analysis with same criteria for both columns. CLP SOW does not designate primary and confirmation.	
Reporting limits - may vary depending on chromatographic data	CLP SOW CRQLs	CLP SOW CRQLs	
Dilutions	As needed to provide accurate quantitation Single component pesticides will be within initial curve range. Multi-component targets are calculated from single point and will be diluted to be within approximately 20%-200% of standard (this is the typical range of 5 point curve for 8080 CLP has no criteria for dilution of PCBs or Tox.)	Per CLP SOW	
Report	Form Is	CLP Forms	
EData	CDA		

Herbicides by GC/ECD			
Quality Control	DOQ Level 2 Criteria (Screen)	DOQ Level 3 Criteria (8150/8151)	
istrument blanks	Optional As needed Targets < 5 \ RL	Optional Analyzed as needed Targets < R1.	
Method blanks	Targets < 5 x RL	Targets < CRQL	
MS/MSD	Frequency = 1 set / 20 samples Use lab generated limits as advisory Recovery outside of limits will be investigated for possible explanation	Frequency = 1 set / 20 samples Use lab generated limits	
Surrogate spikes	Use lab generated limits as advisory Recovery outside of limits will be investigated for possible explanation and corrective action	Use lab generated limits	
LCS (a blank spike is	No criteria	Frequency = 1 per MS/MSD	
prepped with every MS/MSD for internal OC & control charting)		Use lab generated acceptance limits if MS/MSD does not meet criteria	
Initial calibration	3 point of all targets and surrogates Curve should ≥ 0.95 correlation coefficient or 25%RSD	5 point of all targets and surrogates Curve ≥ 0 995 correlation coefficient or 20% RSD Establish initial RT windows	
Continuing calibration	Mid-level injected after every 20 samples (approximately every 12 hours) Criteria ≤25%D from initial. Then recalibrate with this as single point	Mid -level injected after every 10 samples Criteria ≤ 15% D from initial RT windows can be updated once a day	
Retention time windows	No defined RT windows Analyst will compare RT and/or RRT to nearby applicable standards when targets are tentatively identified	RT windows are based upon actual retention time variation measured in accordance with Method 8000 published in SW-846, Test Methods for Evaluating Solid Waste, Third Edition. Nov 1986 Can be updated once per day	
nternal standards	Internal standard quantitation will be used. No quantitative criteria for IS response.	Internal standard quantitation will be used No quantitative criteria for IS response	
Cleanup	Cleanups will be performed as described in lab SOPs	Cleanups will be performed as described in lab SOPs	
Second-column confirmation - will be done as needed	Same criteria as primary But as long as criteria is met on one column, analysis will continue	Same criteria as primary But as long as criteria is met on one column (and confirmation of any compound exceeding limits is not needed) analysis will continue	
Reporting limits - may vary depending on chromatographic data	Typical lab RL (attached)	Typical lab RL (attached)	
Dilutions	As needed to provide accurate quantitation Dilutions will be performed so that targets are within initial curve range	As needed to prevent target compounds from exceeding instrument calibration range	
Report	Form Is	CLP-like forms	
EData	CDA		

PNAs (Polynuclear Aromatic Hydrocarbons) by GC/FID			
Quality Control	DOQ Level 2 Criteria (Screen)	DOQ Level 3 Criteria (8100)	
Instrument blanks	Optional As needed Targets < 5 \ RL	Optional Analyzed as needed Targets < RL	
Method blanks	Targets < 5 x RL	Targets < CRQL	
MS/MSD	Frequency = 1 set / 20 samples	Frequency = 1 set / 20 samples	
	Use lab generated limits as advisory Recovery outside of limits will be investigated for possible	Use lab generated limits	
	explanation		
Surrogate spikes	Use lab generated limits as advisory Recovery	Use lab generated limits	
	outside of limits will be investigated for possible explanation and corrective action	j	
LCS (a blank spike is	No criteria	Frequency = 1 per MS/MSD	
prepped with every		Use lab generated acceptance limits if MS/MSD	
MS/MSD for internal		does not meet criteria	
QC & control charting)			
Initial calibration	3 point of all targets and surrogates Curve	5 point of all targets and surrogates Curve >	
	should ≥ 0 95 correlation coefficient or 25%RSD	0 995 correlation coefficient or 20% RSD Establish initial RT windows	
Continuing calibration	A feet level encoted offer even; 20 complex		
Continuing Canbration	Mid-level injected after every 20 samples (approximately every 12 hours) Criteria <25%D	Mid -level injected after every 10 samples Criteria ≤ 15% D from initial	
	from initial Then recalibrate with this as single	RT windows can be updated once a day	
	point	KT windows can be updated once a day	
Retention time	No defined RT windows Analyst will compare	RT windows are based upon actual retention time	
windows	RT and/or RRT to nearby applicable standards	variation measured in accordance with Method	
	when targets are tentatively identified	8000 published in SW-846. Test Methods for	
		Evaluating Solid Waste, Third Edition, Nov. 1986	
·		Can be updated once per day	
anternal standards	Internal standard quantitation will be used. No	Internal standard quantitation will be used. No	
	quantitative criteria for IS response.	quantitative criteria for IS response	
Cleanup	Cleanup necessity and technique will depend on matrix	Cleanups will be performed as described in lab SOPs	
Second-column	Same criteria as primary But as long as criteria	Same criteria as primary But as long as criteria	
confirmation - will be	is met on one column, analysis will continue	is met on one column (and confirmation of any	
done as needed		compound exceeding limits is not needed)	
		analysis will continue	
Reporting limits - may	Typical lab RL (attached)	Typical lab RI. (attached)	
vary depending on			
chromatographic data			
Dilutions	As needed to provide accurate quantitation.	As needed to prevent target compounds from	
-	Dilutions will be performed so that targets are	exceeding instrument calibration range	
Danort	Within initial curve range	CI D like Germa	
Report FData	Base level (spreadsheet) or Level 1 Form Is	CLP-like forms	
ट छत्तव	LUA	<u> </u>	

PROJECT: MEMPHIS DEFENSE DEPOT

GC/MS			
	LEVEL 2	LEVEL 3	
NO PROCEDURAL CHANGES IN SAMPLE PREPARATION			
Instrument Tune or Tune Verification	1/24 Hrs. Full Method Compliance	Every 12 Hours Full Method Compliance	
Method Blank	1/day/instrument or 1/batch or as needed Target Analytes < 5 x RL	1/20 or 1/Batch Common Contaminants - CLP Guidelines	
Initial Calibration	3 Levels (VOA 10-200) (SVO 20-160) RSD < 50%; Minimum RF - None Select List of Compounds (CCC)	5 Levels (VOA 10-200) (SVO-20-160) Method Criteria	
Continuing Calibration	Mid Point: 1/day RPD <50% Select List (CCC + SPCC)	Method Criteria	
MS/MSD	1 pair/20 samples or as requested Method Specified List %R within + 20% D from Method Criteria	1/20 Per Matrix Method Specified List Method Criteria	
Surrogates	All samples. Reanalyze of <10% - >200% of method specified recoveries I out each fraction VOA, B/N, A/E	All samples CLP Criteria	
Internal Standards	Every injection +150%, -75% up to 2 out Analyst's discretion	Every injection Method Limits (+100%, -50%)	
Second Vendor Standard	None	Analyze after each new stock calibration mix	
Sample Screening	As needed	As needed	
Sample Cleanup	If needed	CLP Guidelines	
Reporting Levels	CLP/CRDL	CLP/CRDL	
Dilutions	20% above the highest standard Analysts' discretion	CLP Guidelines	
Report	Form I; E-Data - CDA	QAL Level 2	
Review	Analyst 100% Tech Review 5%	Analyst 100% Forms 100% Tech Review 100%	
Price			

TRIANGLE LABS DIOXINS/FURANS GCMS

	LEVEL 2	DLFM01.1 (CLP)
NO PROCEI	OURAL CHANGES IN SAMPLE PR	EPARATION
Instrument Tune	Same	Verified prior to each sample: per method and instrument specifications
Method Blank	1/20 or batch, target analytes <[DL	1/20 or batch . Target analytes < 2% of internal standard
Initial Calibration	Same	5 point RSD <15%
Continuing Calibration	Same	Midpoint 1/12 hours %D < 30%
MS/DUP	Same	i Pair/20 Samples, method analyte, % recoveries 50-150% RPD < 50%
LCS/LCSD	Same	When MS/DUP not requested same analytes & criteria
Surrogates/Internal Standards	Same	All samples, % recoveries 25- 150%, some out - analyst discretion
Recovery Standards	Same	All samples, signal to noise > 10 1; retention time within 10 sec of calibration
Sample Screening	If needed	lf needed
Sample Cleanup	Same	As per method
Reporting Levels	Same	EDL's. Soil Water Tetra 1 ppb or 10 ppt Penta Hepta 2-5 ppb or 25 ppt Octa 5 ppb 50 ppt
Dilutions	On saturated peaks exceeding linear range	On analytes greater than calibration range at client request (chargeable rerun)
Report	Formaster (Form I): Case Narrative, Sample Documentation	Full CLP package
Review	Data Review, Peer Review/QC	Data Review, Peer Review/QC, Quality Assurance Review
Second Column Confirmation	No .	If TEF> 7ppt (water) or 0 7 ppb (soil)

FINAL PAGE

ADMINISTRATIVE RECORD

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